

**HISTORICAL MINING CONTAMINATION AND FLOODPLAIN EVOLUTION  
ALONG LOWER PEARSON CREEK, SW MISSOURI**

A Masters Thesis

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The Graduate College of  
Missouri State University

In Partial Fulfillment

Of the Requirements for the Degree

Master of Science, Geospatial Sciences in Geography and Geology

By

Patrick J. Womble

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# **HISTORICAL MINING CONTAMINATION AND FLOODPLAIN EVOLUTION ALONG LOWER PEARSON CREEK, SW MISSOURI**

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## **ABSTRACT**

Contaminated historical mining sediment has been used in the past as a stratigraphic tracer to study the effects of settlement on floodplain deposition. Lead and zinc mining near Pearson Creek watershed (58 km<sup>2</sup>), Springfield, Missouri began around 1885, peaked around 1912, and ended by 1920. The purpose of this study is to use the historical stratigraphic record in floodplain deposits to determine channel response to land use changes. The objectives are to (1) determine the magnitude and distribution of mining-contaminated sediment within active and historical alluvial deposits; (2) identify geo-stratigraphic assemblages using floodplain sedimentology and trace-metal dating; and (3) use geo-stratigraphic assemblages to develop a geomorphic model of historical floodplain evolution. Geochemical and textural data from soil samples collected along cross-sections were used to identify geo-stratigraphic assemblages and calculate sedimentation rates. Three assemblages were identified based on down-core stratigraphic patterns of Zn and soil color: Terrace Veneer, Floodplain Drape, and Channel Fill. Mean Zn concentration increased from Terrace Veneer (85 ppm) to Floodplain Drape (396 ppm) to Channel Fill (1,441 ppm). Sedimentation rates were highest during the mining period (mean=2.20 cm/yr) and decreased during the post-mining period (mean=0.64 cm/yr). Terrace abandonment and vertical accretion of uncontaminated sediment were dominant during the pre-mining period. Lateral migration upstream and vertical accretion downstream dominated during the mining-period. Vertical accretion has dominated the post-mining period. Alluvial deposits along lower Pearson Creek are contaminated with mining-related Zn and post-settlement land use changes have influenced floodplain sedimentation patterns.

**KEYWORDS:** floodplains, geomorphology, Pearson Creek, mining pollution, land use

This abstract is approved as to form and content

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# CHAPTER 1

## INTRODUCTION

Concerns exist worldwide over the long-term effects of mining pollution on water quality and sediment contamination in rivers. Historical mining for base metals such as lead and zinc released large amounts of metalliferous waste into nearby streams, potentially contaminating food and drinking water sources and altering the natural balance of ecosystems. Pearson Creek (Figure 1) is an outlying sub-district of the Tri-State Mining District located near the junction between Missouri, Oklahoma, and Kansas. Lead and zinc mining near Pearson Creek began in the early 1840s, intensified during the late 1880s, and ended around 1920 (Thomson, 1986). During those times, mining waste disposal was not regulated and mining operations would dispose of waste in unstable tailings piles or discharge mill waste directly into Pearson Creek (Fairbanks and Tuck, 1915). A previous screening-level study indicated that a significant volume of mining sediment is stored within the alluvial deposits of nearby floodplains and active stream channel deposits (Owen and Pavlowsky, 2000). Mining-related metal contamination has also been released from Pearson Creek into the James River (Owen and Pavlowsky, 2000; Frederick, 2001) and more recently Lake Springfield (Tannehill, 2002). However, the spatial distribution of mining sediment within floodplain deposits along lower Pearson Creek remains largely unknown.

Watershed-scale contamination of river systems by metals released from mining operations is dependent on the sediment transport and storage capacity of the stream. Concentrations of contaminated sediment tend to be high close to abandoned mine sites and decrease with distance downstream (Bradley and Cox, 1986; Graf, 1996; Carlson,

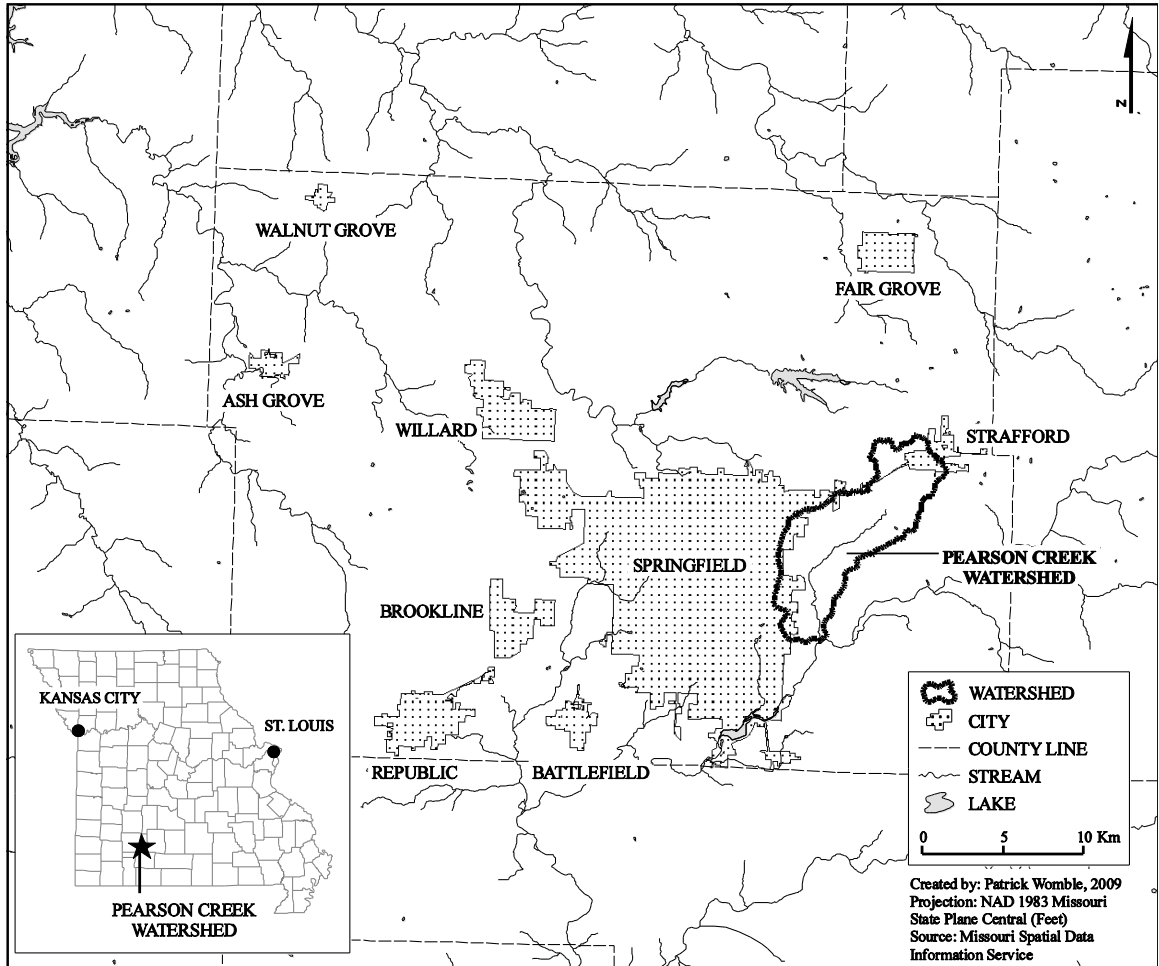


Figure 1. Pearson Creek watershed.

1999; Lecce and Pavlowsky, 2001; Trimble, 2001). At the local scale, the magnitude and distribution of contaminated sediment can vary considerably depending on the types of fluvial forms present, how and when they were formed, and how effectively they store sediment. Mining sediment can be sorted by fluvial processes in a reach where fines are deposited on floodplains or flushed downstream and/or where sand and gravel are deposited on the bed or in temporary bar forms (Graf, 1996, Hudson-Edwards, 2003).

Sediment stored in fluvial systems is often remobilized or recycled back into the stream. This process can be physical and/or chemical in nature and may result in continuing pollution long after mining has ended as contamination is re-introduced back into the channel for transport (Lewin et al., 1977). Physical processes, such as erosion caused by channel migration, can reincorporate metalliferous material back into the flow while chemical processes, such as dissolution and pedogenesis, can alter the geochemistry of the metals into forms readily transported in solution or more bioavailable to plants (Horowitz, 1991). The long-term risk of pollution is more of a geomorphic problem in areas where physical processes (erosion and channel migration) occur at much faster rates than chemical releases. In such areas, physical processes occur relatively fast so there is not sufficient time for chemical weathering or pedogenesis to take effect. Therefore, factors that cause channel instability such as increased sediment and/or water supply increase the chances that contaminated sediment stored in floodplains will be remobilized.

Stream channels have a natural tendency to migrate, but when the process is accelerated by anthropogenic activities such as urbanization or agriculture, sediment remobilization occurs at a greater rate. It is well known that land use changes in a watershed influence geomorphic processes such as floodplain sedimentation rates,

erosion, and channel form (Knox, 1977; Trimble and Lund, 1982; Magiligan, 1985; Beach, 1994; Jacobson and Primm, 1994; Faulkner, 1998; Walling, 1999). To explore the effects of anthropogenic influence on a watershed, geomorphologists study the stratigraphy and geomorphic history of the streams within it. To do this, the stratigraphy of physical, chemical, biological, or anthropogenic materials within alluvial sediments are used to serve as temporal markers to date sediment. Types of indicators, or tracers, include, but are not limited to, buried soils, pollen, archaeological artifacts, geochemical changes in substrate, radioisotopes, and trace elements. Mining-contaminated sediment has been used by many workers in the United States and abroad to investigate timing and rates of sedimentation, sediment provenance, floodplain evolution, anthropogenic impacts on the watershed, and patterns of floodplain sediment storage (Lewin et al., 1977; Bradley and Cox, 1986; Knox, 1987; Bradley 1989; Marron, 1992; Graf, 1996; Brewer and Taylor, 1997; Hudson-Edwards et al., 1998; Smith et al., 1998; 1999; Lecce and Pavlowsky, 2001; Ciszewski and Malik, 2004; Lecce et al., 2008).

Studies by Knox (1987) and Lecce and Pavlowsky (2001) demonstrate the feasibility of using Zn-contaminated sediment as a reliable method for dating alluvial deposits. Knox (1987) used Zn concentrations and buried soils in floodplain sediment to date sediment layers and determine overbank sedimentation rates in the Galena River watershed in Wisconsin and Illinois. He found that sedimentation rates were higher during periods of intense agriculture prior to the use of conservation practices and that channel enlargement decreased sedimentation rates over time by containing larger floods. Similarly, in the same region, Lecce and Pavlowsky (2001) also used buried soils and mining-related Zn concentrations to date channel and floodplain deposits to investigate how floodplain sedimentation changed over time within the Blue River Watershed in

Wisconsin. They found that sedimentation rates were high early on in the headwaters, metal peaks were buried deeper downstream, and lateral migration terraced historical floodplains. Both studies found high sedimentation rates in the headwaters and low sedimentation in the lower valleys during the pre-mining period. Following this, channel widening in the headwaters enabled those streams to contain and convey sediment and floods downstream, decreasing sedimentation in the headwaters and increasing sedimentation in the lower valleys.

### **Previous Studies near Pearson Creek**

There have been previous studies of mining-affected stream sediment in the Tri-State Aurora sub-district in Lawrence County, Missouri by Carlson (1999) and Trimble (2001). Carlson (1999) explored floodplain sedimentation rates using mining tracers in Honey Creek while Trimble (2001) calculated in-channel and overbank sediment budgets to estimate contamination release and risk in Chat Creek. Carlson found that Zn concentrations were as much as 575 times background concentrations and overbank floodplain sedimentation rates immediately following land clearing and during mining averaged 0.82 cm/yr and decreased to 0.60 cm/yr after mining. Trimble found that bank erosion releases 929 Mg of sediment and that 321 kg of Zn are released into Chat Creek each year. Both of these studies used bank exposures to estimate contamination and did not explore the spatial distribution of contaminants in floodplain deposits across the valley floor.

Nearer to Pearson Creek, Frederick (2001) examined phosphorous concentrations in active channel sediments along the James River and included Zn concentration data. Three of Frederick's sites were located near Pearson Creek: one upstream of Pearson

Creek on the James River, one on Pearson Creek, and one downstream of the confluence. For Zn, Frederick reported 54 ppm upstream, 1,100 ppm in Pearson Creek, and 264 ppm just downstream. The five-fold concentration increase from the upstream site to the downstream site indicates that Pearson Creek is presently discharging mining-related Zn into the James River. Tannehill (2002) supported this conclusion while studying metal concentrations in the bottom sediment of Lake Springfield, approximately 7.5 kilometers downstream of where Pearson Creek enters the James River. The mean value for Zn in all lake bottom sediment was 113 ppm, over double the concentration found by Frederick (2001) upstream of Pearson Creek. These two studies show that Zn from historical mining along Pearson Creek is probably entering the James River and being transported downstream and deposited in Lake Springfield.

A Brownfield Targeted Assessment (BTA) conducted in 2007 by the Missouri Department of Natural Resources near Pearson Creek and Ash Grove focused on near-surface topsoil contamination of lead, zinc, and asbestos in neighborhoods in the lower and middle portion of the watershed (MoDNR, 2008). The report concluded that mining operations in the area did not significantly contaminate topsoil and would not pose a large threat to the surrounding community. However, sample sites in the MoDNR study were located on the surrounding uplands, not in the valley bottoms.

An initial undergraduate study by Owen and Pavlowsky (2000) focused on the distribution of historical mining pollution within the floodplain deposits in the current study area. The study examined sixteen in-channel sediment samples and six cutbank exposures along lower Pearson Creek and the James River. Three bank sites were located on historical floodplains and three on older, pre-mining terraces. Two main findings were: (1) in-channel sediment samples from Pearson Creek and the James River,



upstream and downstream of the confluence, revealed high zinc concentrations along lower Pearson Creek that decreased in the downstream direction; and (2) terrace surfaces were capped by only 30-60 cm of contaminated sediment, while historical, lower elevation floodplain surfaces were contaminated throughout. They concluded that the stream experienced a significant amount of sedimentation since the mining period and considerable amounts of contaminated sediment are actively moving and stored within the system.

The previously highlighted studies in southwest Missouri show that (1) a question of the degree and extent of contamination along lower Pearson Creek remains and (2) metal contamination trends across the valley floor of Pearson Creek have not been determined. Furthermore, excluding the Owen and Pavlowsky (2000) study, no research has addressed the dissemination of mining-related Zn in historical and recent floodplain sediment near Pearson Creek. This study expands on the findings of Owen and Pavlowsky to characterize the vertical and lateral trends of mining-related contamination in lower Pearson Creek. In addition, this study attempts to develop a timeline of geomorphic change using contaminated historical mining sediment as a tracer.

### **Purpose and Objectives**

Ozark streams as a whole have not been widely studied from the environmental and geomorphic perspective which has resulted in a severe gap in the literature as to how they have responded to historic land use changes induced by settlement. Exceptions include work by Jacobson and Primm (1994) on the effects of land use changes on streams in eastern Missouri, several Missouri State University Master's Theses regarding historical channel changes and channel geometry in streams in southwest Missouri

(Legleiter, 1999; Horton, 2003; Wyllie, 2002), and the previously mentioned mining-related studies by Carlson (1999), Trimble (2001), MoDNR (2008), and Owen and Pavlowsky (2000). However, none of these studies specifically examined Pearson Creek pollution or the sedimentology and distribution of mining sediment at the Pearson Creek-James River confluence zone. The purpose of this study is to better document the distribution of Zn in floodplain deposits and to use the historical mining record in floodplain deposits to determine channel response to land use changes since European settlement. The objectives are to:

- (1) Determine the magnitude and distribution of mining-contaminated sediment within active and historical floodplain and terrace alluvial deposits;
- (2) Identify geo-stratigraphic assemblages using floodplain sedimentology and trace-metal dating; and
- (3) Develop a geomorphic-based model to describe contamination patterns in floodplain deposits and interpret stratigraphic relationships among contaminated floodplain deposits.

## **Benefits**

First, this research will help us understand how streams in the Ozarks have responded to historical land use change by exploring spatial-stratigraphic relationships of mining-contaminated floodplain deposits. Second, this study examines stratigraphic sedimentation patterns and relates them to land use changes in a tributary-main stem confluence zone. The literature surrounding confluence zones has largely ignored confluence stratigraphy due to its complex nature and instead mainly focused on hydrologic flow modeling (Rhoads and Kenworthy, 1994; De Serres et al., 1999), textural

and morphological characteristics of channel beds (Biron et al., 1993; Rhoads et al., 2009; Unde and Dhakal, 2009), and spatial patterns of channel change (Roy and Woldenberg, 1986). Finally, this study will document the environmental contamination in Pearson Creek, which managers can use to assess the risks associated with the remobilization of contaminated sediment and respond appropriately. Information presented here can lead to a better understanding of long-term metal contamination of river systems in the Tri-State District in general, including the more heavily mined areas in the Spring River Basin to the west and the Big River Basin to the east.

## **CHAPTER 2**

### **GEOMORPHIC CONTROLS ON THE DISTRIBUTION OF MINING CONTAMINATION IN RIVERS**

This chapter reviews the processes controlling sediment transport and distribution in fluvial systems, how those processes control the fate of contaminated sediment, and how geomorphologists use contaminated sediment profiles to interpret past geomorphic change. Geomorphic approaches have been used to understand how the dispersal patterns of metals in fluvial sediment are linked to anthropogenic alteration in watersheds (Lewin et al., 1977; Bradley and Cox, 1986; Knox, 1987; Lecce and Pavlowsky, 2001). These studies used metals as tracers to determine the timing and magnitude of changes in channel configuration and sedimentation rates in response to human impacts. In this study, mining sediment is composed of a range of relatively mobile tailings and mill waste material introduced to land areas and streams by mining operations.

#### **Watershed Systems**

Geology, climate, physiography, and land use of a watershed control the behavior of streams within it (Knighton, 1998). Changes in these variables alter the hydrologic regime of the system and bring about changes in the supply and nature of sediment transported through the watershed. Once in the fluvial system, fluvial processes govern the transport, storage, and distribution of sediment. Sediment introduced into the system has three broad origins: anthropogenic, accelerated, and natural. Anthropogenic inputs are those introduced or created directly by human activities such as direct dumping of mine tailings into the stream. Accelerated inputs include soil erosion due to agricultural

land clearing, construction, and clear-cutting. Natural inputs are dependent on the geology of the system and originate from natural erosion processes along channel boundaries, inputs from tributaries upstream, or slope wash (Knighton, 1998). After being introduced, sediment is transported downstream and can get trapped, often multiple times, in storage areas such as floodplains or lakes. Storage can be short- or long-term depending on whether it is closer to (proximal) or farther from (distal) the active channel. In general, proximal sediment is more temporary than distal sediment. Over time, sediment will continue to migrate downstream and out of the watershed to successively larger rivers (Knighton, 1998).

### **Human Impacts on Overbank Sedimentation**

It is well documented that land use change affects sedimentation in fluvial systems (Lewin et al., 1977; Knox, 1977, 1987, 1989; Trimble and Lund, 1982; Magilligan, 1985; Jacobson and Primm, 1994). Vegetation on hillslopes dissipates energy and reduces the erosivity of runoff by interrupting its flow path. When vegetation is removed or soil is exposed, the resistance of hillslopes decreases, allowing the erosivity of runoff to increase. The lack of vegetation also decreases the infiltration rate and capacity of soils in the watershed, generating more runoff. Excess runoff enables the stream to carry more material and accelerates erosion, causing the formation of rills and gullies on hillslopes. Introduction of material removed during hillslope erosion can have negative impacts on aquatic habitats, destroy crops growing on floodplains, and damage infrastructure downstream. Higher rates of overland flow also increase the magnitude and frequency of floods. Channels respond to increased discharge by deepening, widening, and altering bed forms and can get big enough to effectively cut off overbank

events altogether, conveying more sediment downstream (Brakenridge, 1988; Lecce, 1997). Human-induced changes can also include introducing pollutants into alluvial sediments.

Metal pollutants are introduced into streams via industrial, municipal, agricultural, and mining operations. Industrial and municipal metal pollutants are widespread and can include sewage, water treatment effluent, airborne particulates from power plants, landfills, and surface pollutants removed by storm water runoff. Agricultural pollutants are mainly limited to metals derived from fertilization. Base-metal mining pollutants typically include metals mobilized by tailings dam failure, eroded from tailings piles, or chemically leached from waste piles. In addition, other metal pollutants may be released by acid mine drainage, dust particulates, and waste water effluent. Pollutants derived from base-metal mining operations are the primary focus of this study.

### **Mining Contaminants in Fluvial Systems**

**Sediment Characteristics.** The main sources of contamination in watersheds with a history of mining are abandoned mines, mine waste piles, and reworked colluvial and alluvial deposits (Hudson-Edwards, 2003). In early Pb/Zn mining operations, ore was sorted by hand, broken up with hammers, and separated from gangue (host rock) with small hand jigs, a process known as concentration. As mining operations became more mechanical, ore concentration was done with large jigs operated by steam, air, or electricity (Taggart, 1945). Water was used to increase the buoyancy of the grains and allow grains with higher specific gravity than the gangue to migrate down through the vat and settle to the bottom more easily (Taggart, 1945). Screens at the bottom of the jig would catch larger gangue particles and allow passage of the concentrate. Jets of water

were commonly used to speed up the process and convey the resulting gangue slurry into nearby streams or to tailings piles. Although convenient, jigging is blind to what it sorts. For example, if grains of ore and gangue had comparable specific gravities, they would be treated equally by the system, flushed through it, and discarded. The inefficiency of this method was acceptable in areas where ore was coarsely disseminated through the host rock or at small operations because it was not economically viable to reprocess the tailings. In large operations that reprocessed sediment, the sand-sized fraction would be further ground into silt-sized sediment (fines), concentrated via flotation, and transported to holding ponds. However, slimes, the smallest size fraction ( $<50 \mu\text{m}$ ), could not be concentrated and went out with the wash water during jigging. In addition, relatively small fragments of metalliferous minerals are attached to the gangue and also ended up in tailings piles.

Many physical (grain size, surface area, specific gravity, surface charge) and chemical (adsorption, precipitation and coprecipitation, organometallic bonding, incorporation in crystalline minerals) factors control metal concentrations in sediment (Horowitz, 1991). Horowitz (1991) explained that physical and chemical controls are highly interrelated and grain size plays a role in all of these processes. Fine-grained particles have large unit surface areas and net negative surface charges, which attract positively charged metal ions (Horowitz, 1991). Therefore, since surface area increases as grain size decreases, the concentration of metals in fine-grained sediment will be higher than in coarse-grained sediment. Similarly, organic matter can concentrate metal ions due to large surface areas, high cation exchange capacity, high negative surface charge, and physical trapping. Metal ions can also be incorporated, via replacement, into Fe and Mn oxide coatings as they form on sediment grains or in soils.

**Transport and Dispersal Trends.** The suspended sediment load in a stream contains much higher concentrations of trace elements than the dissolved load and is the dominant means by which most metal contaminants are transported downstream (Horowitz, 1991). The fate of bed and suspended sediment, and thus contaminated sediment, is determined by sorting processes inherent to stream systems which preferentially transport sediment based on size and density. Fine-grained sediment is transported farther downstream or across floodplains than coarse-grained sediment due to the relative ease with which it is entrained. Local-scale distribution can vary considerably and obscure large-scale trends (Axtmann and Luoma, 1991). However, metal concentrations in both channel and floodplain deposits tend to be highest closer to abandoned mine sites and decrease with distance downstream (Lewin and Wolfenden, 1978; Bradley and Cox, 1986; Graf, 1996; Carlson, 1999; Lecce and Pavlowsky, 2001; Trimble, 2001). Downstream reductions in concentration are often attributed to physical dilution and mixing between contaminated and uncontaminated sediment (Leenaers, 1989). Sources of “clean” sediment include tributary inputs from unmined watersheds and bank erosion (Graf, 1996). Another factor controlling the decrease in concentration downstream is storage or removal of contaminants from the stream. Graf (1996) observed that local-scale variations in metal concentrations downstream are based on trap efficiency and storage capacity, and that areas capable of effectively trapping more sediment, such as wide channels or valleys, will have more contamination present than narrow zones.

**Alluvial Storage.** As sediment is transported downstream, it is stored over different timescales in channel and overbank floodplain areas (Bradley, 1989). Floodplains can form through point bar construction, vertical accretion, or a combination



of the two. Point bars are formed on the inside of meander bends as channels migrate across the valley bottom. Increased flow separation and/or bed resistance on the inside of the bend decreases the velocity of the water and causes sediment to fall out of suspension, which then becomes a nucleus for additional deposition laterally and vertically (Brakenridge, 1988). As it builds upward, flows of greater magnitude are required to inundate the surface and eventually result in the construction of a floodplain through vertical accretion. Vertical accretion is the process where, during flood events, successive deposition of fine-grained sediment slowly increases the height of the banks (Brakenridge, 1988). As the bank height increases, the rate of deposition decreases due to the greater volume of water needed to breach the banks (Brakenridge, 1988; Knighton, 1998). This type of floodplain formation is more common in low energy streams where coarse-grained sediment transport is lacking (Lecce and Pavlowsky, 2001). Floodplain deposits typically contain higher concentrations of mining-related contaminated sediment than their in-channel counterparts (Lecce and Pavlowsky, 1997; Carlson, 1999; Trimble, 2001). In fact, Lecce and Pavlowsky (1997) found that Zn levels in floodplains were as much as five times higher than those in adjacent point bar sediments.

Metal pollutants in floodplains can behave as non-point sources if remobilized and released back into the stream (Lewin et al., 1977; Knox, 1987; Bradley, 1989; Pavlowsky, 1995; Lecce and Pavlowsky, 1997; Smith et al., 1998). Remobilization is the process whereby previously stored sediment is recycled back into the streamflow due to bank erosion and stream course changes. The duration of storage between periods of remobilization is known as residence time, the length of which increases with distance from the active channel: beds (event), bars (annually), short-term floodplains (decades to centuries), and long-term floodplains or terraces (centuries to millennia). If these

landforms are contaminated, residence time estimates can help managers determine the threat and timing of contaminated sediment remobilization and thus prepare accordingly.

**Floodplain Distribution.** Floodplain contamination trends differ depending on the process controlling floodplain formation. Brewer and Taylor (1997) describe three styles of contaminant distribution controlled by vertical accretion or lateral migration in the Severn Basin, UK: flood frequency, channel incision, and lateral reworking (Figure 2). Flood frequency-controlled floodplains (Figure 2A) are located in systems with stable terrace surfaces and are controlled by how often a surface is inundated by flood waters. Smaller and more frequent floods inundate low surfaces and deposit sediment more often than higher surfaces, which require larger and less frequent floods to submerge them. Similarly, as channels incise (Figure 2B), higher terrace surfaces are progressively flooded less often over time, decreasing the amount of contaminated sediment deposited on higher surfaces as time advances. The difference between flood frequency and channel incision styles of floodplain formation is that the elevation of the channel bed in the flood frequency style is constant whereas the elevation of the bed in the channel incision style decreases. Lateral reworking (Figure 2C) is controlled by lateral bank instability of the channel and surfaces are built successively across the valley floor. Laterally reworked deposits can contain appreciable amounts of mining pollutants as well as reworked floodplain sediment.

### **Tracer Studies**

Tracer studies are based on the assumption that there is a temporal connection between the date mining sediment was released and the timing of deposition downstream. Metal tracers are a popular and reliable tool to identify geomorphic change in fluvial

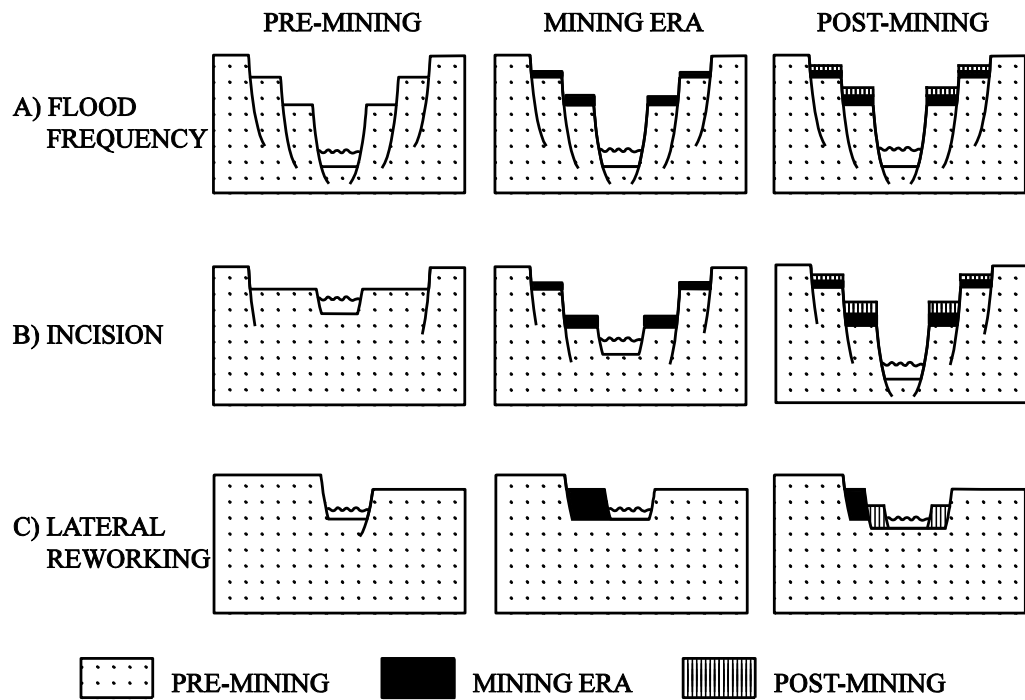


Figure 2. Styles of floodplain formation. Three floodplain styles (A) flood frequency, (B) channel incision, and (C) lateral reworking show the distribution of sediment during the pre-mining, mining era, and post-mining period. Modified from Brewer and Taylor (1997).

environments (Macklin, 1985; Knox, 1987; Bradley, 1989; Lecce and Pavlowsky, 2001). Zinc profiles in historical mining sediments can be used as stratigraphic markers to date recent sediments and calculate historical and recent sedimentation rates (Lecce and Pavlowsky, 2001). Assuming that the present surface material has not been significantly scoured or removed, two stratigraphic intervals can usually be identified: mining initiation to peak mining, and peak mining to present day. In the Zn profile, the first occurrence depth coincides with the year mining began, the peak concentration is associated with peak mining production, and everything above the peak Zn depth is representative of post-mining deposition (Lecce and Pavlowsky, 2001). Sedimentation rates can be determined by dividing each thickness by the corresponding time span related to mining production records. The presence of other stratigraphic markers such as buried soils, artifacts, or radioisotopes can help to more precisely determine timing of sedimentation.

However, one concern associated with sediment tracer studies is the mobility of the metal being investigated. The average solubility of Zn in soils ranges between 4 ppb and 270 ppb depending on soil chemistry and the method used to analyze the soil (Kiekens, 1995). Organic matter content, pH, and grain size control the solubility of Zn in soils (Kabata-Pendias and Pendias, 2000). Mobility of the  $Zn^{2+}$  ion is reduced as organic matter and pH increase or as grain size decreases. Organic matter and clay-sized particles are capable of strongly arresting  $Zn^{2+}$  ions in basic environments (Kabata-Pendias and Pendias, 2000) while acidic environments promote solubilization and desorption (Horowitz, 1991; Marron, 1992, Merrington and Alloway, 1994; Pavlowsky, 1995; Hudson-Edwards et al., 1998). Pavlowsky (1995) suggested that carbonate environments neutralize water and sediment pH, reducing the production of acid and

making Zn a reliable and stable indicator of mining sediment presence. In the Ozarks, Shepard and Gutiérrez (1999) performed sequential extraction on a soil contaminated by sewage sludge to assess the availability and mobility of heavy metals. The results showed that heavy metals only leach downward about 20 cm at most, but are bioavailable to fescue grass. Because the mineralization at Pearson Creek is hosted by limestone (typically >90% calcite), chemical mobility over periods of a century or so should not be a large factor influencing the distribution of Zn concentrations in floodplain profiles.

## **CHAPTER 3**

### **STUDY AREA**

#### **Regional Setting**

Pearson Creek watershed (58 km<sup>2</sup>) is located in Greene County, Missouri (Figure 1). The creek is a major tributary of the James River that drains the southeastern portion of the county. The watershed relief spans more than 100 m; from 353 masl in the north to 455 masl where Pearson Creek enters the James River. In July 2007, Springfield, the largest city in Greene County, had the third largest population in the state at an estimated 154,777 persons; the next largest city in the County, Republic, had an estimated population of 13,021 (U.S. Census Bureau, 2008a). Other cities in Greene County include Battlefield, Brookline, Willard, Strafford, Ash Grove, Walnut Grove, and Fair Grove (Figure 1). Pearson Creek drains the eastern portion of Springfield and the southern half of Strafford, Missouri.

#### **Geologic Setting**

The Ozarks in Missouri are part of a large asymmetric dome, the high point of which is formed by the St. Francois Mountains (Sauer, 1920). Pearson Creek is situated in the Ozark Plateau Region atop the Springfield Plateau (Thomson, 1986). The Springfield Plateau is a topographic feature dominated by Mississippian-age carbonate rocks (Thomson, 1986). The Mississippian-age rocks in the area are the Osagean (Burlington-Keokuk Limestone, Elsey, and Pierson Formations) and Kinderhookian (Northview, Compton, and Bachelor Formations) Series (Table 1; Figure 3). Chert nodules are abundant in the Lower Burlington-Keokuk, Elsey, and Pierson Formations

Table 1. General geologic stratigraphy of Greene County, Missouri from Thomson (1986) and Fairbanks and Tuck (1915).

| System                 | Series        | Group or Formation          | Lithology           | Thickness (ft)              | Mineralization |
|------------------------|---------------|-----------------------------|---------------------|-----------------------------|----------------|
| Quaternary             |               | Alluvium (Qal)              | Sand and Gravel     | Variable                    |                |
|                        |               | Terrace Deposits (Qt)       |                     | Variable                    |                |
| Pennsylvanian          |               | Channel Sand Deposits (Pcs) | Sandstone           | Variable                    |                |
| Mississippian          | Meramecian    | Warsaw Formation (Mw)       | Limestone           | >50                         |                |
|                        | Osagean       | Burlington-Keokuk (Mbk)     | Limestone           | 120-340                     |                |
|                        |               | Elsey Formation (Me)        | Cherty Limestone    | 50-80                       |                |
|                        |               | Pierson Formation           | Dolomitic Limestone | 30-40                       |                |
|                        | Kinderhookian | Northview Formation (Mnv)   | Shale               | 5-80                        |                |
| Compton Formation (Mc) |               | Limestone                   | 7-25                | Pb/Zn deposits along faults |                |
| Bachelor Formation     |               | Sandstone                   | ≤2                  |                             |                |
| Ordovician             | Canadian      | Cotter Dolomite (Oc)        | Dolomite            | 50-175                      |                |
|                        |               | Jefferson City Formation    | Dolomite            | 190-220                     |                |
|                        |               | Roubidoux Formation         | Dolomite/Sandstone  | 140-180                     |                |

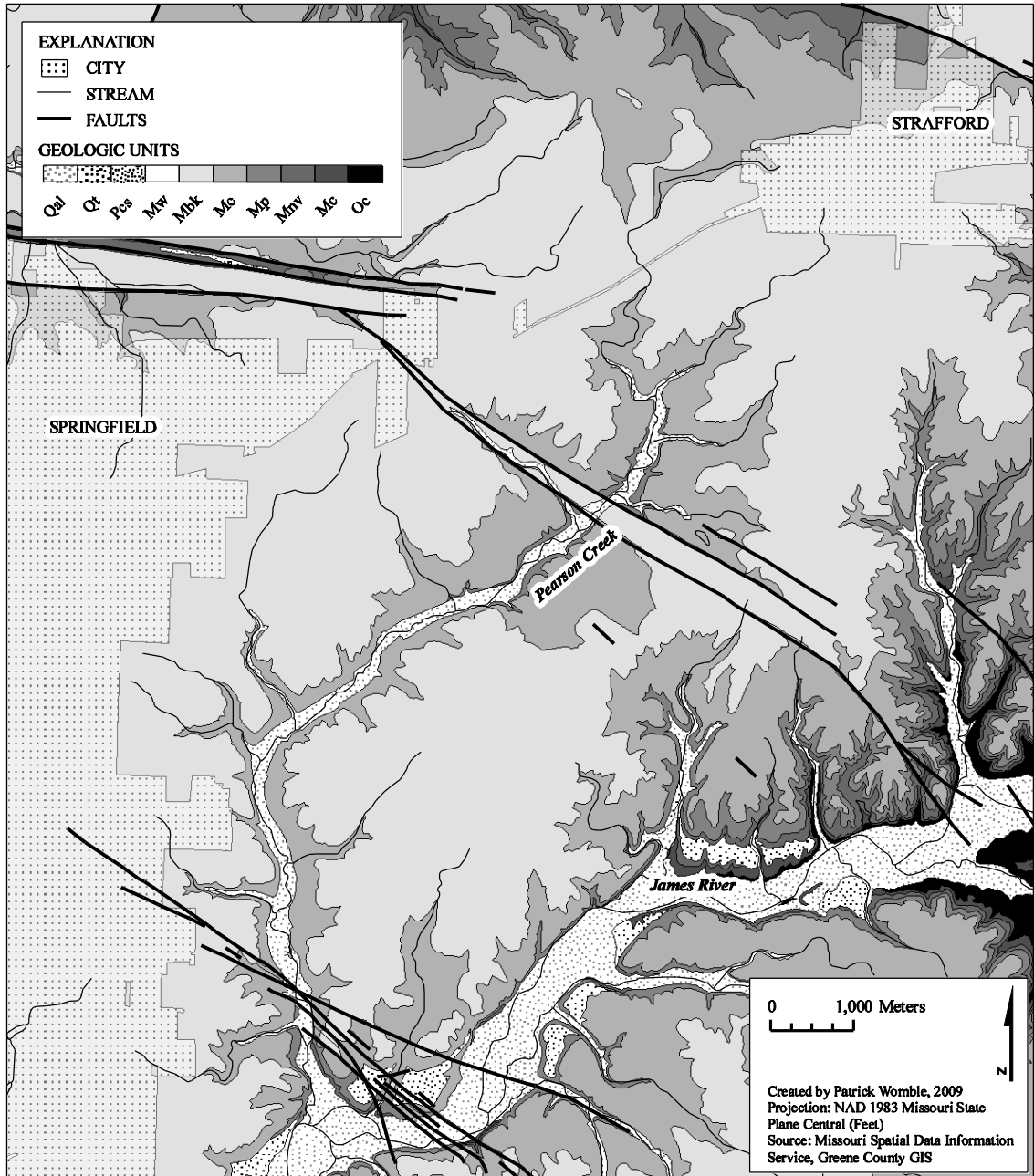


Figure 3. Stratigraphic and structural geology map of Pearson Creek watershed.



and they are found as gravel fragments in bed and bar deposits in streams. Surficial deposits include residuum, alluvium, colluvium, and Pleistocene loess (Hughes, 1982). Red cherty residuum formed from the weathering of the limestone lies on top of the surrounding ridges while alluvium and colluvium reside in the valleys and form terraces, floodplains, alluvial fans, and other features.

Faults are present in the northern and southern parts of the watershed (Figure 3) that formed as a result of the Ozark Uplift. Mineralization is concentrated along these fault zones in the Northview shale just above the Bachelor Sandstone (Thomson, 1986). Mineral deposits consisting of galena and sphalerite, and minor amounts pyrite and chalcopyrite, are typically disseminated in tallow or gumbo clay accumulations in these faults (Fairbanks and Tuck, 1915; Thomson, 1986).

A karst landscape is found in the study area and all across the Ozarks where horizontally-bedded limestone is at the surface. Karst features are formed when dissolution processes expand bedding planes and fractures in carbonate rock to form caves and conduits. Some karst features present in Greene County include cutters, pinnacles, sinkholes, springs, caves, and losing streams (Thomson, 1986). In and around the Pearson Creek watershed are numerous springs, losing streams, caves, and sinkholes.

## **Soils**

The parent material of upland soils in the watershed is generally composed of loess over residuum. Goss, Wilderness, and Peridge soil series are present on the uplands around Pearson Creek (Figure 4, Table 2; Hughes, 1982). Goss soils are deep, well-drained, and located on hillsides and formed in residuum weathered from cherty limestone or dolomite. Wilderness soils, also formed from weathered cherty limestone,

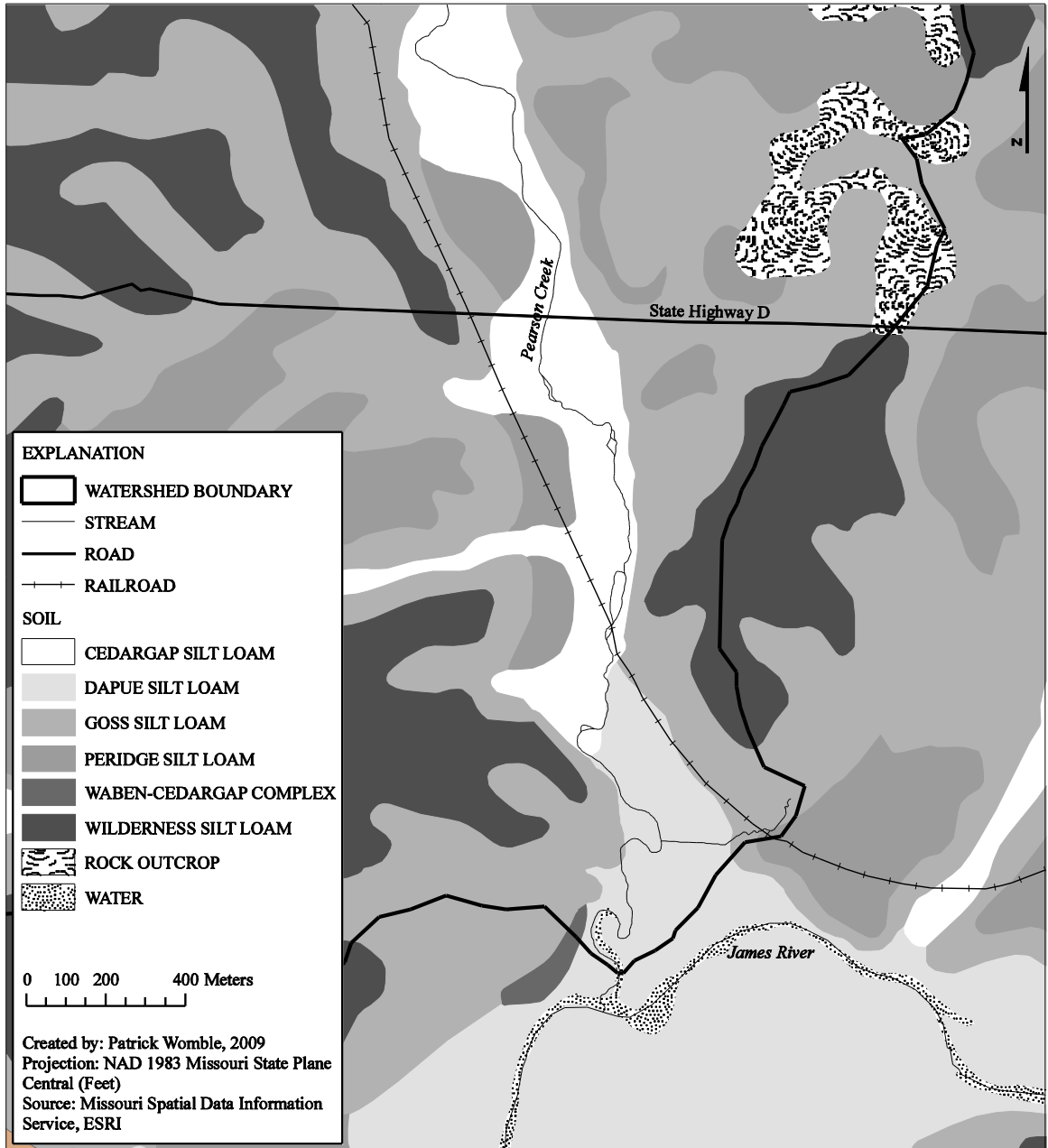


Figure 4. Soils along lower Pearson Creek.

Table 2. General description of soil series found along Pearson Creek (Hughes, 1982; NRCS, 2008).

|                | Soil Series            | Parent Material   | Landform Position                     | Slope (percent) | Taxonomic Class  |
|----------------|------------------------|---|---------------------------------------|-----------------|--|
| UPLAND SOILS   | Goss                   | Colluvium and residuum weathered from cherty limestone                            | Upland slopes                         | 2 to 20         | Clayey-skeletal, mixed, active, mesic Typic Paleudalfs   |
|                | Wilderness             | Colluvium and residuum weathered from cherty limestone                            | Upland flats/<br>broad areas          | 2 to 9          | Loamy-skeletal, siliceous, active, mesic Oxyaquic Fragiudalfs  |
|                | Peridge                | Older alluvium to colluvium and residuum weathered from cherty limestone or loess | Upland/<br>Terrace                    | 0 to 8          | Fine-silty, mixed, active, mesic Typic Paleudalfs  |
| ALLUVIAL SOILS | Dapue                  | Silty alluvium  | Low Terrace<br>Floodplain             | 0 to 3          | Fine-silty, mixed, active, mesic Fluventic Hapludolls  |
|                | Cedargap               | Alluvium  | Floodplain                            | 0 to 5          | Loamy-skeletal, mixed, superactive, mesic Cumulic Hapludolls   |
|                | Waben-Cedargap Complex | Cherty alluvium or colluvium  | Alluvial-colluvial fan,<br>foot slope | 0 to 5          | Loamy-skeletal, siliceous, active, mesic Ultic Hapludalfs/Loamy-skeletal, mixed, superactive, mesic Cumulic Hapludolls |

are located on the tops and sides of upland ridges, and are moderately well-drained.

Peridge soils, found on the tops and sides of upland ridges, in upland depressions, and as Pleistocene (or older) alluvial terraces and upland benches, can be formed from cherty limestone residuum or weathered Pleistocene loess.

The alluvial soils series found along Pearson Creek are Dapue, Cedargap, and the Waben-Cedargap complex (Figure 4, Table 2). Dapue soils are found in the southern portion of the study area, near the confluence of Pearson Creek and the James River. They are well-drained soils formed in silty alluvium and are found on floodplains and low stream terraces of rivers (NRCS, 2008). Cedargap soils are limited to the northwest corner of the study area. They are typically found on floodplains of small streams near active channels and are characterized by a high content of chert fragments (Hughes, 1982). The Waben-Cedargap complex, a combination of Cedargap (40%) and Waben (45%) soils, is found near the confluence between Pearson Creek and the James River. Waben soils are very deep, well-drained, and form in cherty alluvium or colluvium sometimes associated with alluvial fans (NRCS, 2008).

## **Climate**

The climate in the region of Pearson Creek is characterized by warm, humid summers and mild, cool winters. Weather fronts generally move west to east with warm, moist air moving north from the Gulf of Mexico, and cool air moving south from Canada. The mean annual temperature between 1971 and 2000 recorded at the Springfield-Branson Airport was 56.2° Fahrenheit, the annual mean low was 45.0° Fahrenheit, and the annual mean high was 67.4° Fahrenheit. The mean annual precipitation between 1971 and 2000 was approximately 45 inches. The months with the lowest annual mean

precipitation (December, January, and February) also have the coldest mean annual temperatures. The wettest months are typically April, May, June, September, and November and the two hottest months are July and August (Figure 5).

## **Hydrology**

The limestone geology in the area has led to complex karst hydrology, demonstrating its influence through the presence of gaining and losing streams, sinkholes, and springs. All of the tributaries along Pearson Creek, with the exception of Jones Branch, are classified as losing streams (Figure 6). Also, the main stem of Pearson Creek has a losing segment just above the Jones Branch tributary input (Bullard et al., 2001). There are a few small sinkholes scattered throughout the watershed (Figure 6). Just outside the eastern and western boundaries of the watershed are large fields of documented sinkholes.

A gaging station operated by the USGS along Pearson Creek is located just upstream of the study area (Figure 7). Flow records for the gage were available from 1999-2008 and are summarized in Table 3. The mean annual discharge is 24.0 cfs. Backflooding from the James River is common during floods and can back water up past where the railroad bridge crosses Pearson Creek in a 10-year flood (USACE, 1970). The highest recorded flood during this time period was on June 13, 2008 and had a discharge of 2,980 cfs. Flood waters from the James River backed up Pearson Creek far enough to inundate the entire study area.

## **Land Use History**

Population around Pearson Creek is influenced by the City of Springfield.

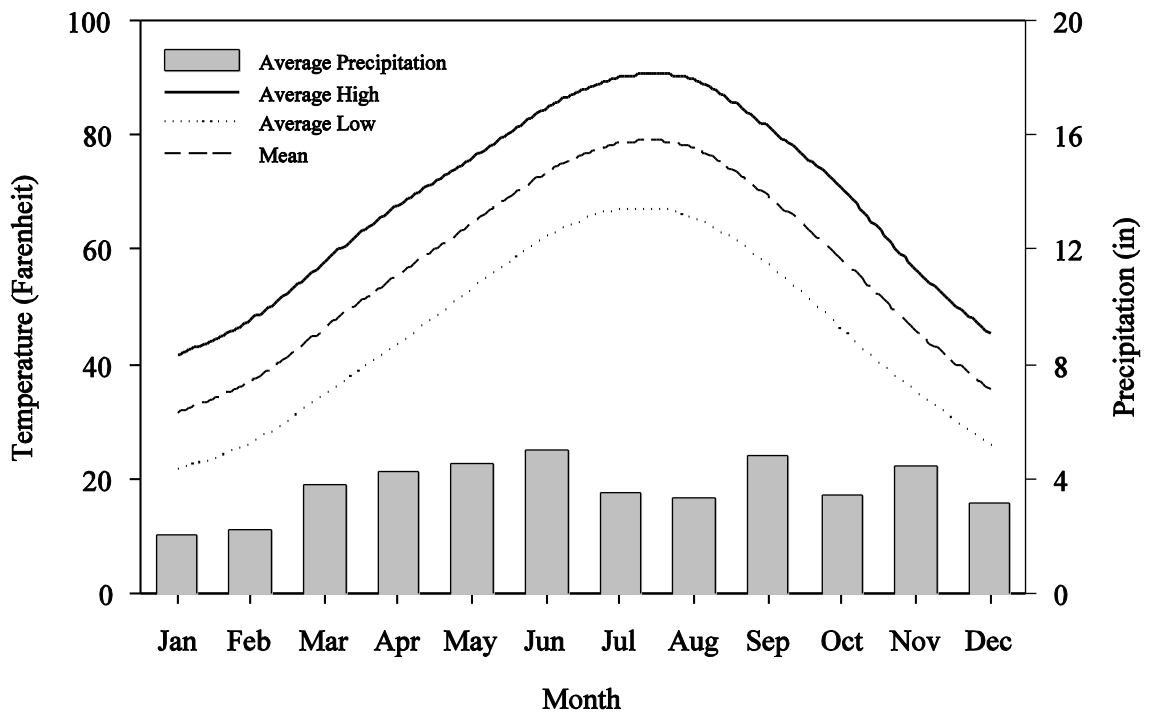


Figure 5. Monthly average temperatures and precipitation. Data recorded at the Springfield-Branson National Airport between 1971 and 2000 (Midwestern Regional Climate Center, 2009).

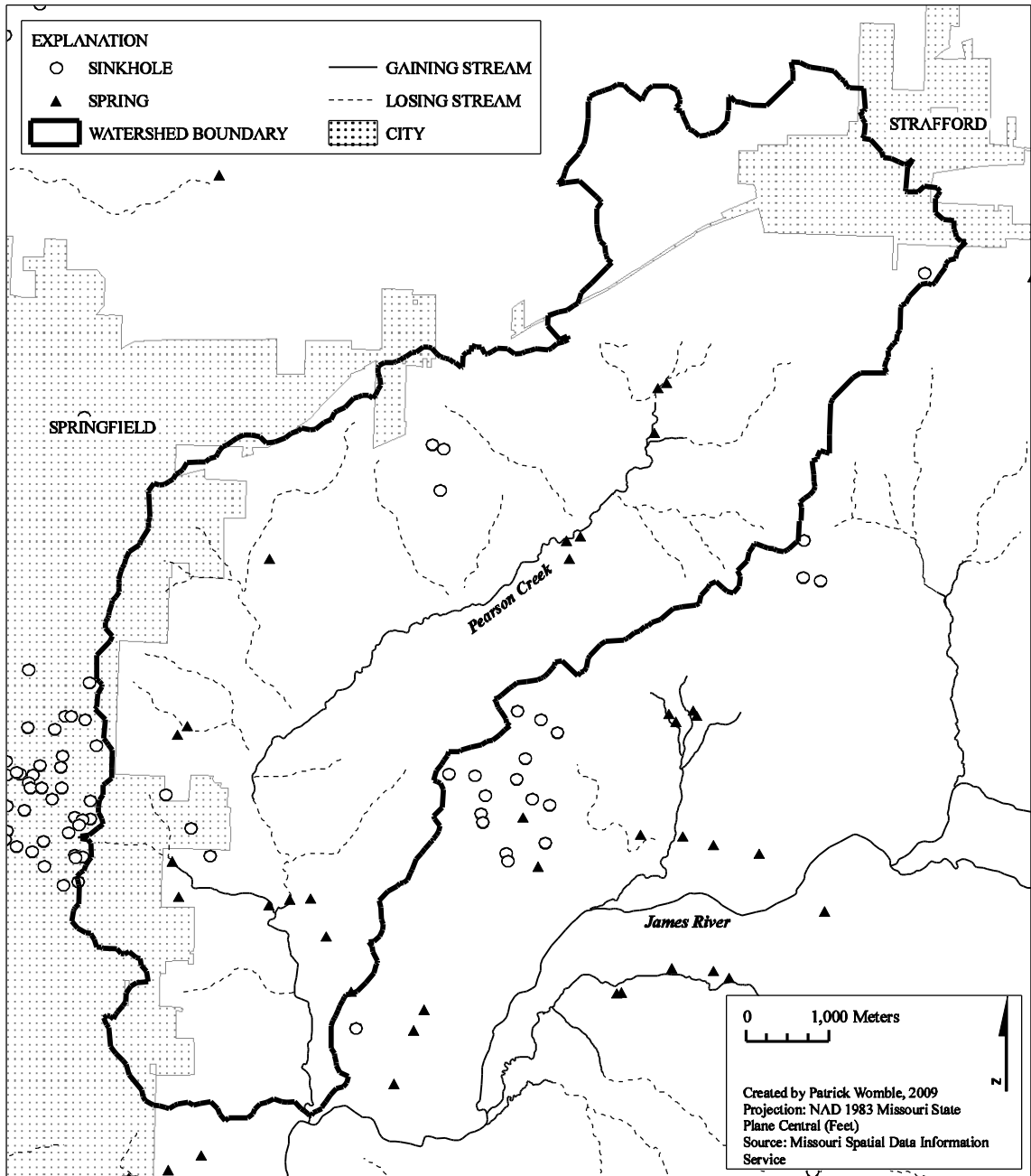


Figure 6. Karst features in Pearson Creek watershed.

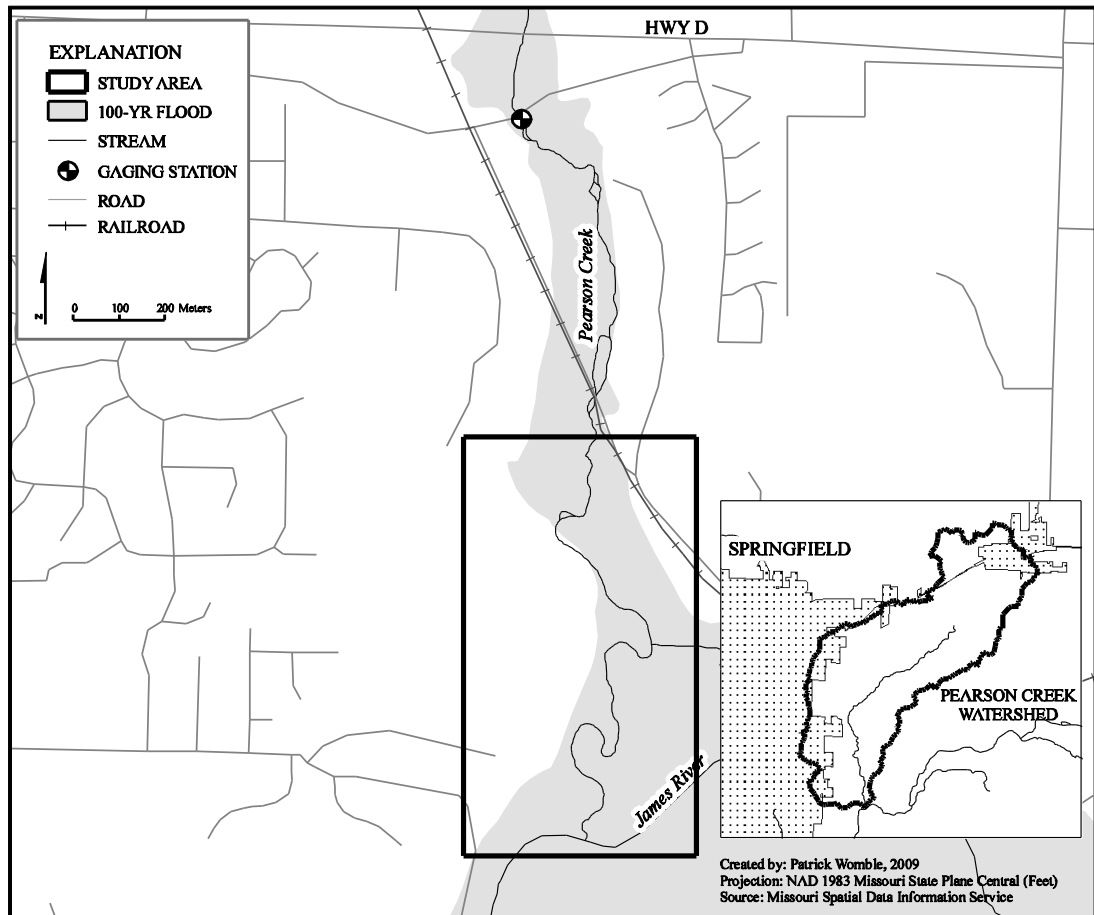


Figure 7. Location of USGS gaging station and 100-year flood.



Table 3. Annual discharge statistics from USGS gage 07050690 located upstream of the study area (USGS, 2008).

| Period of Record | Mean Q (cfs) | Max Q (cfs) | Percentile             |                        |                        |
|------------------|--------------|-------------|------------------------|------------------------|------------------------|
|                  |              |             | 10 <sup>th</sup> (cfs) | 50 <sup>th</sup> (cfs) | 90 <sup>th</sup> (cfs) |
| 1999-2008        | 24.0         | 2,980       | 52                     | 9.4                    | 2.4                    |

Springfield grew rapidly during the late 1800s and early 1900s. Land clearing practices in the Ozarks began as early as the 1830s (Rafferty, 1980), significantly altering upland and lowland environments. Grazing is currently the dominant form of land use in the watershed and urbanization is occurring in the most southern portion.

**Land Use Change.** The presettlement vegetation in the Ozarks largely consisted of oak-hickory forests with scattered bluestem prairies (Rafferty, 1980; Rafferty, 1996). Land use and land clearing in the Ozarks began to change as settlers initiated subsistence and livestock farming. During the 1870s, subsistence farming transitioned to farming for profit (also referred to as general farming) with the invention of new technology that made farming more efficient (Rafferty, 1980). General farming continued to dominate until the 1940s when dairy farming became more profitable (Rafferty, 1980). Since the 1960s, livestock (cattle) farming has been more widespread in the Ozarks than any other form of agriculture (Rafferty, 1980). Figure 8 illustrates Rafferty's four periods of Ozarks land use related to agricultural production, number and type of livestock, and population in Greene County since settlement. One thing to note in the figure is that trends in farming production match fairly well with the four periods described by Rafferty. However, the dairy farming era in Greene County began sooner than Rafferty suggests, overlapping more with the general farming (i.e. corn and wheat). Furthermore, Rafferty does not take into account swine farming, which in Greene County was present throughout Rafferty's subsistence and general farming periods.

Each type of farming has a different amount of impact on the land surrounding it. In general, soil is more likely to be eroded during corn and wheat (row crop) farming due to the loose nature of the soil in the fields. In pastured areas, roots from grasses reduce

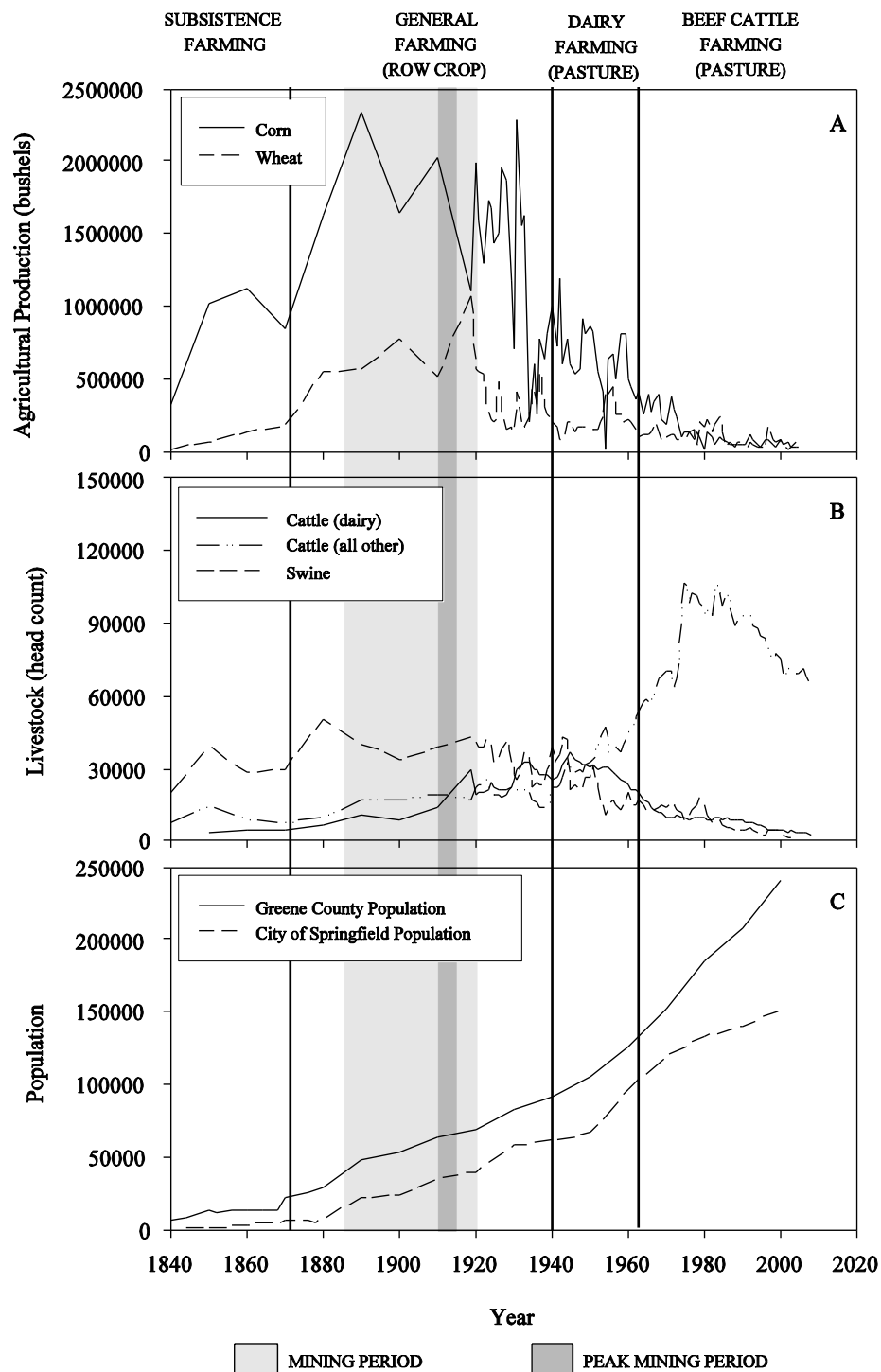


Figure 8. Land use time periods for the Ozarks and Greene County, Missouri. Four land use time periods are shown in relation to trends in agricultural production (A), livestock inventory (B), and population (C) for Greene County, Missouri (Rafferty, 1980; SGCL, 2007).

erosion by trapping and holding soil in place. Also, soil conservation practices put in place slow the erosional impact of various farming practices. Therefore, it makes sense that the amount of erosion occurring in the watershed would have decreased as land use changed from general farming (row crops) to pasture farming, and as soil conservation practices were implemented. However, the combination of swine, dairy farming, and general farming from the early 1800s to early 1900s would have likely caused accelerated hillslope erosion.

According to land use/land cover (LU/LC) data from 2003, the major LU/LC classes present in the Pearson Creek watershed are grassland (57.5%), low intensity urban (14.5%), and deciduous forest (11.4%). Less abundant LU/LC classes are impervious (5.9%), high intensity urban (0.3%), barren or sparsely vegetated (0.6%), cropland (5.1%), evergreen forest (0.3%), deciduous woody/herbaceous (4.0%), herbaceous-dominated wetland (0.1%), and open water (0.3%). The majority of the urban development is located in the southern part of the watershed near the Springfield city limits (Figure 9).

**Population.** Settlement in Greene County began in the 1820s with the arrival of frontier settlers from the east (Fairbanks and Tuck, 1915). The area became popular due to the abundance of springs and fertile soil, despite some early conflicts with the local Delaware Indians (Fairbanks and Tuck, 1915). The population of Greene County has increased at a nearly exponential rate since the mid 1800s (Figure 8C). The population of Greene County was first reported in the 1840 Census as 5,372, quadrupled by 1870 (21,549), then again doubled by 1890 (48,616), with nearly half the population (21,850) residing in the City of Springfield. The Springfield Metropolitan Statistical Area was ranked the 49<sup>th</sup> fastest growing metropolitan area in the nation after an increase in

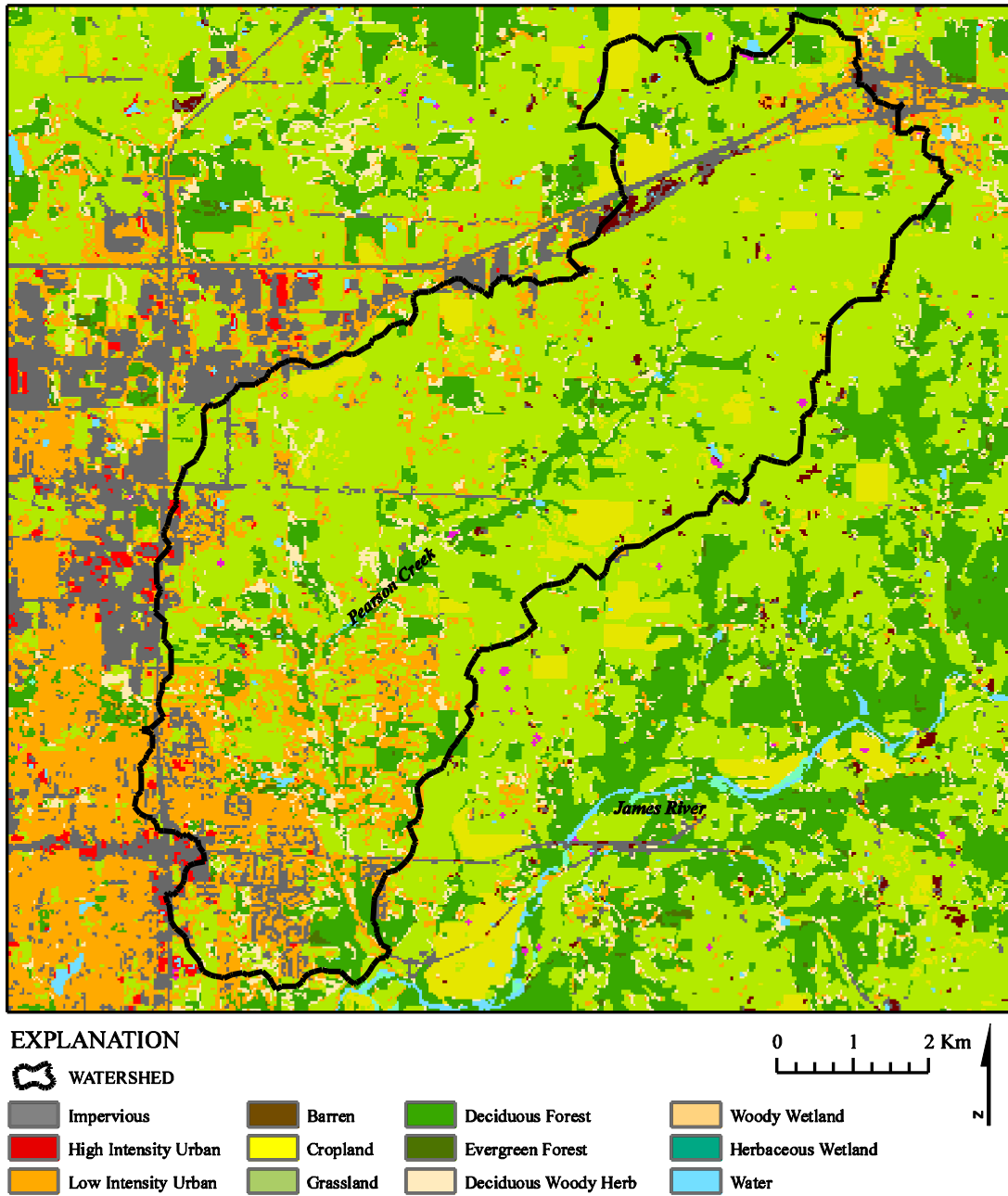


Figure 9. Land use/land cover of Pearson Creek watershed in 2005.

population from 410,619 to 420,020 between 2006 and 2007 (Census Bureau, 2008b).

### **Mining history**

Henry R. Schoolcraft was the first European explorer to document the presence of lead and zinc ore in the Pearson Creek area on an expedition through Arkansas and southern Missouri in 1819 (Rafferty, 1996). Prior to Schoolcraft's expedition, Delaware Indians and trappers in the area mined and smelted lead on a small-scale to create bullets (Rafferty, 1996). Schoolcraft described the lead as "situated in the west bank, and in the bottom of the river, as lumps of ore can be seen through the water." He also noted that the ore was "imbedded in the bank of the river in red clay."

The mines at Pearson Creek are considered to be a sub-district of the Tri-State Mining District, which is located at the junction of Missouri, Kansas, and Oklahoma. Production in the Tri-State area began in the early 1840s as small operations first in Greene (Pearson Creek Mines) and Webster Counties near Springfield, MO and later near Joplin, MO in 1848 (Figure 10; Rafferty, 1980). Large deposits near Joplin were discovered in 1854. Mining in the Tri-State District ended in 1967 and produced over 23 million tons of zinc and 650,000 tons of lead (Rafferty, 1980; Brosius and Sawin, 2001).

The first documented mining prospects near Pearson Creek and the present study area began in 1844 at the Phelps Diggings, located 1.5 km southeast of the Pearson Creek-James River confluence, not in the watershed itself (Figure 10; Fairbanks and Tuck, 1915; Rafferty, 1996). Mining stopped shortly after it began due to transportation expenses and falling lead prices caused by increased production in the Tri-State District and Old Lead Belt mines. Mining south of the James River did not recommence until 1875 (Fairbanks and Tuck, 1915). Shortly after mining at the Phelps Diggings was

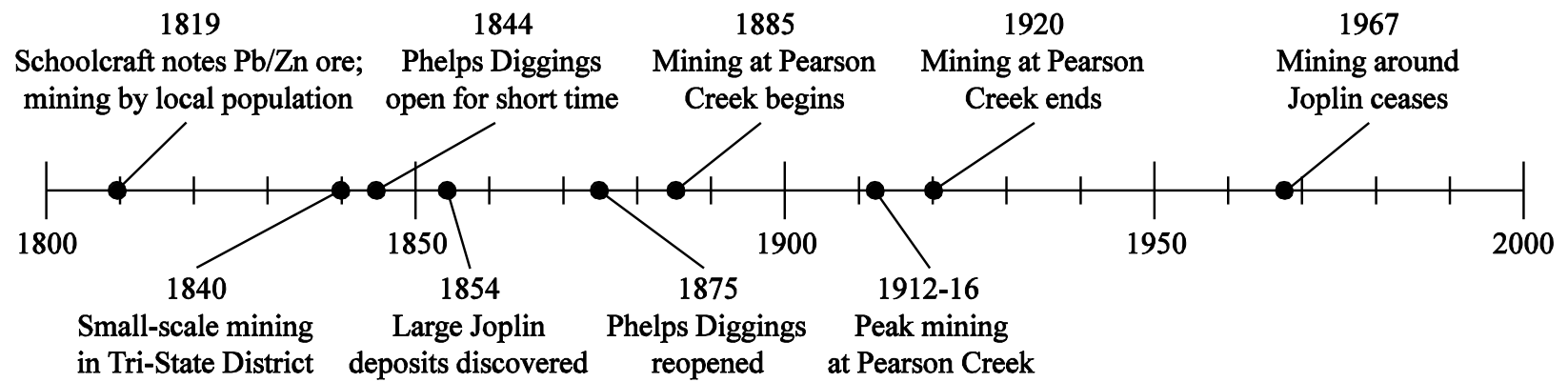


Figure 10. Timeline of mining in the Tri-State District (Fairbanks and Tuck, 1915; Rafferty, 1980; Thomson, 1986; Brosius and Sawin, 2001).

restarted, the Kershner mines (later known as the Suffolk Shafts) were opened to the northwest along the NW trending fault, still outside of the watershed (Figure 11).

Lead and zinc mining in the lower Pearson Creek valley began around 1885, reached its peak around 1912, and ended by 1920 (Figure 10; Thomson, 1986). Approximately 40 mines and prospects were situated in the area during the 35-year span (DGLS, 2008). Mining operations consisted of horizontal tunnels from the valley floor and vertical shafts sunk from the top of the ridge (Figure 12; Thomson, 1986). The mineralized zones probably originated from the injection of mineral-charged fluids along faults, during or just following the Ozark uplift (Thomson, 1986). The weathered Northview Shale, in which the ore was located, was sticky gray clay that made extraction difficult (Fairbanks and Tuck, 1915). Fairbanks and Tuck (1915) describe that due to extraction difficulties, the tailings piles contained a considerable amount of unextracted ore. Today's evidence of mine waste piles cover approximately 168 acres (0.68 km<sup>2</sup>) and are mainly located on the east side of the valley (Figure 11).



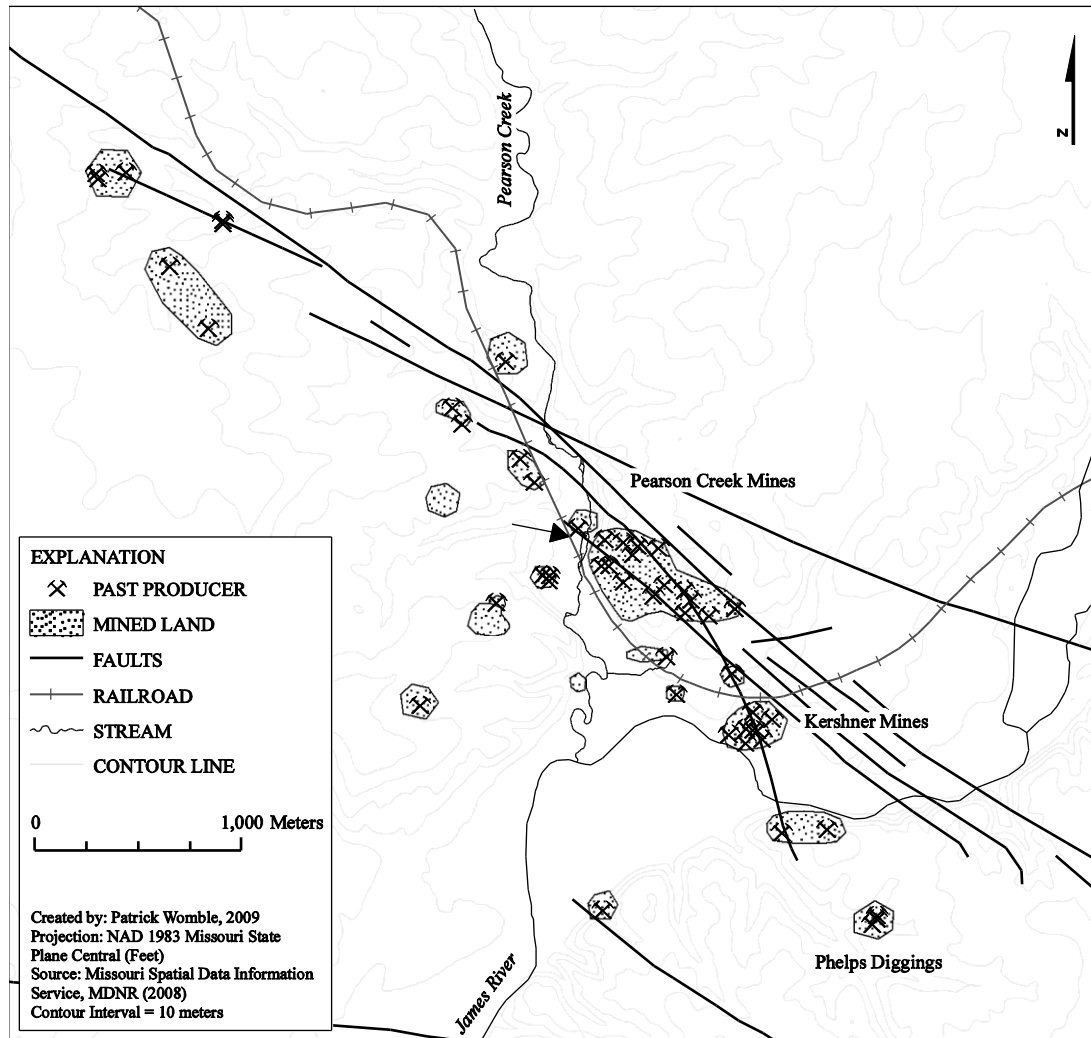
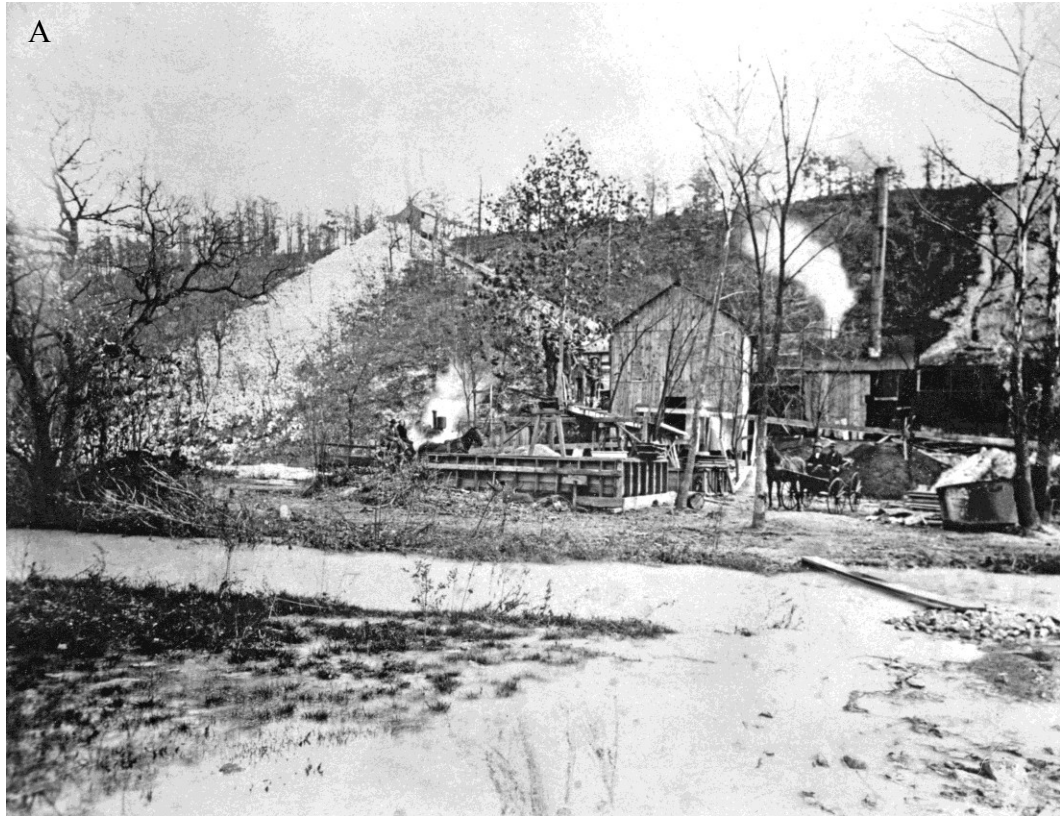


Figure 11. Mining locations in the vicinity of the study area. Note that the majority of the mines are located along the NW-trending faults. Arrow indicates the direction from which the photographs in Figure 12 were taken.



B



Figure 12. Historic photographs of a mining operation circa 1900. Historic photographs of a mining operation circa 1900. The top photograph (A) shows a close up view of a mine located just upstream of where the railroad bridge crosses Pearson Creek. Pearson Creek is in the foreground with a steam operation next to it and a mill up on the ridge in the distance. The bottom photograph (B) shows the same mining operation from a distance and highlights the extent of mining waste produced by the mine (white mound in the center of the photograph). Courtesy of the History Museum for Springfield-Greene County.

## **CHAPTER 4**

### **METHODOLOGY**

This chapter describes the field, laboratory, and data analysis methods used in this study. Field work and laboratory analysis were conducted between March of 2008 and August of 2009. In the field, cross-section locations were identified and surveyed in order to select the best sites for soil cores. Soil cores were then sampled and transported to the laboratory for geochemical analysis. Geochemical analyses included quantifying zinc concentrations; total carbon, nitrogen, and sulfur content; and grain-size. All laboratory work was completed in the Ozarks Environmental and Water Resources Institute's Geomorphology Laboratory at Missouri State University. Data was analyzed using Excel spreadsheets, SigmaPlot, Logplot, and the geographic information system ArcMap.

#### **Site Selection**

Eleven cross-valley transects along Pearson Creek were selected to sample stratigraphic and geochemical attributes of historical overbank and recent near-channel deposits (Figure 13). Transects included areas of the flood valley that would typically be inundated by flows of the 10-year flood. Sites were chosen based on the degree of disturbance at the location and the abundance of geomorphic surfaces present adjacent to the stream. Sites containing more surfaces provide a better representation of recent and historical changes in the locality of the channel. Background samples were collected from 3 different locations near the middle of the watershed and from one site outside of the Pearson Creek watershed along the James River at Turners Station (approximately

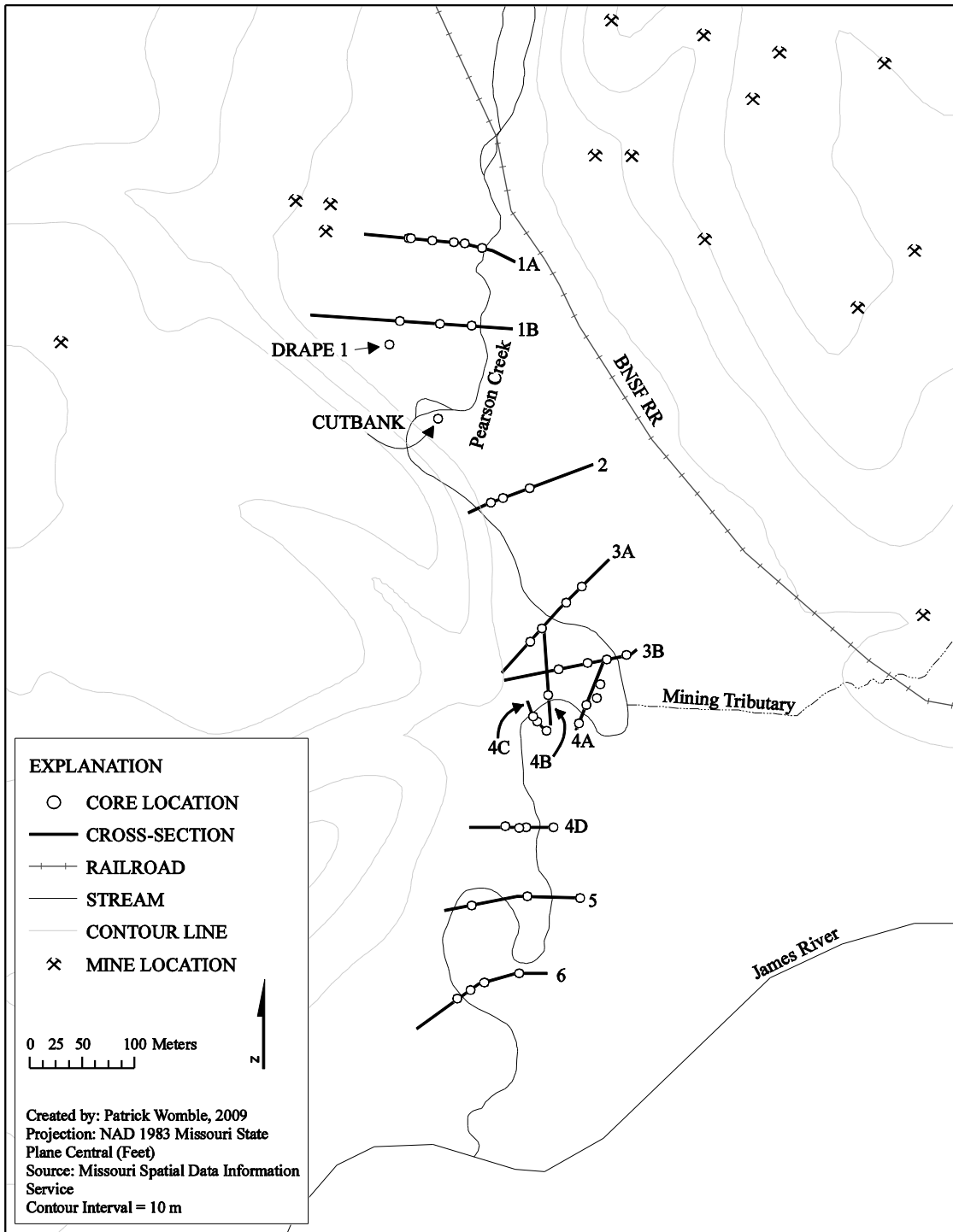


Figure 13. Cross-section and soil core locations.

6 km upstream of the confluence) to determine the natural concentrations of Zn present in alluvial sediment (Figure 14). Two tailings piles, located along a small tributary immediately downstream of Site 3B, were sampled to determine Zn concentration of one source of Zn. Active channel bed sediment in the mining tributary was also sampled to investigate the extent to which this source could be releasing contaminated sediment into Pearson Creek. Sediment collected from Pearson Creek with concentrations above the mean background level plus three times the standard deviation were considered contaminated.

### **Field Methods**

Fieldwork was mainly conducted between winter of 2008 and fall of 2009 on the property of Mr. John Hopkins, who graciously allowed unlimited access to the Pearson Creek study area. Surveying and soil sample collection were the primary field objectives. Soil samples were then prepared back in the laboratory for geochemical and grain-size analysis.

Eleven valley bottom cross-sections were surveyed using an auto-level to determine geomorphic surface elevations relative to the active channel bed. A measuring tape was stretched across the channel at each site and a stadia rod was placed along the tape on the ground surface at 2-3 meter intervals or breaks in slope. Each reading was recorded in a field book and compiled upon returning from the field. Wooden survey stakes were placed at the beginning, middle, or near the banks of the cross-sections and then surveyed with the total station during the longitudinal profile survey. This allowed lines to be drawn between the stakes in a GIS, depicting the actual location and extent of the cross-sections.

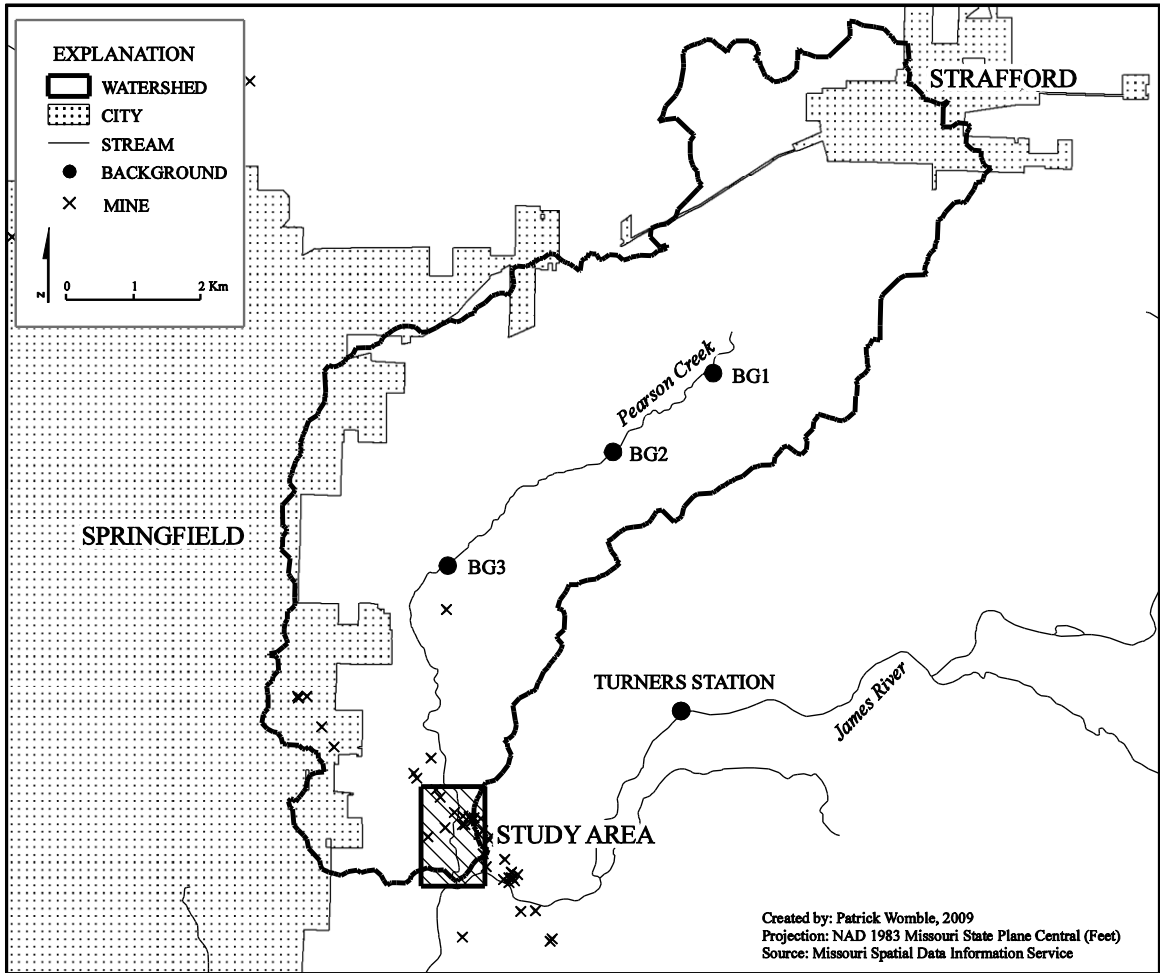


Figure 14. Background sampling locations. Nine samples were retrieved along Pearson Creek and 28 from the Turners Station site.

An Oakfield soil corer ( $\frac{3}{4}$ " dia.) was used along cross-sections to sample at 38 soil core locations to ascertain floodplain stratigraphy and geochemical makeup (Figure 13). Two different types of cores, short and long, were collected on landforms. Short cores were sampled ~1 m below the surface while long cores were sampled to refusal or where gleying began. Cores were sampled in increments based on the length of the soil tube on the Oakfield, typically 20-30 cm. After each increment was retrieved from the core hole it was placed in a soil tray and aligned with the previous increment. Once refusal was reached, or it was decided that no further sampling was necessary, soil properties such as color, texture, horizon, and horizon thickness were recorded in a field book. Core length and hole depth were measured to determine if the core was compressed during sampling and recorded in the field book as well. Soil cores were subdivided and sampled based on horizon or observable stratigraphic units such as mining sediment. Sample sizes exceeding 30 cm yielded results that were too general and were thus avoided. Samples of less than 10 cm lacked sufficient volume to be analyzed reliably with the XRF analyzer and were also avoided. Samples were then placed in labeled plastic freezer bags for transport back to the laboratory. The total number of soil samples collected for this study was 391: 9 from background sites, 377 from cross-sections, and 5 from the mining tributary and tailings piles.

Along each cross-section, depth to refusal was measured using an AMS steel tile probe. Depth to refusal was measured across different surfaces as well as in the channel bed. Depth was recorded in a field book and entered into a spreadsheet to be plotted with the cross-section.

A Trimble GeoXH handheld GPS unit was used to plot cross-sections and sample locations in a Geographic Information System (GIS). It was also used to map boundaries

of geomorphic surfaces to create the final geomorphic landform map. The GeoXH GPS was connected to a Zephyr antenna and placed next to or on top of the feature being recorded. Each of the points were allowed to collect at least 1,400 positions at one-second intervals during the longitudinal survey and at least 20 positions at one-second intervals during surface mapping. Differential correction of GPS points was done with Trimble's GPS Pathfinder Office V3.10 software using nearby base stations. The corrected data points were used to plot core locations.

### **Laboratory Methods**

All laboratory work was completed by the Ozarks Environmental and Water Resources Institute (OEWRI) Geomorphology Laboratory at Missouri State University. Samples were prepared and subject to geochemical, grain size, and organic matter analyses. These soil properties were used to identify stratigraphic sequences.

Immediately following collection, soil sample bags were opened and placed in an oven to dry at 60 C for several days. Once dried, each sample was labeled with a unique identification number, disaggregated with a mortar and pestle, and passed through a 2 mm sieve to remove any large rock fragments or organic detritus. Between each sample, the mortar, pestle, 2 mm sieve, and sieve tray were cleaned with a solution of 1% hydrochloric acid to remove any residual metals that could cross contaminate subsequent samples. Samples were then transferred into metal-free bags for analysis with the XRF.

An X-MET 3000TXS+ was used to conduct XRF analysis per instructions from the standard operating procedures (OEWRI, 2007b) on all 398 samples. Zinc, Fe, and Ca were detected in 100% of the samples, Pb in 90% of the samples, and Mn in 97% of the samples. Samples in metal-free bags were loaded into the sample holder on the XRF.



The X-MET 3000TXS+ uses a miniature X-ray tube to bombard samples with X-ray radiation for 90 seconds. The instrument reads the intensity and magnitude of fluorescence that is induced by the X-ray bombardment and then calculates element concentrations based on the number of spectral hits in the sample. Results are saved to a portable Digital assistant (PDA) for later download to a computer. For every twenty samples, two laboratory duplicates (LDs), one standard, and one bag blank were analyzed.

Grain-size analysis was performed with an LS 13-320 Laser Diffraction Particle Size Analyzer per the standard operating procedures (OEWRI, 2008) on all 398 samples. After sample preparation, a 200 mg portion of each sample was transferred into separate sample tubes. To remove organic matter, 3 ml of de-ionized water, 600  $\mu$ l of 30%  $H_2O_2$ , and 1 drop of 1% acetic acid were added. Each sample was stirred using a Daigger Vortex Genie for approximately 5 seconds, left to digest for 24 hours, and centrifuged for 3 more minutes. The liquid supernatant was removed and 3 ml of 3% sodium-hexametaphosphate was added to each sample and stirred with a Daigger Vortex Genie for approximately 5 seconds. The purpose of sodium-hexametaphosphate is to aid the disaggregation of sediment particles during sonification. Each sample was stirred again, allowed to settle for approximately 5 minutes, and loaded into the auto-prep station on the instrument where an additional sonification prepared them to be pumped into the aqueous liquid module (ALM). The ALM suspends the samples and re-circulates it through the optical system where particle size is measured. The optical system employs 126 photodetectors that record scattered light intensity patterns as it passes through the sample. The instrument is capable of detecting sediment between 0.04  $\mu$ m and 2000  $\mu$ m.

## **Data Processing and Analysis**

After returning from the field, cross-section, depth of refusal, and core profile data were transferred from the field book into a Microsoft Excel spreadsheet, which was used to compile and store all data received from each of the laboratory instruments and plot cross-sections, CNS, Zn, and grain size trends, and calculate various values such as mean depth to peak Zn, local and average sedimentation rates, and background values for Zn.

ArcMap from ESRI was used to accomplish all GIS and cartographic tasks. A 10 m DEM was used to determine the extent of the watershed via tools in the Watershed Toolbox. Base map photography was a 2005 color aerial obtained by MSU through Greene County with a resolution of 0.5 feet. Relevant map layers were downloaded from the Missouri Spatial Data Information Service (MSDIS) and the Center for Applied Research and Environmental Systems (CARES), hosted by the University of Missouri. Additional data was obtained from the United States Geological Survey (USGS) and Missouri Department of Natural Resources. The projection used for all map layers was North American Datum 1983 Missouri State Plane (Central).

Sedimentation rates for the time intervals of 1885-1912 and 1912-2008 were calculated based on the total depth of contamination and the depth to peak contamination. The depth at which Zn concentrations exceed background coincides with the year mining began (1885 at Pearson Creek) while the peak is associated with peak mining production (1912 at Pearson Creek). Everything above the peak Zn depth is representative of how much sediment has been deposited since 1912. Sedimentation rates during the mining period can be determined by calculating the depth between the first occurrence and the peak Zn concentration and dividing it by the time span those values represent, which, at

Pearson Creek, is 27 years. In the same fashion, the sedimentation rates for 1912-2008 can be calculated. One problem when calculating sedimentation rates is establishing the date of the surface. Erosional processes acting upon the surface can remove the sedimentary record and expose sediment deposited at an earlier time. If it was assumed that the date of the surface was contemporary, then the sedimentation rates calculated would be underestimates. However, it is difficult to identify the age of surficial sediment lacks tracers, which is the case at Pearson Creek. Therefore, in this study, the age of the surface was assumed to be the year 2008.

The amount of a pollutant stored in soil is calculated by multiplying the total mass of contaminated soil by the concentration of the pollutant (in percent). The mass of contaminated sediment is determined by:

$$M_{soil} = (A * Dc) * \rho_s \quad \text{Equation 1}$$

where  $A$  is the area of the contaminated soil (in square meters),  $Dc$  is the depth of the contaminated soil (in meters), and  $\rho_s$  is the bulk density of the soil (in  $\text{kg/m}^3$ ). The mass of contaminant can then extracted by:

$$M_{pollutant} = M_{soil} * C \quad \text{Equation 2}$$

where  $M_{soil}$  is the mass of contaminated soil and  $C$  is the pollutant concentration (in percent). The area of the contaminated soil was derived from a digitized map of geo-stratigraphic assemblages divided up by zone. Depth was the average thickness of contamination for cores of the same assemblage type. In this area, the bulk density is approximately  $1.3 \text{ kg/m}^3$  (Hughes, 1982). The mass of contaminated sediment (Equation 2), Zn, and Pb were calculated for each assemblage within each zone.

## Method Validation

Accuracy and precision demonstrate the limits of instrumentation and provide a way to assess the error of the method. The precision of an analysis reports on the ability of the instrument to get the same results when repeatedly analyzing a sample. In this study, this was done by analyzing lab duplicates of samples. The accuracy of an analysis reports on the instruments ability to determine the actual value of the sample. This was done by analyzing a standard with known concentrations and comparing how close the value determined by the XRF was to the value reported for the standard.

The standard used in the first three batches was supplied by the manufacturer. The reported value of Pb was not accurate and lacked some elements. Therefore the standard was changed after 9/27/2008 to a U.S. Geological Survey soil standard GXR-1. The standard and lab duplicates were used to determine the accuracy and precision of each batch of XRF analyses, which were the result of not being able to analyze all samples in one session. Therefore, the error analysis can be used to identify errors between batches that might cause the need for samples to be reanalyzed. To do this, the measured XRF results were compared to actual values by calculating the relative percent difference (RPD):

$$RPD = ((M - A)/(Average (M, A)) * 100\% \quad \text{Equation 3}$$

where  $M$  is the value measured value and  $A$  is the actual value. When determining accuracy for each batch, values determined by the XRF for the standard sample were averaged and used for  $M$  and the actual value reported in the standard by the USGS value for  $A$ . Determining precision was a two-step process: first, the RPD for each pair of duplicates was calculated ( $A$  was the initial analysis,  $M$  was the duplicate); and second,

the average of all those values was calculated and used to determine a value for the analysis batch.

The results of the accuracy and precision assessment for Zn, Pb, Fe, Mn, and Ca are provided in Table 4 and Table 5. Negative mean values in the accuracy assessment indicate that the XRF measurements were below the actual value of the standard while positive error values indicate that the measurements were above the actual value. Zn and Fe were consistently under predicted, Mn and Pb were under predicted in all but one batch, and C (excluding one batch) was consistently over predicted. Zn had the smallest range of values (-1 to -9%), indicating that it tended to be the most accurately analyzed element while Mn had the largest range (-40 to 3%), signifying that it was the most inaccurately analyzed. Fe was the most precisely analyzed element with the smallest range of values while Mn was the least precisely analyzed with the largest range of values. Steps were taken to reduce analysis error, however, several factors could influence the accuracy and precision, including: the heterogeneity of the sediment in the sample bag, void space in the sample, moisture content, insufficient sample size, and cross contamination. Since error values in both the accuracy and precision assessment (excluding Mn) were below  $\pm 20\%$ , the results were deemed acceptable and passed the quality assurance/quality control policy of the lab. However, it is reasonable for XRF values to be slightly less than those reported for the standards because standard analyses are based on total digestion while the XRF relies on surface activity only.

Table 4. X-ray fluorescence accuracy assessment. Values are the relative percent difference between the known concentrations of the standard and the concentrations determined by the XRF. Values crossed out were given incorrect standard concentration from the manufacturer of the standard and were therefore excluded. Values labeled “NA” indicate that a value from the manufacturer was not supplied for the standard or there were not enough values to calculate the average RPD for the batch.

| Date Analyzed      | Zn    | Pb               | Fe     | Mn     | Ca    |
|--------------------|-------|------------------|--------|--------|-------|
| 4/3/2008           | -2.4% | <del>82.9%</del> | -12.5% | NA     | 4.9%  |
| 9/25/2008          | -2.3% | <del>87.9%</del> | NA     | NA     | 11.6% |
| 9/27/2008          | -7.8% | <del>87.9%</del> | NA     | NA     | -1.9% |
| 12/16/2008         | -8.8% | -9.8%            | -1.1%  | -40.3% | 5.7%  |
| 4/16/2009          | -1.7% | -4.9%            | -2.1%  | 2.8%   | 3.7%  |
| 4/21/2009          | -2.9% | 4.5%             | -3.9%  | -16.0% | 3.6%  |
| 4/23/2009          | -5.8% | -0.3%            | -3.3%  | -23.9% | 3.3%  |
| 4/26/2009          | -4.1% | -3.1%            | -1.9%  | -10.9% | 7.3%  |
| 4/30/2009          | -2.2% | -4.3%            | -0.7%  | -23.2% | 5.1%  |
| <i>n</i> batches   | 9     | 6                | 7      | 6      | 9     |
| Mean               | -4.3% | -3.0%            | -3.7%  | -18.6% | 4.8%  |
| Median             | -1.7% | -3.8%            | -2.1%  | -19.6% | 5.0%  |
| Standard Deviation | 2.6%  | 4.8%             | 4.0%   | 14.4%  | 3.6%  |
| Mean +1 S.D.       | -1.6% | 1.8%             | 0.4%   | -4.2%  | 8.5%  |
| Mean -1 S.D.       | -6.9% | -7.9%            | -7.7%  | -33.0% | 1.2%  |

Table 5. X-ray fluorescence precision assessment. Values are the average relative percent difference for each batch between the initial analyses and the laboratory duplicate.

| Date Analyzed      | Zn     | Pb    | Fe    | Mn     | Ca     |
|--------------------|--------|-------|-------|--------|--------|
| 4/3/2008           | -0.01% | 0.01% | 0.00% | 0.01%  | 0.00%  |
| 9/25/2008          | 14.9%  | -4.7% | 1.9%  | -3.9%  | -6.6%  |
| 9/27/2008          | -2.9%  | 0.3%  | -2.4% | -9.2%  | -8.8%  |
| 12/16/2008         | 13.3%  | 5.2%  | -2.4% | -15.1% | 14.7%  |
| 4/16/2009          | 7.4%   | 2.2%  | -0.9% | -0.4%  | 3.6%   |
| 4/21/2009          | 5.3%   | -2.3% | 1.2%  | 4.8%   | 4.7%   |
| 4/23/2009          | 1.7%   | -5.3% | 2.2%  | 0.5%   | -14.4% |
| 4/26/2009          | 5.0%   | -6.6% | -0.6% | -5.4%  | -3.7%  |
| 4/30/2009          | -1.4%  | -2.3% | -2.1% | -5.2%  | 3.7%   |
| <i>n</i> batches   | 9      | 9     | 9     | 9      | 9      |
| Mean               | 4.8%   | -1.5% | -0.3% | -3.8%  | -0.8%  |
| Median             | 5.0%   | -2.3% | -0.6% | -3.9%  | 0.0%   |
| Standard Deviation | 6.3%   | 3.8%  | 1.8%  | 5.9%   | 8.7%   |
| Mean +1 S.D.       | 11.1%  | 2.3%  | 1.5%  | 2.1%   | 7.9%   |
| Mean -1 S.D.       | -1.5%  | -5.3% | -2.1% | -9.7%  | -9.5%  |

## **CHAPTER 5**

### **TEXTURAL AND GEOCHEMICAL CHARACTERISTICS OF FLOODPLAIN SEDIMENT**

Results from geochemical and textural analyses are presented and discussed in this chapter. The chapter is divided into four sections: background Zn determination, floodplain sediment geochemistry, physical attributes of floodplain sediment, and distribution of Zn in floodplains. Establishing background Zn levels help to distinguish between natural and mining-enriched sediment. Sediment geochemistry will be the foundation for validating Zn as a tracer in this study. Zn-sediment relationships will be used to determine what type of sediment Zn is most associated with. Relating Zn concentrations to properties such as elevation, distance from channel, and distance downstream gives clues as to what controls Zn distribution within alluvial deposits.

#### **Background Zn Concentration**

Pearson Creek background data were used evaluate the natural geochemistry of the watershed (Figure 14). Nine samples from cutbanks along Pearson Creek upstream of the mining areas were analyzed with the XRF. These values were compared to values from 28 samples along the Upper James River upstream and out of the mining area (Figure 14). Background concentrations of Zn in Pearson Creek watershed averaged 54 ppm with a standard deviation of 14 ppm and for Turners Station along the James River averaged 40 ppm with a standard deviation of 8 ppm (Table 6). An upper limit was determined by adding 3 times the standard deviation to the mean value of the 9 Pearson Creek samples. All samples with concentrations of Zn greater than this value (97 ppm)



Table 6. Background Zn statistics from Pearson Creek, the James River near Turners Station, 7.5YR samples, and 10YR samples.

| Location                         | <i>n</i> | Mean (ppm) | Geometric Mean (ppm) | Standard Deviation (ppm) | Coefficient of Variation (%) | Mean + 3X Standard Deviation (ppm) |
|----------------------------------|----------|------------|----------------------|--------------------------|------------------------------|------------------------------------|
| Pearson Creek                    | 9        | 54         | 52                   | 14                       | 26                           | 97                                 |
| James River near Turners Station | 24       | 40         | 39                   | 8                        | 20                           | 64                                 |
| 7.5YR Samples (<97 ppm)          | 17       | 41         | 38                   | 16                       | 38                           | 88                                 |
| 10YR Samples (<97 ppm)           | 111      | 69         | 67                   | 14                       | 21                           | 111                                |

were considered to be anthropogenic-related and deposited since mining began in 1885. Results show that background sampling locations along upper Pearson Creek seem to be slightly more enriched with Zn than the James River at Turners Station. This could be from industrial inputs, urban effects, or the result of dissimilar geology between the two locations. For example, Pearson Creek has several faults in the upper part of the watershed that could contain minor deposits of Pb and Zn ore and elevate the background levels slightly (Figure 3).

In addition to comparing Pearson Creek to James River sediment, floodplain sediment samples with 7.5YR and 10YR color with concentrations below 97 ppm Zn were analyzed (see Chapter 6 for details on soil color dates). Samples with 7.5YR color were analyzed to see what background concentrations might have been between the Early and Late Holocene. Similarly, samples with 10YR color were analyzed to see what background concentrations might have been between the Late Holocene and the initiation of mining. Results show that mean background concentration between the Early and Late Holocene (41 ppm) were lower than between the Late Holocene and the initiation of mining (69 ppm) and that current mean background concentrations fall between the two (54 ppm). Higher Zn concentration in the 10YR sediment implies that some enrichment occurred during the Late Holocene. This might have been due to natural weathering processes caused by incision into the mineralized zones located along the faults, which it does in several places upstream of the study area (Figure 11). Also, the mean Zn concentration in 7.5YR sediment is similar to the mean Zn concentration along the James River. This suggests that either backflooding of the James River might have been responsible for the formation of surfaces with 7.5YR sediment or a sufficient amount of time has allowed weathering processes to leach away the Zn.

## **Floodplain Sediment Geochemistry**

Geochemical and textural data presented in this section are used to examine the magnitude of Zn, Fe, Mn, and Ca in floodplains along Lower Pearson Creek and relationships between Zn and Fe, Mn, and Ca. Metal-sediment relationships reveal how and where Zn is stored in floodplain sediments.

**Metal Concentrations.** X-ray fluorescence analysis results for Zn, Pb, Fe, Mn, and Ca are displayed in Table 7. The median Zn value indicates that in over half of the samples analyzed, Zn is present in concentrations exceeding background levels (77 ppm) and is more abundant than Pb, the other mining indicator. The large range of concentrations encompasses background (pre-mining) sediment, as well as highly contaminated mining and post-mining sediment. The source of high Ca concentrations is the limestone bedrock in the area primarily in the form of carbonate-rich mill wastes from nearby mining operations. In contrast, Fe and Mn sources are primarily related to natural chemical weathering.

**Zn-Metal Relationships.** Zinc concentrations in both contaminated and uncontaminated samples were plotted against Fe, Mn, and Ca to explore potential relationships. Due to its tendency to be highly mobile, a strong relationship with Mn might suggest that Zn is also mobile, while a strong relationship with Ca could imply that Zn is attached to tailings sediment and is relatively immobile. In contaminated and uncontaminated sediment, the vertical trend in the Fe-Zn plot (Figure 15) indicates Fe concentrations are relatively constant and that Zn is not associated with Fe. This is to be expected since Fe is not related to the mining waste sources. The same conclusion can be applicable to the vertical trend between Mn and Zn in contaminated sediment (Figure 16). However, the horizontal trend between Mn and Zn (Figure 16) in uncontaminated

Table 7. Metal concentrations in floodplain sediment along Pearson Creek.

| Element | <i>n</i> | Min<br>ppm | Percentile              |                         |                         | Max<br>ppm | Mean<br>ppm | Geometric<br>Mean<br>ppm | Standard<br>Deviation<br>ppm |
|---------|----------|------------|-------------------------|-------------------------|-------------------------|------------|-------------|--------------------------|------------------------------|
|         |          |            | 25 <sup>th</sup><br>ppm | 50 <sup>th</sup><br>ppm | 75 <sup>th</sup><br>ppm |            |             |                          |                              |
| Zn      | 382      | 18         | 72                      | 192                     | 666                     | 12,395     | 600         | 230                      | 1,151                        |
| Pb      | 347      | 11         | 25                      | 69                      | 147                     | 4,768      | 190         | 64                       | 404                          |
| Fe      | 382      | 12,683     | 16,789                  | 18,115                  | 19,540                  | 25,560     | 18,160      | 18,037                   | 2,123                        |
| Mn      | 378      | 34         | 928                     | 1,152                   | 1,288                   | 5,870      | 1,131       | 965                      | 566                          |
| Ca      | 382      | 1,107      | 3,563                   | 9,355                   | 18,794                  | 181,893    | 16,479      | 8,829                    | 23,727                       |

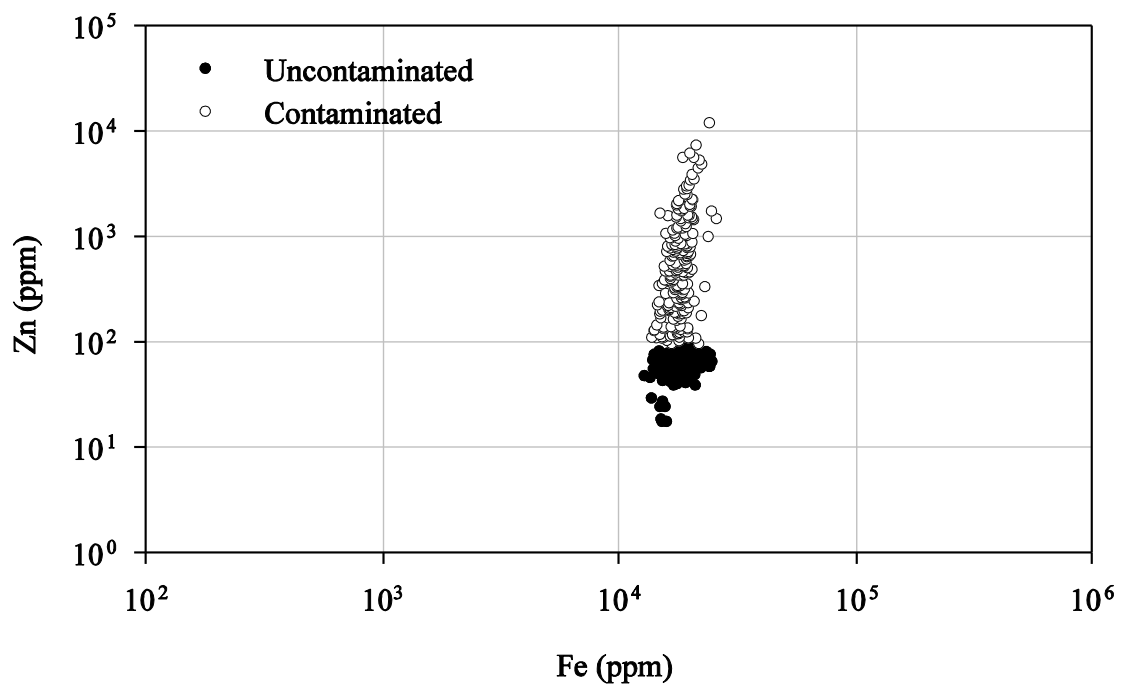


Figure 15. Zn vs. Fe in contaminated and uncontaminated sediment.

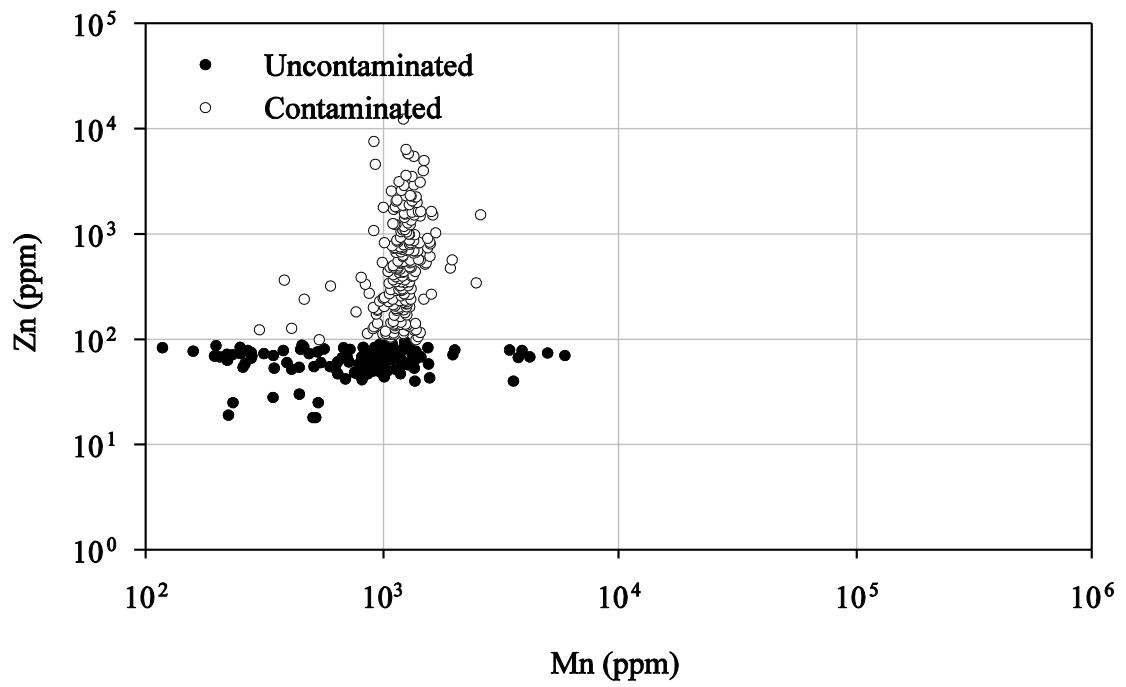


Figure 16. Zn vs. Mn in contaminated and uncontaminated sediment.

sediment can be explained by the high mobility of Mn in a saturated environment. Field observations confirm that Mn staining is present in these sediments and as coatings on gravel from lower floodplain deposits. Also, the strong positive relationship between Zn and Ca in contaminated samples demonstrates that Zn is primarily associated with calcium carbonate rock and fine sediment as sphalerite or sorbed forms (Figure 17). Uncontaminated sediment is within many of the same gleyed and deep samples that Mn depletion occurs and suggests Ca is precipitating out of Ca-rich groundwater during fluctuations in groundwater elevation (Figure 17).

### **Physical Attributes of Floodplain Sediment**

**Soil Color.** Four broad soil colors were observed at Pearson Creek: 10YR, 7.5YR, 10YR 7/1 (mining-related), and gleyed (chroma <2). Soils with 10YR color were interpreted to be A, Bw, and C horizons up to 3 m thick. Sediment in the agricultural field on the eastern side of the valley is predominantly 7.5YR with a thin 10YR plow horizon on top. Mining-related sediment (10YR7/1) is typically within 1 meter below the surface and was discovered as both laminations and layers up to 1 meter thick. Dark gray, gleyed sediment with abundant redoximorphic features (Fe and Mn staining) was present at the bottom of cores that reached or went below the water table.

Sediment color may be used for interpreting the age of the deposit in the Ozarks. Sediments along the Pomme de Terre River with characteristics similar to those found at Pearson Creek were dated using  $^{14}\text{C}$  by Brakenridge (1981). Brakenridge found that 10YR4/3 sediment in the Pippens formation, similar to the deeper 10YR sediment at Pearson Creek, was recent to late Holocene in age (0-1,600 yr B.P.). The 7.5YR sediment in the Rodgers formation, similar to the sediment found in the agricultural field

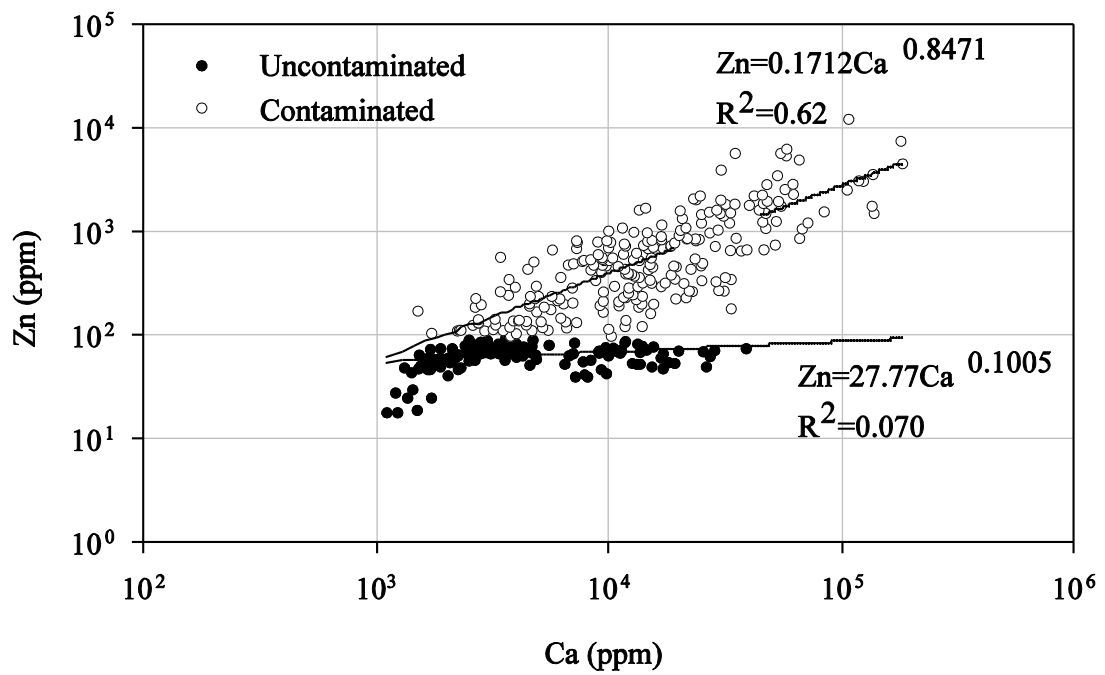


Figure 17. Zn vs. Ca in contaminated and uncontaminated sediment.



at Pearson Creek, was early to late Holocene in age (11,500-1,600 yr B.P.).

**Sediment Texture.** Sediment was classified into sand (2000-62.5 $\mu$ m), silt (62.5-3.9 $\mu$ m), and clay (<3.9 $\mu$ m). More than 92% of the samples were classified as silt loams on a USDA soil texture diagram, with loam, sandy loam, and sand making up the remainder (Figure 18). The dominance of silt loam is reasonable since all but the tailings tributary samples are located within the Cedargap and Dapue soil series, which are classified as gravely silt loam and silt loam, respectively (NRCS, 2008). Vertical profiles of sand, silt, and clay also show a general lack of sand. Three cores (Site 4A: 7 m, 25.5 m; Site 5: 0 m) display a fining upward sequence (Figure 19) and five cores (Site 2: 66 m; Site 3A: 36.4 m, 91.5 m, and 108.5 m) exhibit a slight coarsening upward trend (Figure 20). Fining upward trends are characteristic of fluvial environments where floodplains are formed by lateral and vertical accretion due to the lateral migration of the channel. Coarse material present at the base of the sequence usually represents the elevation of a previous channel bed or a bar. Floods deposit sediment on top of the bar, increasing the height of the surface. Progressively finer sediment is deposited on top of the surface as the flow required to inundate the surface increases. Coarsening upward sequences could be the result of gravel splay deposition on top of previously deposited fine-grained floodplain sediment or changes in sediment source. All remaining cores have occasional small peaks or drops in sand but are mostly uniform. The uniformity of the samples is likely the result of the system being dominated by a bi-modal source of sediment supply, either gravel or fines. Fines (silt and clay) are found in overbank deposits and back swamp environments at Sites 1A and 1B but are generally lacking in active bed sediment. The active channel bed is composed of gravel and very little sand, which is not surprising considering the surrounding geology contains only very minor amounts of sand and no

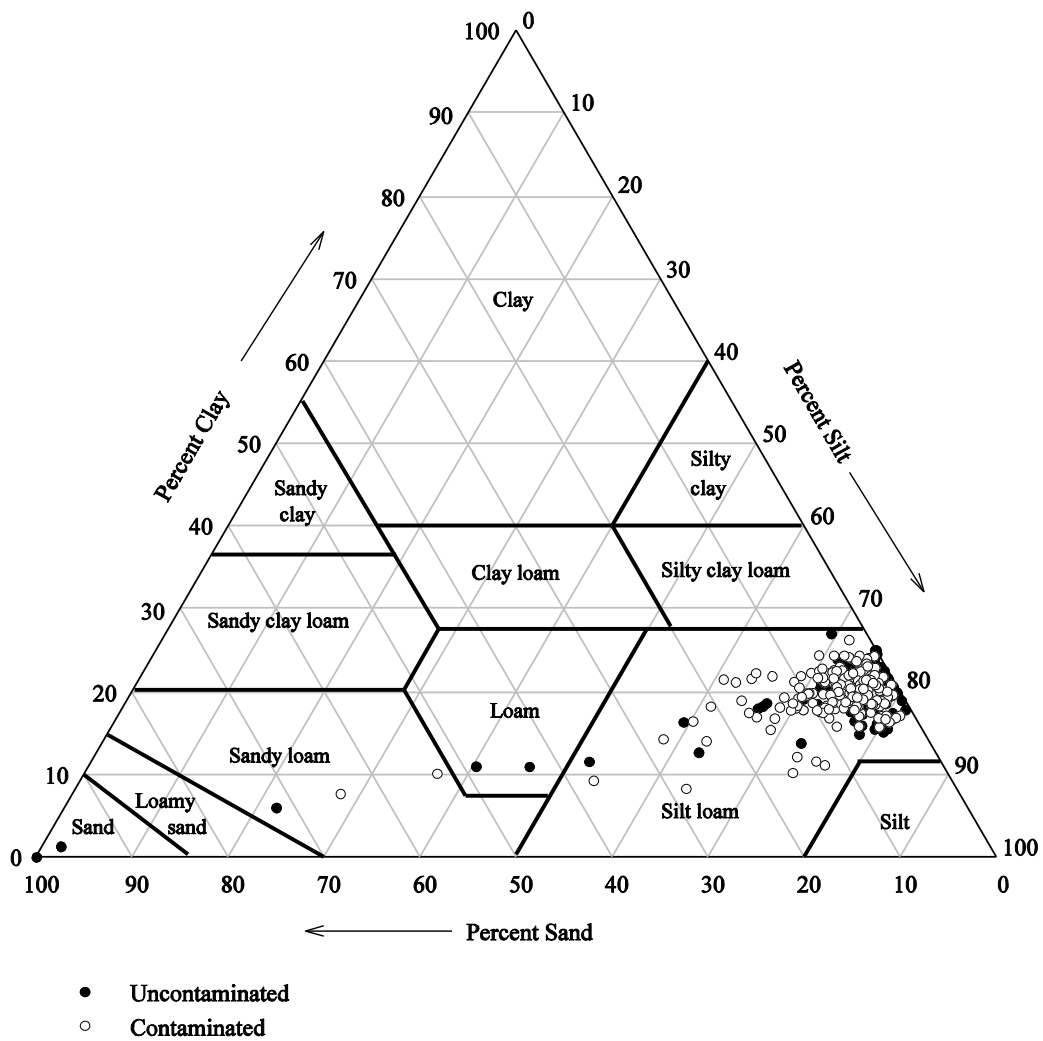


Figure 18. Sediment texture data from Pearson Creek plotted on a texture classification diagram. Modified from Figure 3-16 of Soil Survey Division Staff (1993).

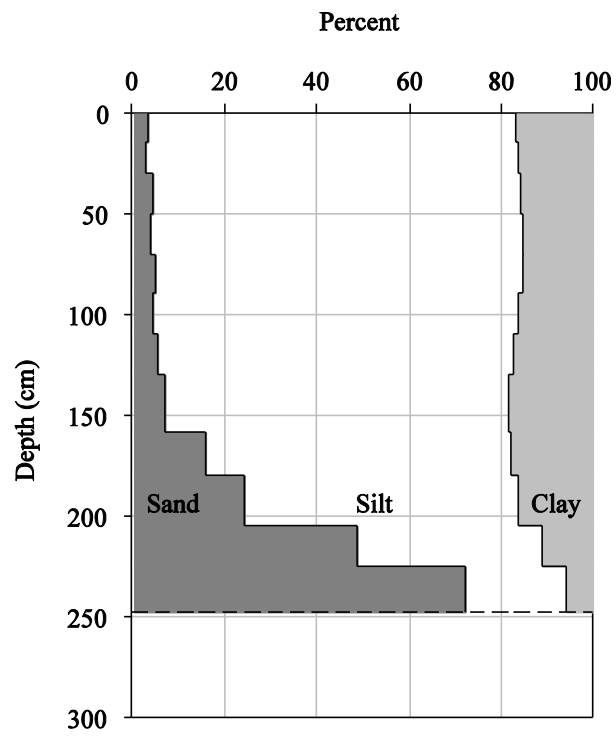


Figure 19. Example of a fining upward sequence from Site 4A at 7 m.

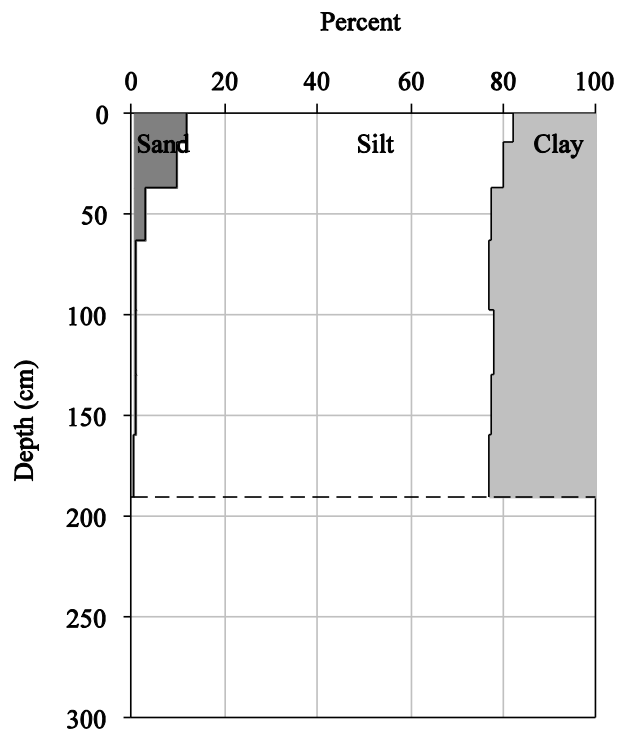


Figure 20. Example of a coarsening upward sequence from Site 3A at 108.5 m.

other significant sources of sand exist in the watershed. Therefore, the only sediment available to be deposited on floodplains during floods is silt and clay.

**Sediment-metal Relationships.** It is important to understand how Zn is associated with sediment size fractions in environmental assessments as it gives clues to source, geochemical behavior, and physical mobility (Leenaers, 1989). Zn was plotted against three grain size fractions: sand (2000 - 62.5  $\mu\text{m}$ ), silt (62.5 - 3.9  $\mu\text{m}$ ), and clay (<3.9  $\mu\text{m}$ ). Sand percent (Figure 21) in contaminated sediment has a weak positive relationship with Zn ( $R^2=0.40$ ) while contaminated silt and clay-sized sediment have no relationship with Zn (Figure 22, Figure 23). Pavlowsky (1995) found a strong relationship between Zn concentration and sand percent; however, the results presented here show a weak correlation, likely the result of waste from the milling process being introduced into the system. Consequently, it appears that in this system, grain size does not play a major role in the distribution of Zn contamination.

### **Distribution of Zn in Floodplains**

**Soil Core Trends.** In these cores, trends are interpreted from the bottom-up by noting high or low Zn concentrations. Zinc concentrations typically start below background, increase sharply, and then gradually decrease up to the surface (Figure 24). The depletion of Zn above the peak Zn concentration could be caused by sediment mixing, reduced flood inundation due to vertical accretion on banks or channel widening, a reduction of contaminated sediment influx following the cessation of mining, or any combination thereof (Knox, 1987; Lecce and Pavlowsky, 2001). The sharp increase in Zn concentration is indicative of the barrier between mining-influenced sediment and

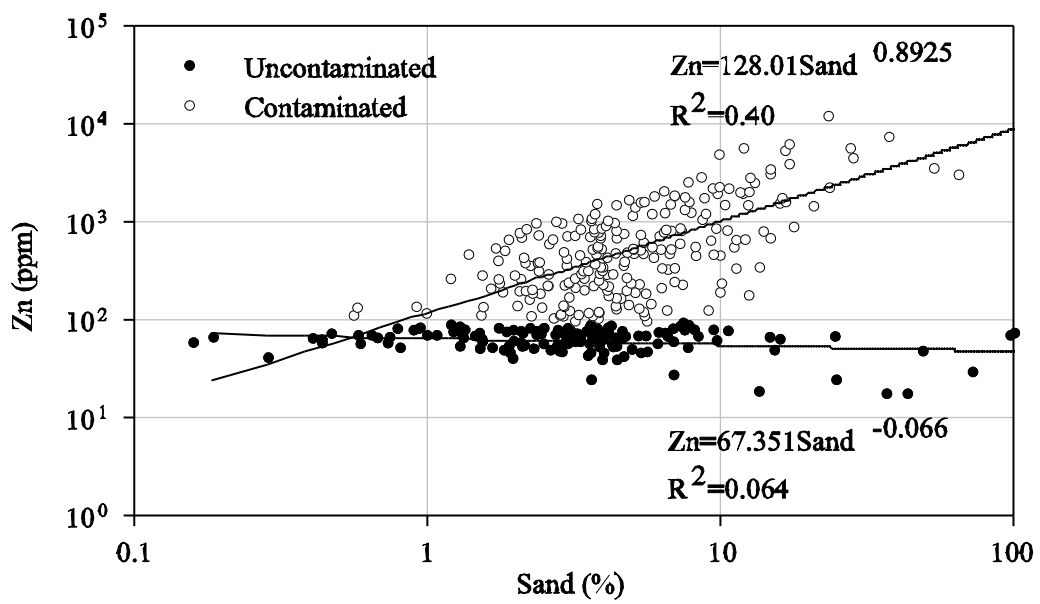


Figure 21. Zn vs. sand in contaminated and uncontaminated sediment.

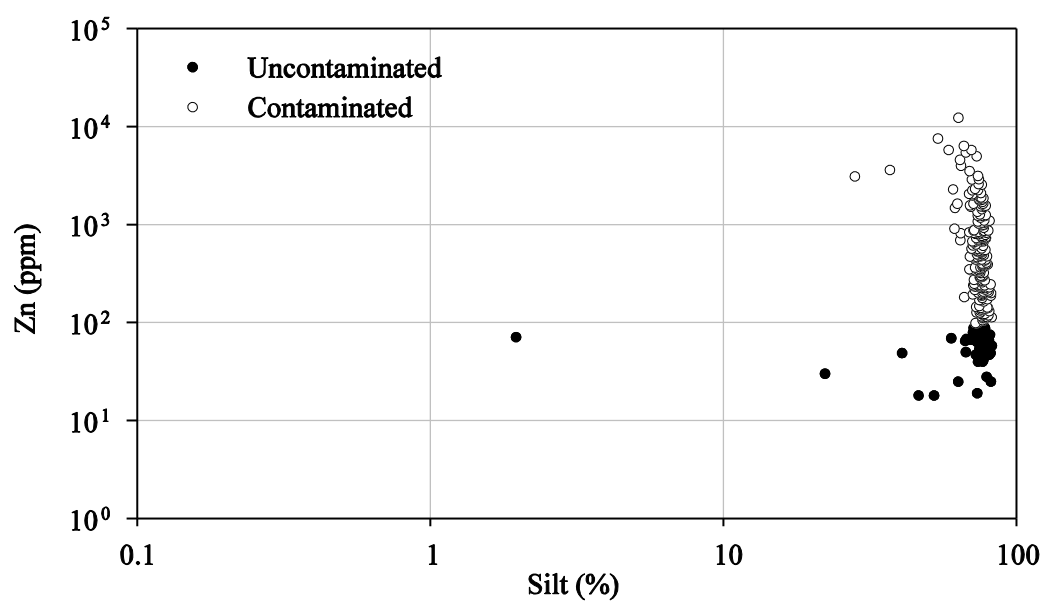


Figure 22. Zn vs. silt in contaminated and uncontaminated sediment.

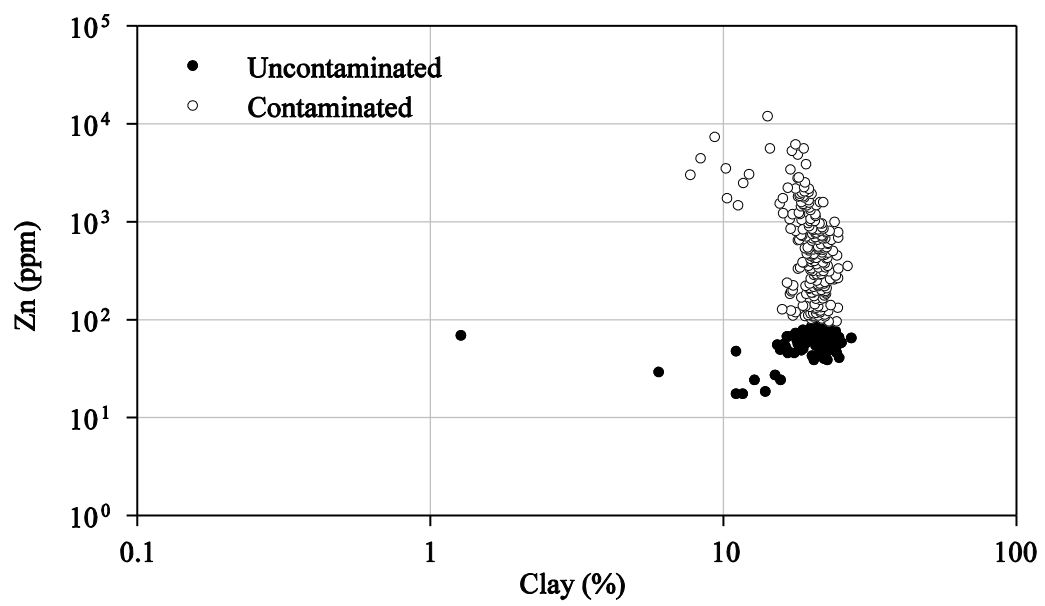


Figure 23. Zn vs. clay in contaminated and uncontaminated sediment.



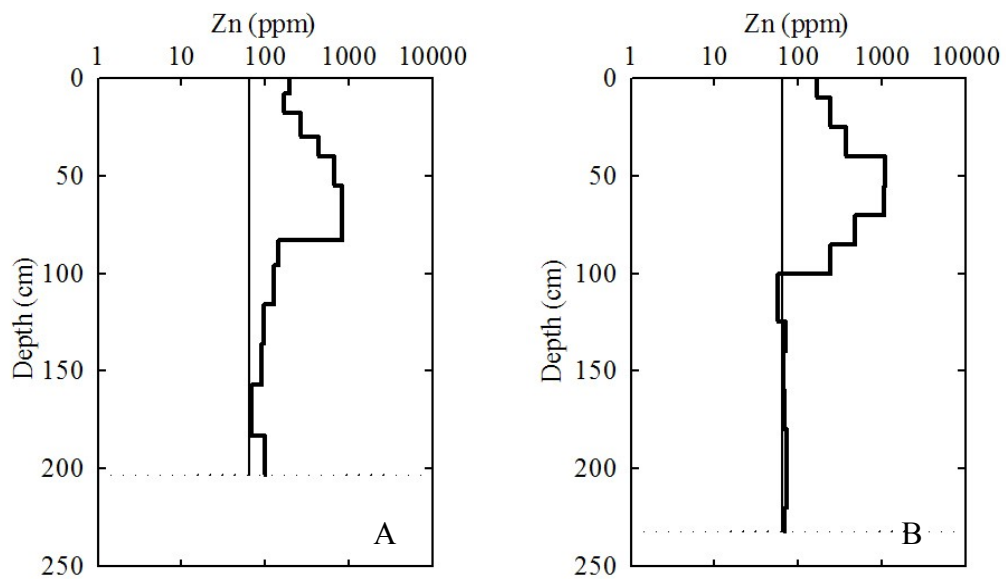


Figure 24. Example of Zn in the down-core direction. (A) Site 1B at 107 m showing possible effects of core extraction contamination and (B) Site 3A at 58 m illustrating a core with very little core extraction contamination. Zinc (thick black line), three times the standard deviation of the average background concentration (thin black line), and bottom of the core (dotted line) are shown.

sediment that was deposited prior to mining. Gradual or drawn out decreases in Zn in the down-core direction are the result of vertical migration of Zn, local inputs by mine diggings (Lecce and Pavlowsky, 2001), weathering of ore outcrops, or Oakfield contamination. Because Zn in this area is not very mobile, vertical migration of Zn would be low. Sampling errors occur for two reasons during sampling: (1) core extraction and (2) sample interval selection. During core extraction, uncontaminated samples located stratigraphically below contaminated samples must be pulled up through contaminated portions of the core hole. The Oakfield barrel is open and can scrape off contaminated soil and lead to cross-contamination. Sampling intervals were based primarily on physical differences present in the core. It is possible in cores that show very little physical differentiation that the point between the initial Zn and uncontaminated sediment was mistakenly located in the middle of the core sample. This would effectively mask the transition between contaminated and uncontaminated sediment by diluting the contaminated sediment with the uncontaminated sediment directly beneath it and result in an overall lower Zn concentration. Early mining operations would have also introduced contaminated sediment into the stream at volumes and concentrations lower than during the peak mining period since the scale of mining production was much lower. The increasing input of mine waste during larger scale mining operations would be reflected in the floodplain stratigraphy as a gradual increase of Zn up to the peak concentration. While there is no direct evidence for early small-scale mining operations in the immediate area or upstream, Schoolcraft noted that the local natives were mining galena from the stream and smelting it to make bullets when he visited in 1819 (Rafferty, 1996). Even though Pb and Zn were in the same deposits, processing techniques for Zn were not available during the early mining, so if an early

mining signal did exist, it would be expressed by a slight increase in Pb stratigraphically below the initial contamination of Zn. However, there are not any deviations of note between Pb and Zn.

The lowest concentrations of Zn were found in gleyed sediment or gravel at the bottom of cores or in the upper terrace surface. The highest concentration of Zn in the study area (12,395 ppm) was found at a cutbank exposure of an historic point bar deposit just south of Site 1B (Figure 13). The sediment at this location is very uniform in size with no discernable laminations or structure present, suggesting that it might have been deposited over a very short amount of time, perhaps one flooding event or following a tailings dam breach. The location suggests that sources upstream of the current study area were contributing significant amounts of mining-related sediment to the system.

**Valley Distribution.** As stated previously, work by others have found that Zn concentrations tend to be highest near abandoned mine sites and decrease with distance downstream (Lewin and Wolfenden, 1978; Bradley and Cox, 1986; Graf, 1996; Carlson, 1999; Lecce and Pavlowsky, 2001; Trimble, 2001). At Pearson Creek, there is a lot of variability in Zn in the downstream direction, however, a general decreasing trend can be observed with a small increase where the mining tributary enters (Figure 25). The mean of the upper 50 cm was plotted to show the concentrations of recent sediment deposits. However, there is little difference between the mean and the mean of the upper 50 cm.

**Distance from Thalweg.** Plots of Zn concentration and distance from the thalweg were used to see how much of a role distance played in the distribution of Zn across floodplains. Zinc concentrations were typically highest close to the thalweg and decreased with distance away from it (Figure 26). However, cores close to, as well as far from, the channel can have high or low Zn concentrations. This is likely because the

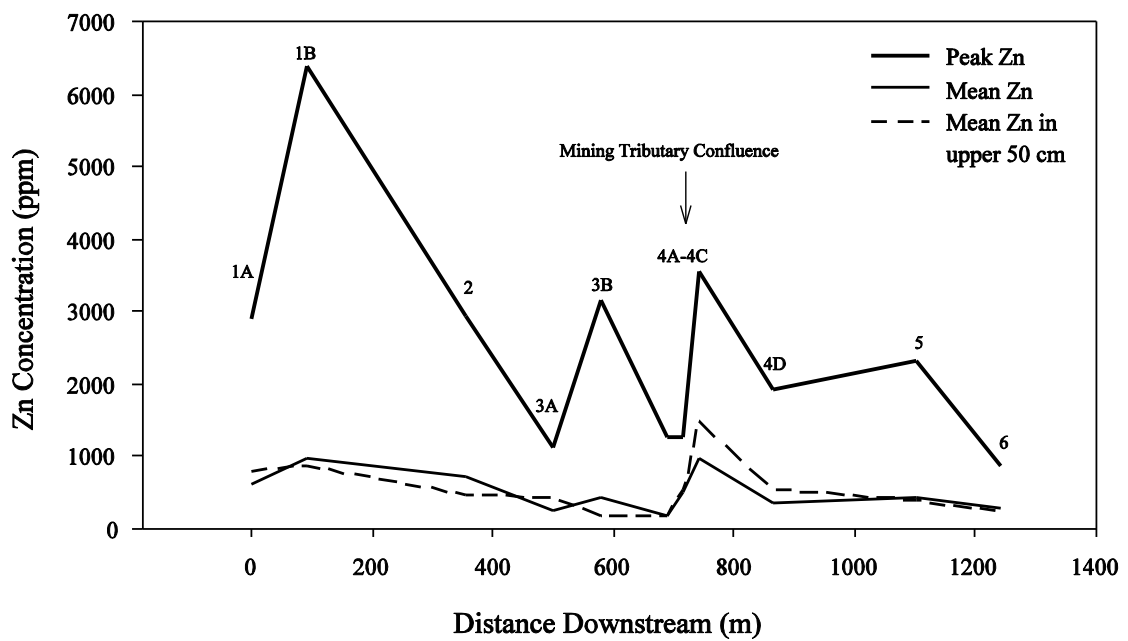


Figure 25. Downstream distribution of Zn. There is a general decrease downstream in Zn concentrations of the peak, mean, and mean in the upper 50 cm.

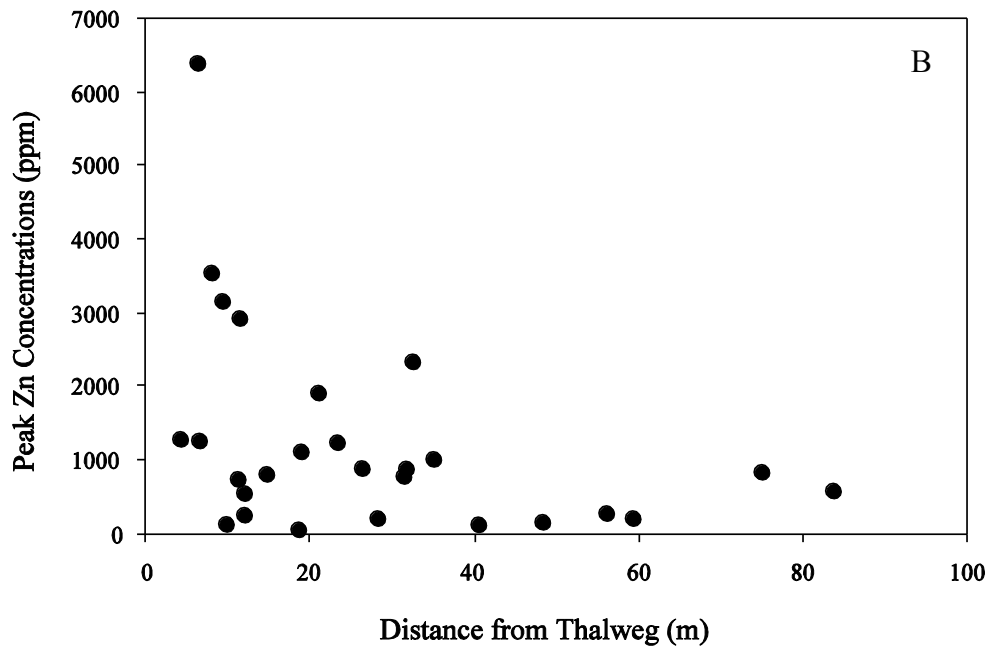
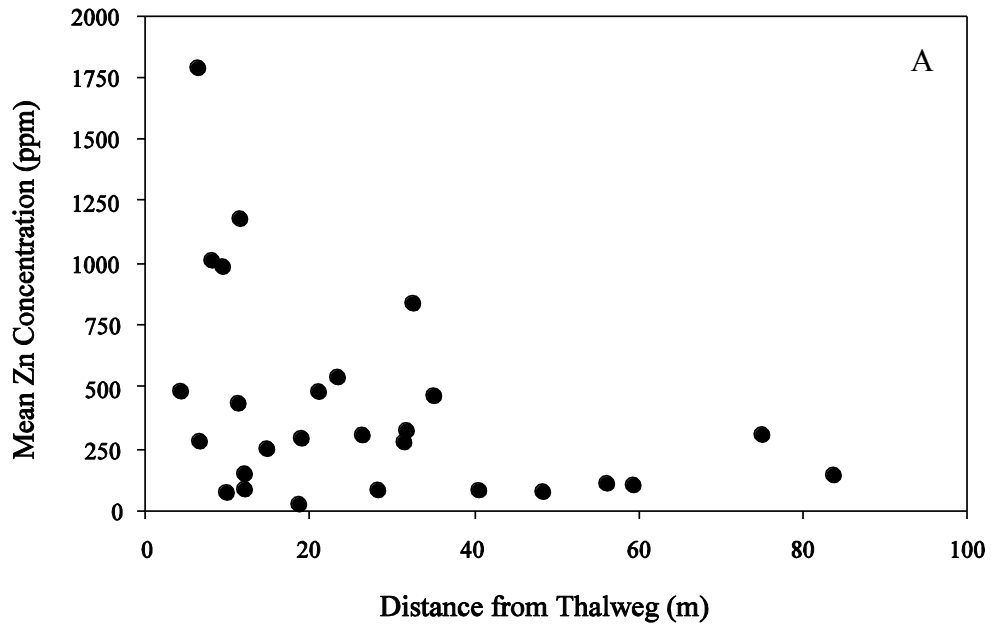


Figure 26. Zn concentration vs. distance from thalweg for the mean (A) and peak (B) Zn concentration.

spatial distribution of Zn across floodplains is complex. Brewer and Taylor (1997) suggest that the complexity is the result of patterns, rates, and timing of deposition tied to the state of the stream at different time periods. Lecce and Pavlowsky (2001) found similar results in cross-valley cores in the Blue River watershed in Wisconsin. They explained that, in addition to floodplain topography, cross-valley distribution of contaminated sediment is determined by the size of the sediment being transported, surface roughness, and available storage space (i.e. wide valleys).

**Elevation above Thalweg.** Plots of Zn elevation and surface elevation above the thalweg were used to see how much of a role surface elevation played in the distribution of Zn within floodplains. As the surface elevation increases, depths to initial and peak Zn concentrations tend to decrease (Figure 27). High surfaces close to the channel tend to have very little contamination present and, as a result, cause scattering of the data.

The distribution of Zn contamination at any location is largely determined by its distance from and elevation above the thalweg. Surface elevation above the thalweg, core distance from the thalweg, and thickness of Zn contamination data were used to create a three dimensional surface and illustrate some general trends in the data (Figure 28). The 3-D surface shown in the graph indicates that the thickest contamination is located within ~20 m of the channel and on low surfaces (<2.5 m). This trend marks recent channel migration and backfilling on the inside of meander bends to the depth of the bed. Thicker packages of contaminated sediment located between 60 and 80 m on the figure are from cores located at Sites 1A and 1B. At both of these sites, the channel is located on the east side of the valley with a low, wide surface extending to the bluff on the west side of the valley. The width of the low surface is greater in these areas than at sites where the channel is located in the center of the valley and, therefore, the distance of

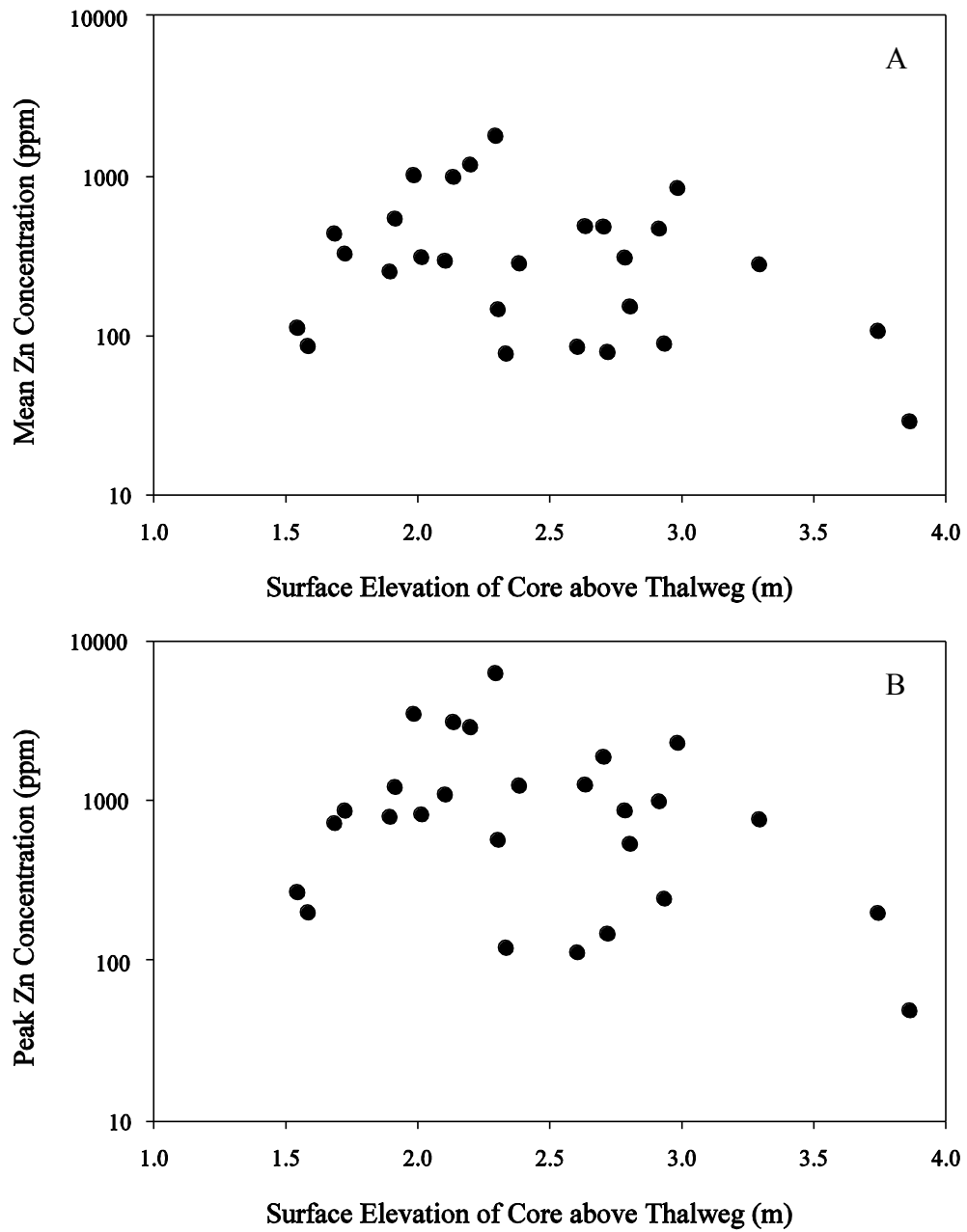


Figure 27. Zn concentration vs. elevation above thalweg for the mean (A) and peak (B) Zn concentration.

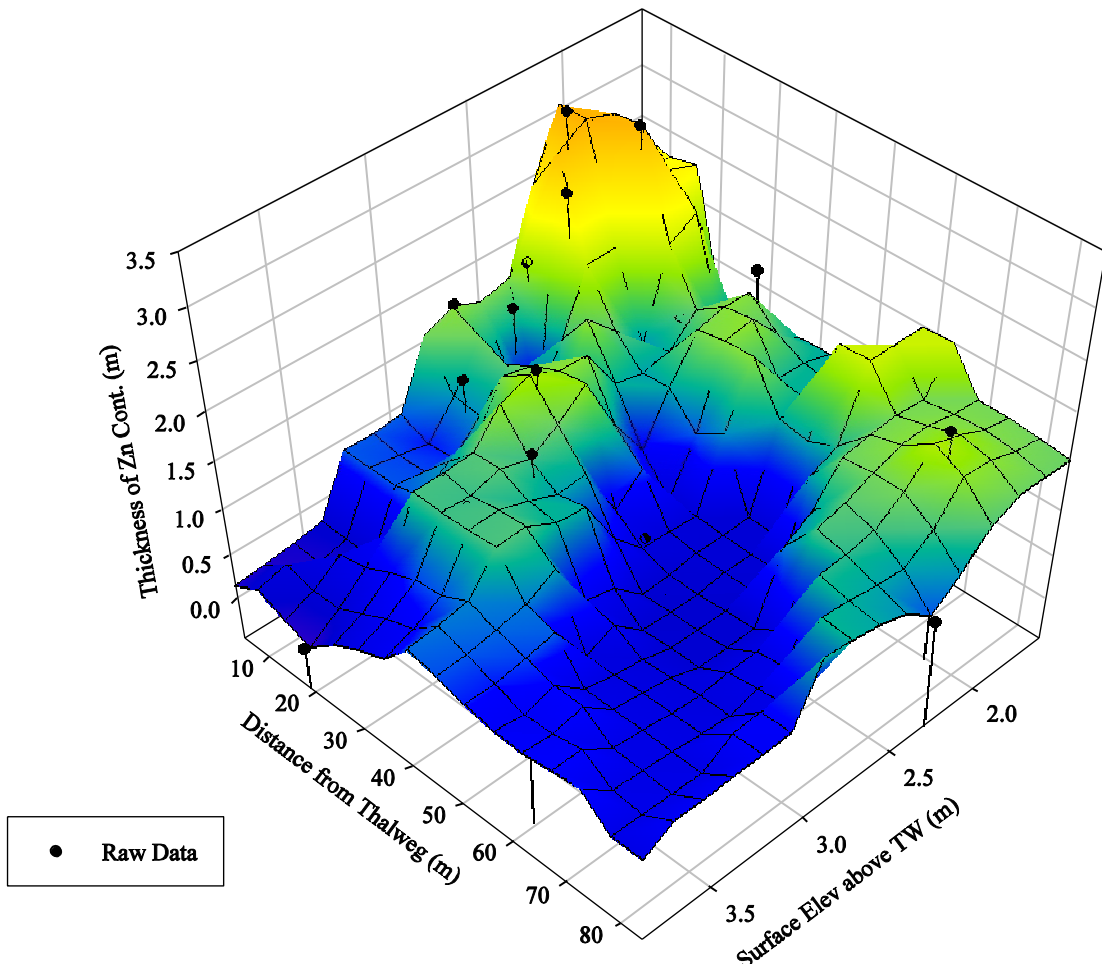


Figure 28. Thickness of Zn contamination vs. surface elevation and distance from thalweg. Generally, the thickness of Zn contamination decreases as both distance and elevation above the thalweg increases. Raw data (black dots) are plotted to illustrate some of the error caused during smoothing of the dataset.



cores on comparable surfaces at those other sites is less. The absence of data greater than 3.0 m above the thalweg and 60 m from the channel is due to the fact that low surfaces were generally limited to within 50 m of the channel. High surfaces close to the channel are due to meandering of the stream eroding into them. They contain little contaminated sediment which is likely due to the fact that their elevation above the channel prevents frequent inundation, as explained by Brewer and Taylor (1997).

**CHAPTER 6**  
**GEO-STRATIGRAPHIC ASSEMBLAGE TRENDS**  
**AND GEOMORPHIC EVOLUTION**

Data presented thus far have focused on physical, spatial, and geochemical relationships among core samples. This chapter focuses on similar comparisons among geo-stratigraphic assemblages. This chapter also provides information managers need to know to locate the contaminant (in this case Zn). First, general geomorphologic characteristics of Lower Pearson Creek are presented and used to distinguish the difference between background sites and study area sites. Second, geo-stratigraphic assemblages are presented and used to describe the across-valley and downstream distribution of Zn. Third, sedimentation rates determined from Zn stratigraphy are used to estimate the relative degree of anthropogenic impact to the watershed. Fourth, an account of the fluvial geomorphic evolution at each site will be presented. Fifth, conceptual diagrams generated from geo-stratigraphic assemblages at cross-sections are used to describe the general geomorphic evolution along lower Pearson Creek. Last, the storage of contaminated sediment, Zn, and Pb is presented in order to address the environmental impact of historical mining within the study area.

**General Geomorphology**

The valley floor of lower Pearson Creek at the study area is composed of floodplains and terraces. Agricultural fields dominate the eastern side of the valley and are dissected by a small tributary. Gravel bars are common along the channel margins of each site. Wide floodplains close to the channel are not common. Instead, in-channel

landforms are typically low, narrow surfaces and manifest themselves at sites 4D, 5, and 6. A buried sewage line trending NNE is located along the western side of the valley (Figure 29). The sewer line follows a flood chute located along the bluff on the west side of the valley between Sites 3A and 4C and crosses just downstream of Site 2. Shallow refusal depths along the flood chute are expressed in cross-sections at Sites 2, 3A, 3B, and 5 were unable to be sampled due to the aggregate put in place to protect the sewer line during installation.

### **Geo-stratigraphic Assemblages**

Geo-stratigraphic assemblage is defined as a stratigraphic arrangement of sediment with unique geochemical and physical properties related to the hydro-geomorphic conditions dominant at the time of deposition. Zinc, soil color, refusal, and floodplain geomorphology data were used to identify geo-stratigraphic assemblages. As was shown in the previous chapter, no marked down-core relationship between texture exists and its use in characterizing cores was very limited. When examining down-core relationships, three vertical stratigraphic patterns were prominent: terrace veneer, floodplain drape, and channel fill. Each core was able to be categorized into one of these three geo-stratigraphic assemblages. Terrace veneers of two different ages were found, however, both are capped with a thin layer (<50 cm) of slightly contaminated 10YR Historical sediment. The Historical 10YR on the younger terrace veneer is underlain by uncontaminated 10YR late Holocene sediment (Figure 30). The Historical 10YR on the older terrace veneer is underlain by uncontaminated 7.5YR early to middle Holocene sediment (Figure 31). Present on the older terraces is a dense 7.5YR silty layer (Bt horizon) approximately 75 to 100 cm below the surface. Data from the two types of

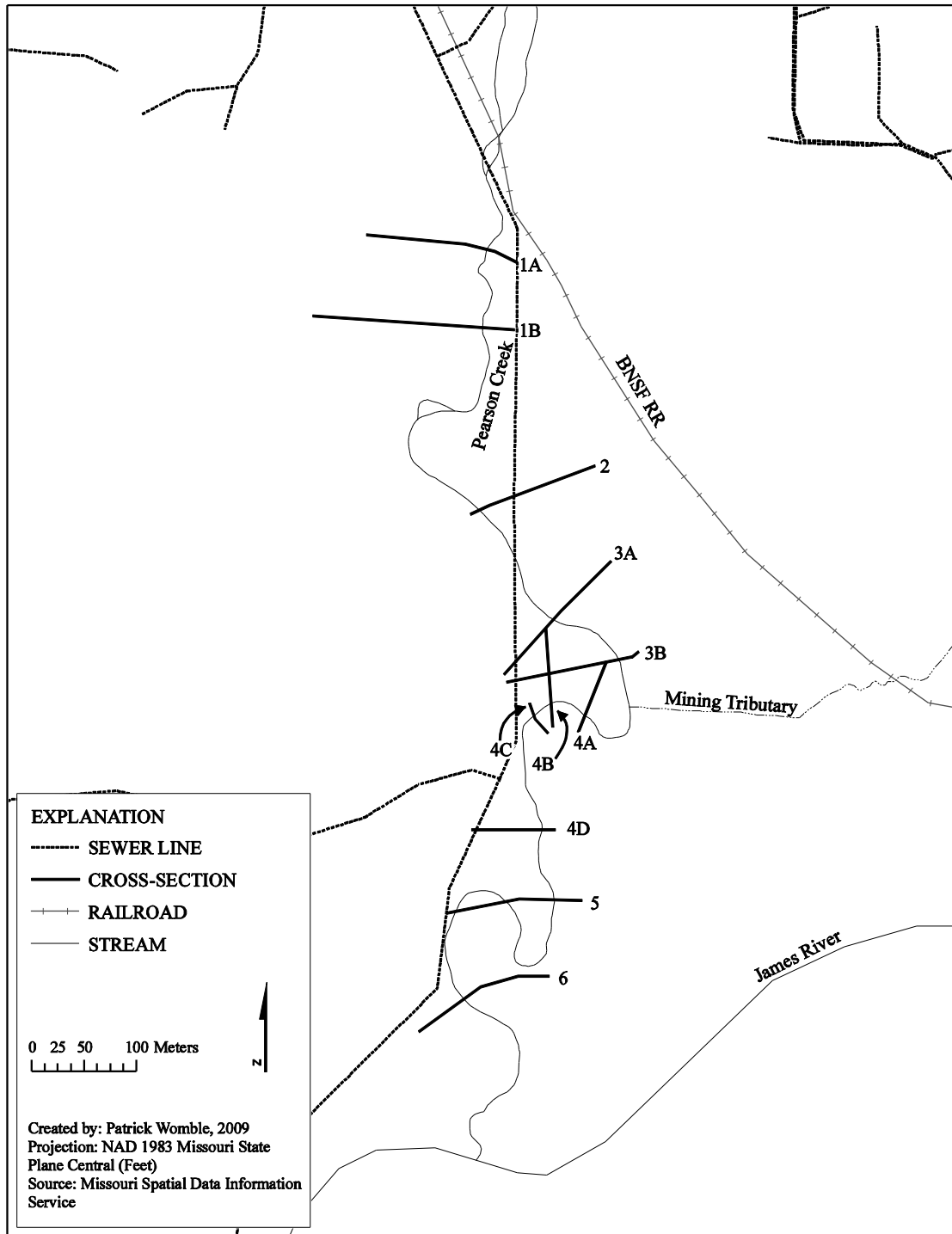



Figure 29. Location of sewer line in relation to cross-sections.

|                    |               |           |        |   |
|--------------------|---------------|-----------|--------|---|
| Project:           | Pearson Creek |           |        |  |
| Site Number:       | 4A            | Date:     | 6/2009 |   |
| Tape Distance (m): | 7             | Landform: | N/A    |   |

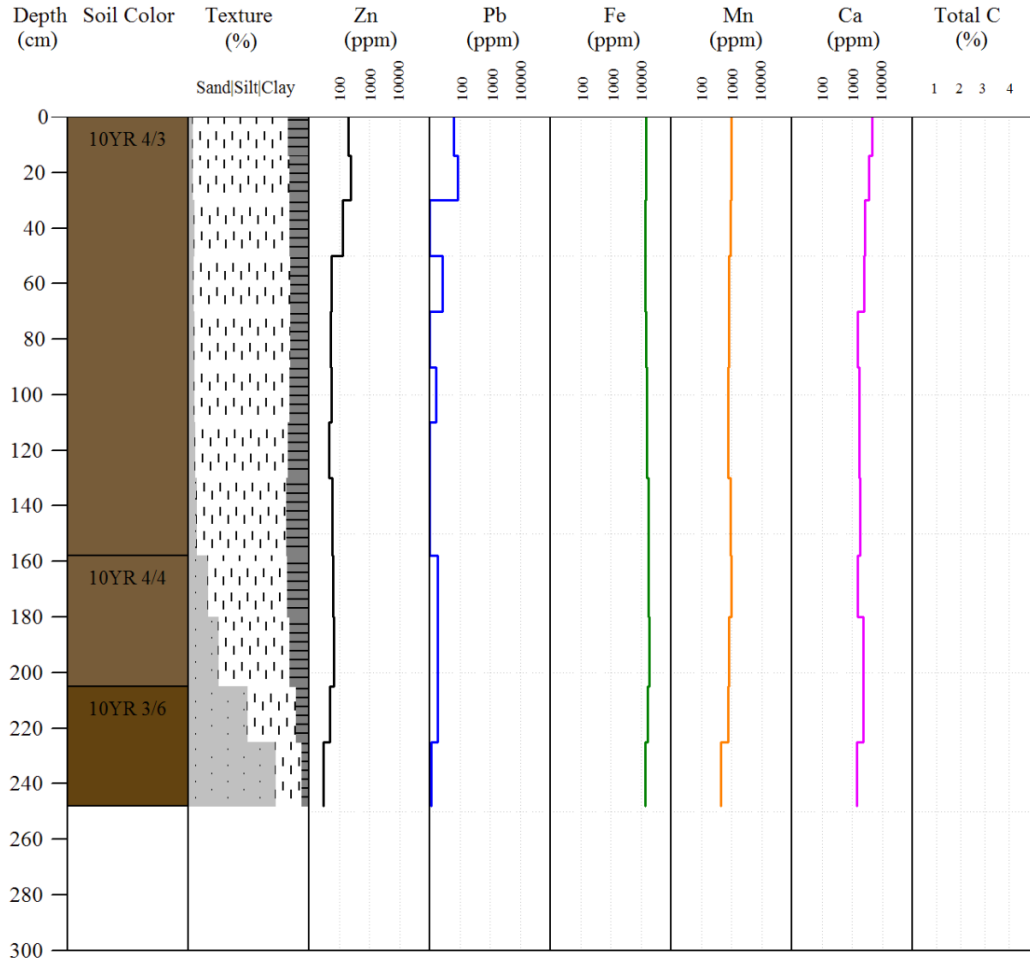


Figure 30. Stratigraphic log example of a 10YR terrace veneer assemblage at Site 4A (7 m).

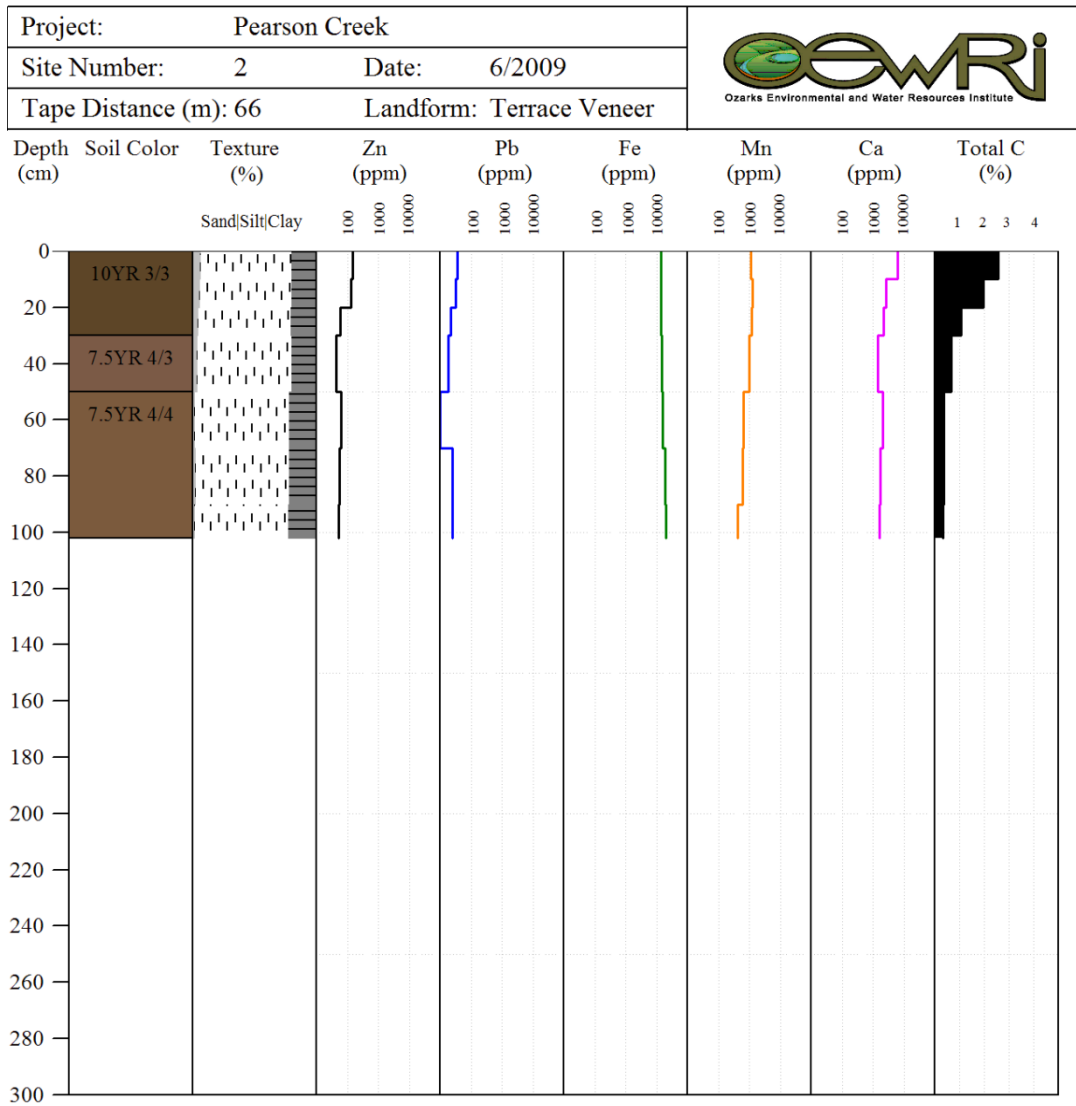


Figure 31. Stratigraphic log example of a 7.5YR terrace veneer assemblage at Site 2 (66 m).

terraces were combined to create a larger sample population due to the low number of samples collected on terraces. Floodplain drape assemblages, the most common in the study area, consist of approximately 1 m of contaminated 10YR sediment over uncontaminated 10YR sediment (Figure 32). Channel fill assemblages are fully contaminated 10YR sediment that can extend below the current stream bed and contain laminations of mining sediment approximately 1 m below the surface (Figure 33).

Trends among geo-stratigraphic assemblages were identified using Zn data as well as median distance from and elevation above the thalweg from core data. Summary statistics for Zn content in each geo-stratigraphic assemblage show that Zn concentrations in all categories are lowest in terrace veneer assemblages and highest in channel fill assemblages (Table 8; Figure 34A). Terrace veneer assemblages tend to be farthest from and highest in elevation above the channel, channel fill assemblages are closest to and lowest in elevation above the channel, and floodplain drape assemblages fall between the two (Figure 34B and Figure 34C).

The longitudinal profile of average geo-stratigraphic assemblage elevations is shown in Figure 35. As stated above, the average surface elevation of each assemblage type increases from Channel Fill to Floodplain Drape to Terrace Veneer (Figure 34C). However, the longitudinal profile shows two locations where Channel Fill assemblages are higher in elevation than Floodplain Drape assemblage. This is due to Channel Fill assemblages in these areas having levees (natural or man-made) capping them, which are at similar or slightly higher elevations than the adjacent Floodplain Drape surfaces. Also, where sites have more than one of the same types of assemblage (e.g. Site 3A), an average elevation was computed. Extremes in elevation would draw up or down the elevation of the point plotted in the longitudinal profile.

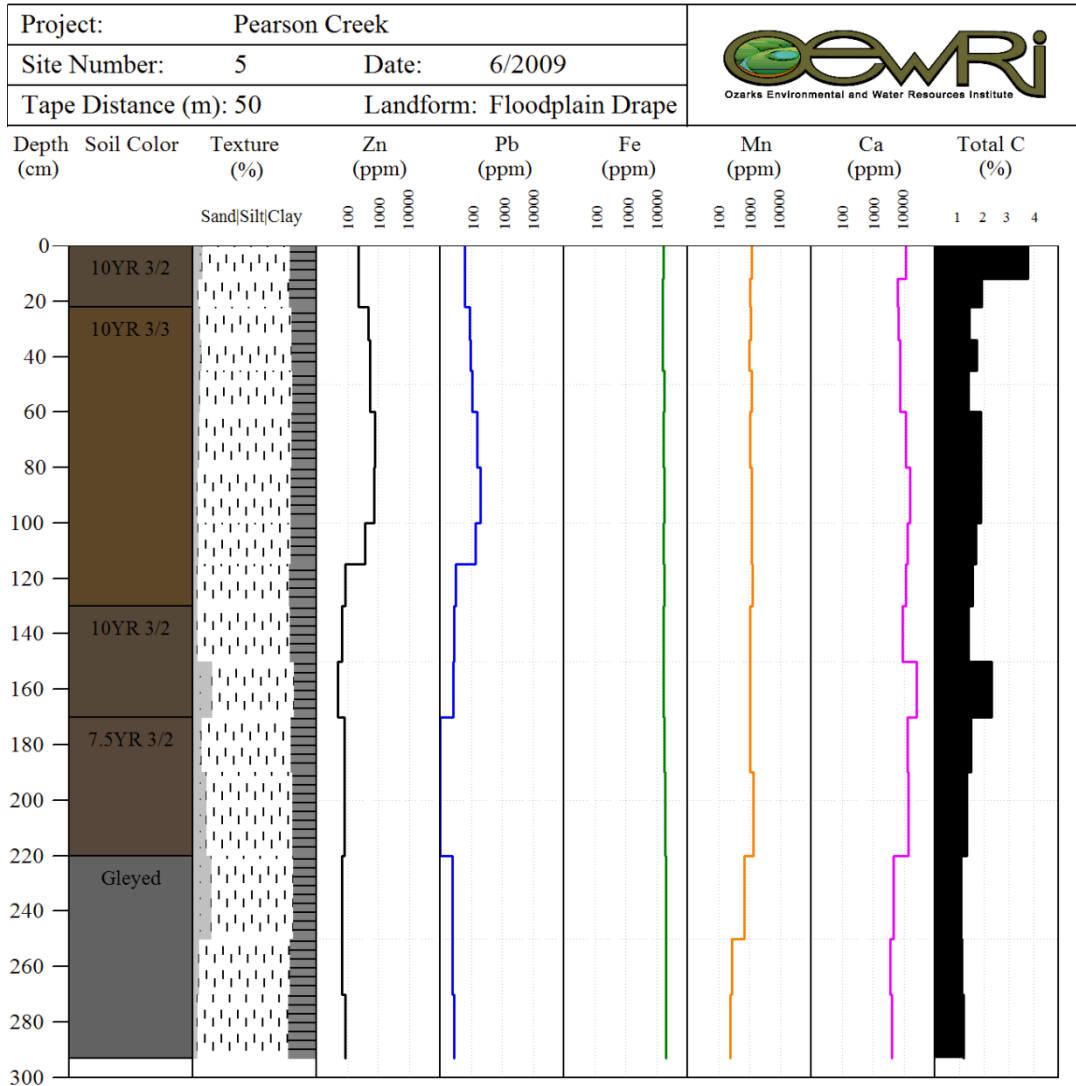


Figure 32. Stratigraphic log example of a floodplain drape assemblage at Site 5 (50 m). The bump in carbon at the contact between the 10YR and 7.5YR sediment suggests that it might be a late Holocene buried horizon.



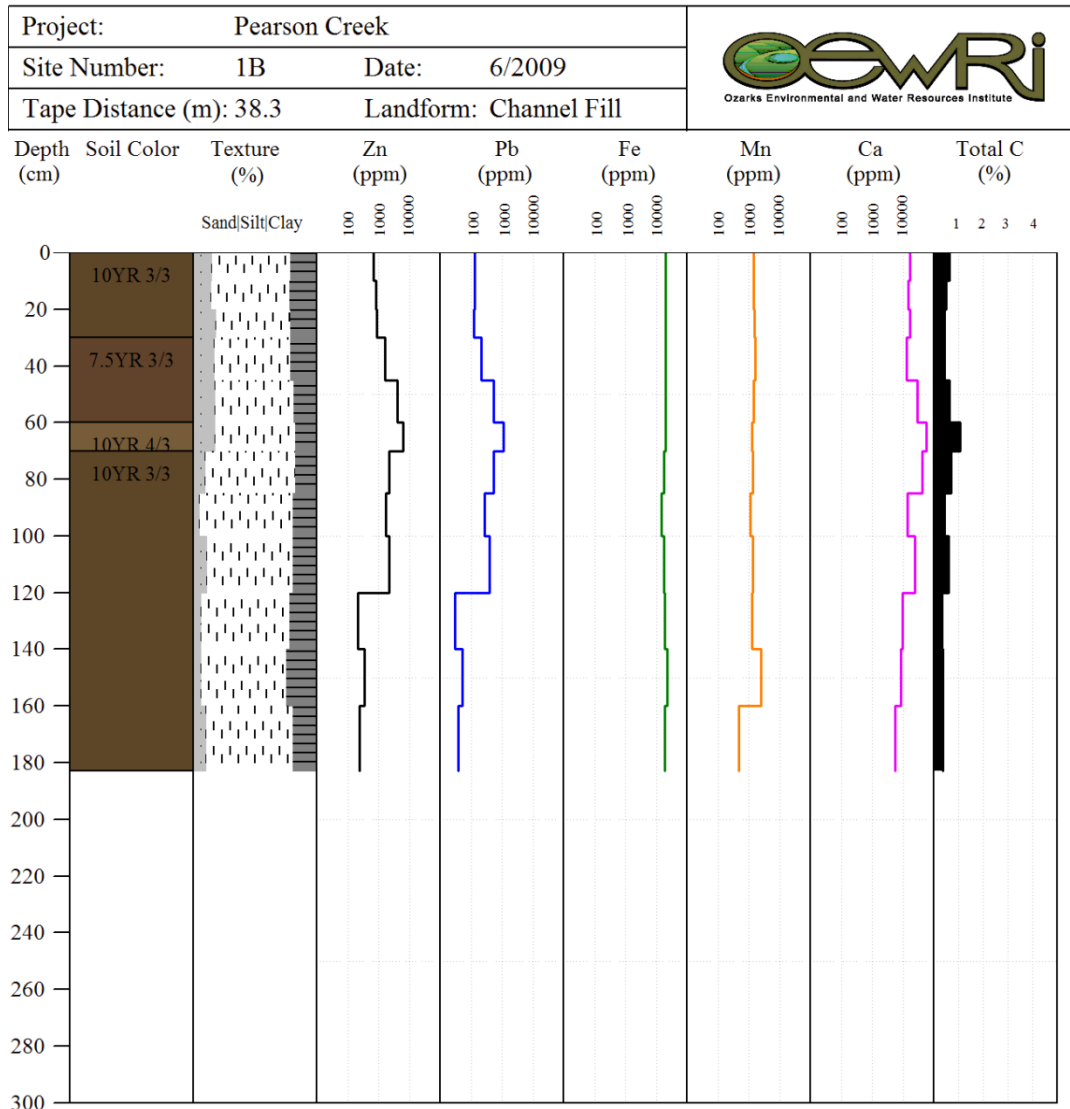


Figure 33. Stratigraphic log example of a channel fill assemblage at Site 1B (38.3 m). The 7.5YR sediment located near the top of the core could be from eroded colluvial and hillslope sources or the result of remobilized alluvial sediments. Regardless of its source, its stratigraphic position indicates that it is not Holocene in age.

Table 8. Summary statistics of Zn content for geo-stratigraphic assemblages. Note that for all statistics, values increase from terrace veneer to channel fill.

| Assemblage       | <i>n</i> | Min | Max    | Mean  | Median | Standard Deviation | Percentile |       |
|------------------|----------|-----|--------|-------|--------|--------------------|------------|-------|
|                  |          |     |        |       |        |                    | 10th       | 90th  |
| Terrace Veneer   | 71       | 18  | 270    | 85    | 66     | 55                 | 41         | 164   |
| Floodplain Drape | 77       | 40  | 3,539  | 396   | 139    | 522                | 59         | 1,036 |
| Channel Fill     | 227      | 179 | 12,395 | 1,441 | 697    | 1,910              | 288        | 3,012 |

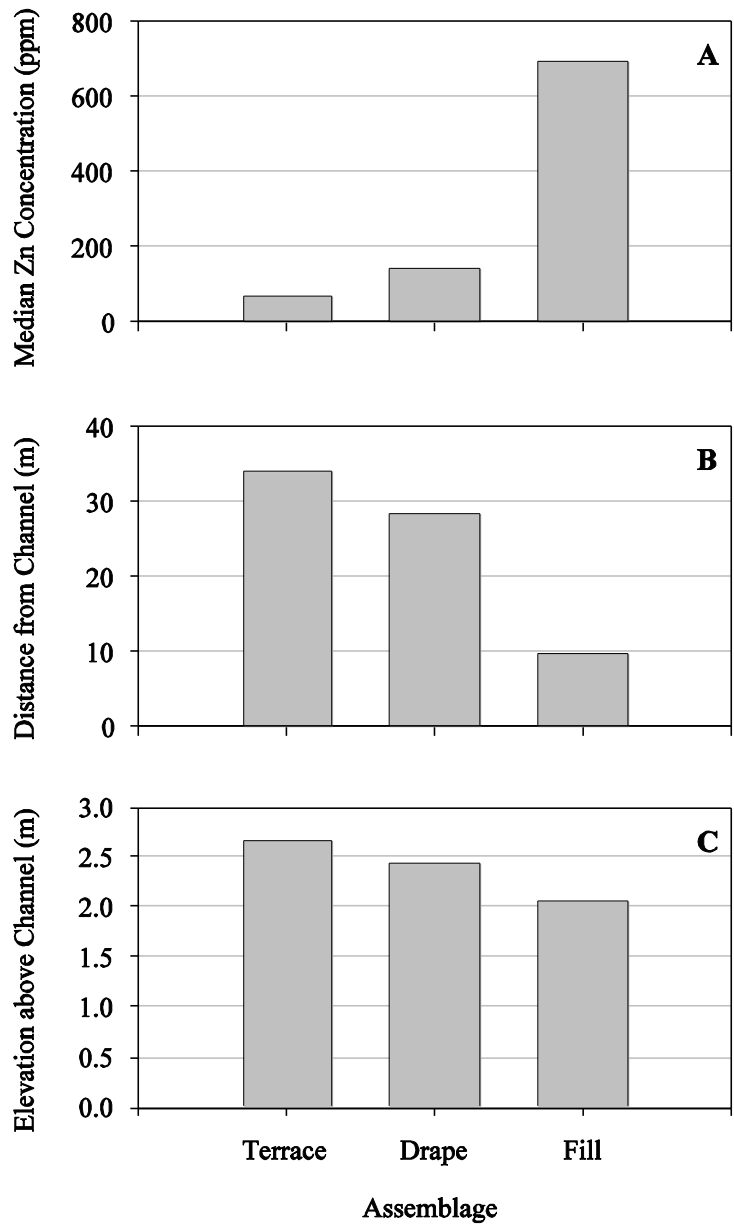


Figure 34. Spatial trends in geo-stratigraphic assemblages. (A) Median Zn concentration, (B) distance from thalweg, and (C) elevation above thalweg. Trends indicate that terrace veneer assemblages tend to have the least amount of Zn, be farthest from the channel, and be highest in elevation. Conversely, channel fill assemblages have the highest Zn concentrations, be closest to the channel, and lowest in elevation. Floodplain drape assemblage values fall between terrace veneer and channel fill values.

At Site 1A and 1B, the elevations of all three assemblages are within 0.39 m of each other. Downstream, at Site 6, the Terrace Veneer assemblage is 2.1 m higher in elevation than the Channel Fill assemblage. Differences between assemblage elevation upstream (Sites 1A and 1B) and downstream (Site 6) can be attributed to the fact that upstream sites lack the presence of active floodplains, whereas downstream, the Channel Fill assemblage is the active floodplain.

Elevation from refusal to the Terrace Veneer increases in the downstream direction (Figure 35). The wedge of sediment is likely the result of a base level rise in the James River at the confluence. An increase in the elevation of the channel bed at the confluence would force water further upstream during flooding, encouraging deposition in the transition zone where flowing water from Pearson Creek met the backflooded water of the James River. Furthermore, base level rise would decrease the slope of the channel, which promotes deposition.

### **Anthropogenic Influence on Sedimentation Rates**

Sedimentation rates, calculated using time references and sediment tracers, can provide insight into how human land use changes have affected the watershed. High sedimentation rates signify the addition of more sediment into the system. The source of which is usually from an erosional process induced by upstream land use changes such as construction, mining, logging, or agricultural practices (Lewin et al., 1977; Knox, 1977, 1987, 1989; Trimble and Lund, 1982; Magilligan, 1985; Jacobson and Primm, 1994). The mean mining-era sedimentation rate at Pearson Creek was 2.20 cm/yr and the mean post-mining sedimentation rate was 0.64 cm/yr. Mining-era sedimentation rates ranged from 0.19 cm/yr in a terrace veneer assemblage (Site 5, 0 m) to 6.30 cm/yr in a channel

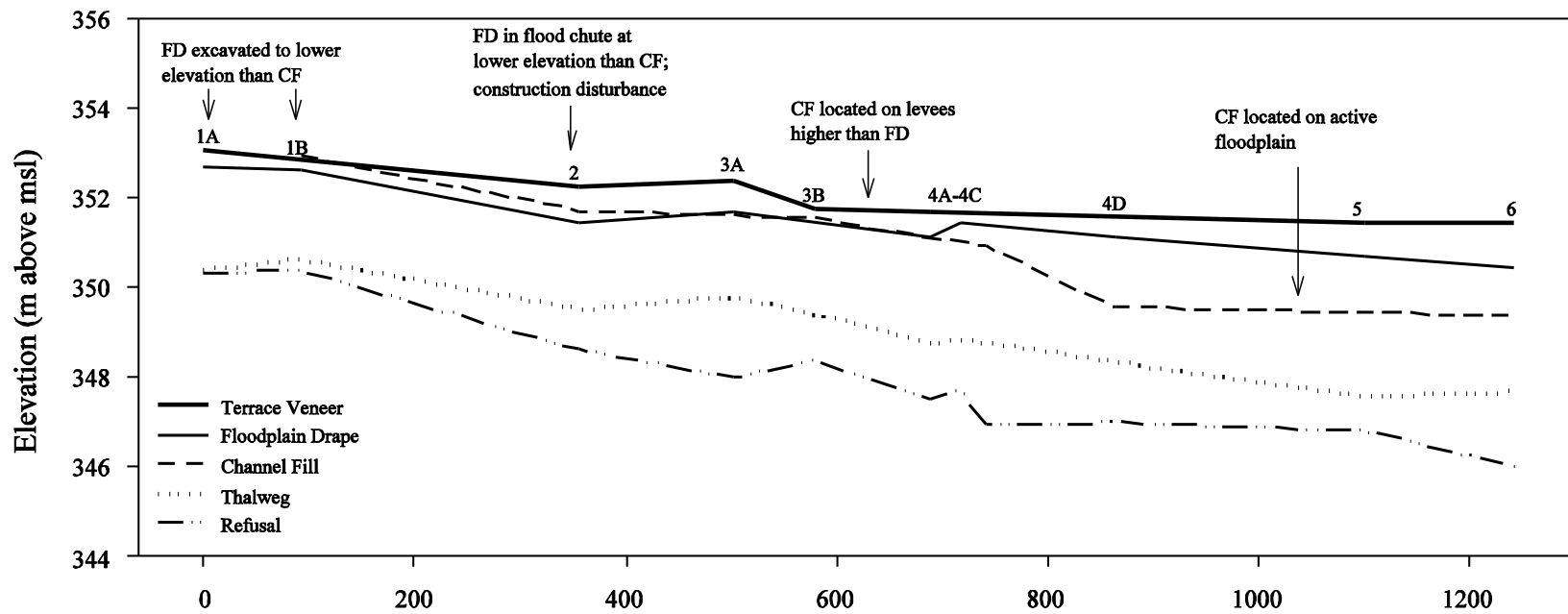


Figure 35. Longitudinal profile by geo-stratigraphic assemblage (FD= Floodplain Drape; CF= Channel Fill).

fill assemblage (Site 2, 102.9 m) (Table 9). Post-mining rates ranged from 0.05 cm/yr in a terrace veneer assemblage (Site 5, 0 m) to 2.08 cm/yr in a channel fill assemblage (Site 6, 76.1 m). Sedimentation rates by geo-stratigraphic assemblage, shown in Figure 36, also show lower post-mining sedimentation rates. Sedimentation rates are highest in channel fill assemblages and lowest in terrace assemblages.

Similar studies in the Driftless Area (Knox, 1987; Lecce and Pavlowsky, 2001), the North Carolina Piedmont (Lecce et al., 2008), and the Ozarks (Carlson, 1999) found comparable sedimentation rates and trends (Figure 37). As at Pearson Creek, every study reported lower sedimentation rates during the post-mining period. Lower post-mining sedimentation rates would point to mining operations as the cause, but this is not the case. In the Driftless Area of Wisconsin, Knox (1987) explained that mining operations have little impact on sedimentation rates and that high sedimentation rates during the mining period were more likely due to simultaneous row-crop farming practices in the region. Therefore, it is probable that a large portion of sediment considered to be contaminated does not have a purely mining-related source but is instead a combination of upland soil and mining waste erosion.

Knox (1987) and Trimble and Lund (1982) further suggest that the decrease in sedimentation following the mining period has little to do with the cessation of mining but rather land use changes and better land management practices. Mining at Pearson Creek (1885-1912) was occurring during the same time that row-crop farming (1870s-1940s) was the dominant land use class in Greene County (Figure 8). This suggests that, similar to Knox's study, sediment erosion from agricultural fields was the major source of high sedimentation rates during the mining period.

Table 9. Mining, post-mining, and total sedimentation rates per core.

| Site | Core<br>m | Mining<br>cm/yr | Post-mining<br>cm/yr | Total<br>cm/yr |
|------|-----------|-----------------|----------------------|----------------|
| 1A   | 107.5     | 1.67            | 0.31                 | 0.61           |
| 1B   | 38.3      | 4.19            | 0.73                 | 1.49           |
| 1B   | 107.0     | 4.44            | 0.86                 | 1.65           |
| 2    | 66.0      | 0.37            | 0.10                 | 0.16           |
| 2    | 91.0      | 3.96            | 0.31                 | 1.11           |
| 2    | 102.9     | 6.30            | 0.90                 | 2.08           |
| 3A   | 36.4      | 0.56            | 0.26                 | 0.33           |
| 3A   | 58.0      | 1.67            | 0.57                 | 0.81           |
| 3A   | 91.5      | 2.22            | 0.52                 | 0.89           |
| 3A   | 108.5     | 1.30            | 0.52                 | 0.69           |
| 3B   | 11.0      | 0.67            | 0.16                 | 0.27           |
| 3B   | 30.2      | 5.00            | 1.93                 | 2.60           |
| 3B   | 48.0      | 0.56            | 0.16                 | 0.24           |
| 3B   | 77.0      | 1.59            | 0.13                 | 0.45           |
| 4A   | 7.0       | 1.33            | 0.15                 | 0.41           |
| 4A   | 25.5      | 3.33            | 0.57                 | 1.18           |
| 4B   | 29.5      | 2.33            | 1.11                 | 1.38           |
| 4C   | 13.0      | 1.78            | 0.77                 | 0.99           |
| 4D   | 0.0       | 2.22            | 0.78                 | 1.10           |
| 4D   | 33.0      | 2.41            | 0.89                 | 1.22           |
| 4D   | 47.0      | 1.78            | 0.52                 | 0.80           |
| 5    | 0.0       | 0.19            | 0.05                 | 0.08           |
| 5    | 50.0      | 2.59            | 0.63                 | 1.06           |
| 5    | 103.0     | 3.22            | 0.66                 | 1.22           |
| 6    | 28.0      | 1.11            | 0.31                 | 0.49           |
| 6    | 61.0      | 2.59            | 1.25                 | 1.54           |
| 6    | 76.1      | -               | 2.08                 | 1.35           |

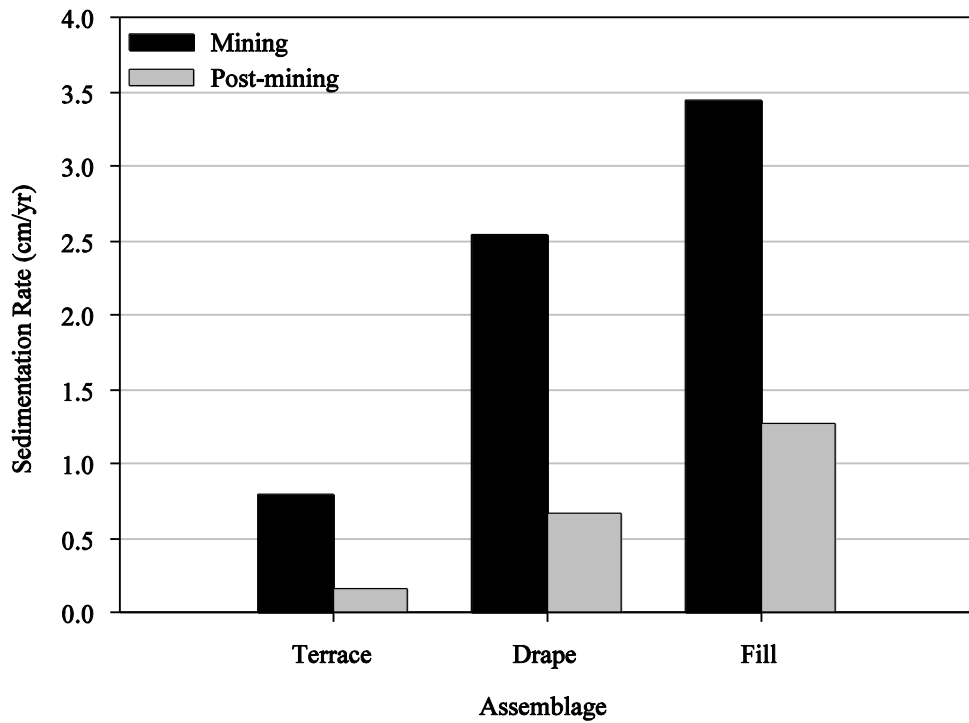


Figure 36. Average sedimentation rates for alluvial assemblages. Sedimentation rates are highest in channel fill assemblages and lowest in terrace assemblages. Post-mining sedimentation rates are lower than mining sedimentation rates for all assemblages.



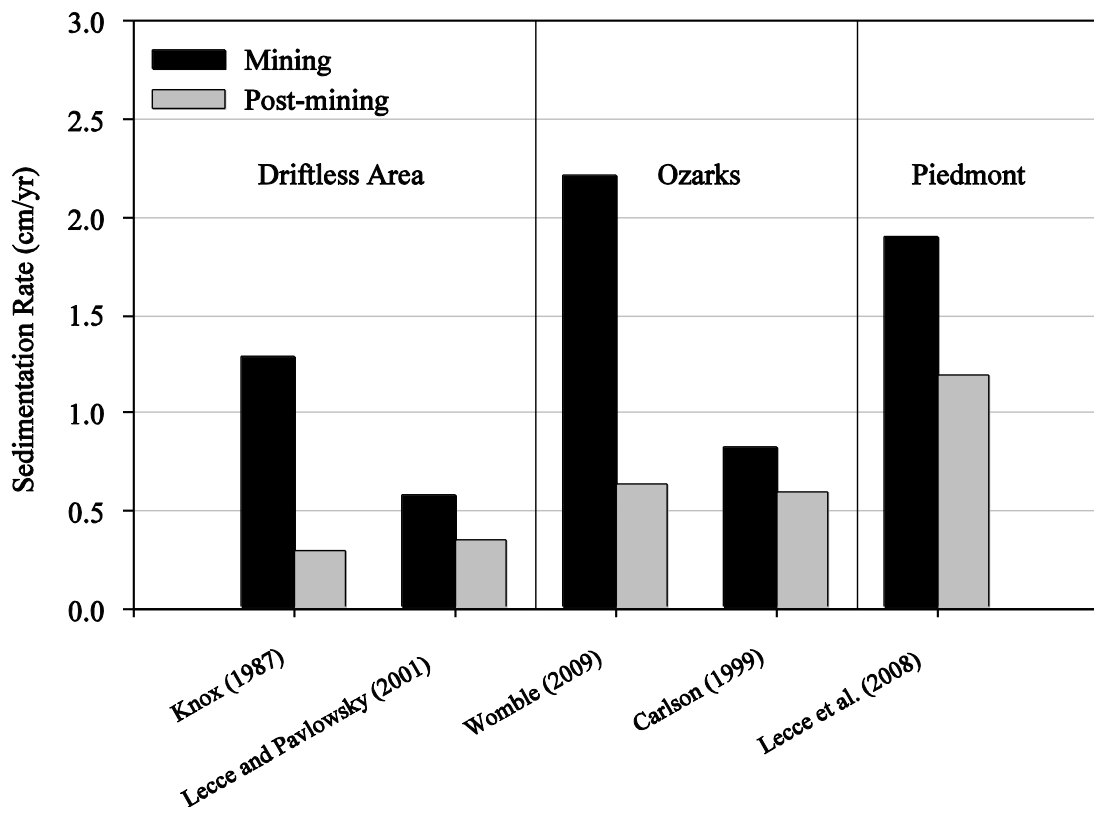


Figure 37. Average sedimentation rate compared to other studies. Mining sedimentation rates are higher than post-mining rates in all studies and rates at Pearson Creek are of the same magnitude as previous studies.

## **Geomorphic Evolution**

**Geomorphic Evolution by Site.** The geomorphic evolution of each site was interpreted using down-core profiles of soil color and Zn concentration. Site 1A is located in the upper most portion of the study area (0 m) where the valley floor is low and wide (Figure 13). Prior to mining, the channel appears to have been in approximately the same location as it is currently. However, the tributary that enters Pearson Creek at the railroad bridge was likely entering further downstream and to the west of the present day main channel. Prior to the mining period, a large bar formed between the two channels, possibly due to an increase in sediment supply from the upper watershed due to increased soil erosion (Figure 38A). The bar might have filled in the tributary channel, forcing the confluence upstream. Following the construction of the bar, contaminated mining sediment began accumulating on top of it, building a new floodplain. The presence of large trees (possibly 100 years old) on top of this surface suggests that it has been stable since mining ended (tree cores are needed to confirm this). Currently, deep excavation scars from topsoil mining created after the mining period on the floodplain provide pathways for flood waters to exploit (Figure 38A). Consequently, as the flow clears the bridge, it combines with the tributary flow and spreads out across the excavated floodplain, removing and depositing material during subsequent flooding events.

Site 1B is located at 91 m on the longitudinal profile, just downstream of Site 1A. The valley here is still wide and topsoil mining scars are present. However, the geomorphic evolution is slightly different. Completely contaminated cores at 38.3 m and 107 m suggest that the channel migrated east across the valley floor during the mining period, in-filling with sediment along the way (Figure 38B). Following mining, overbank

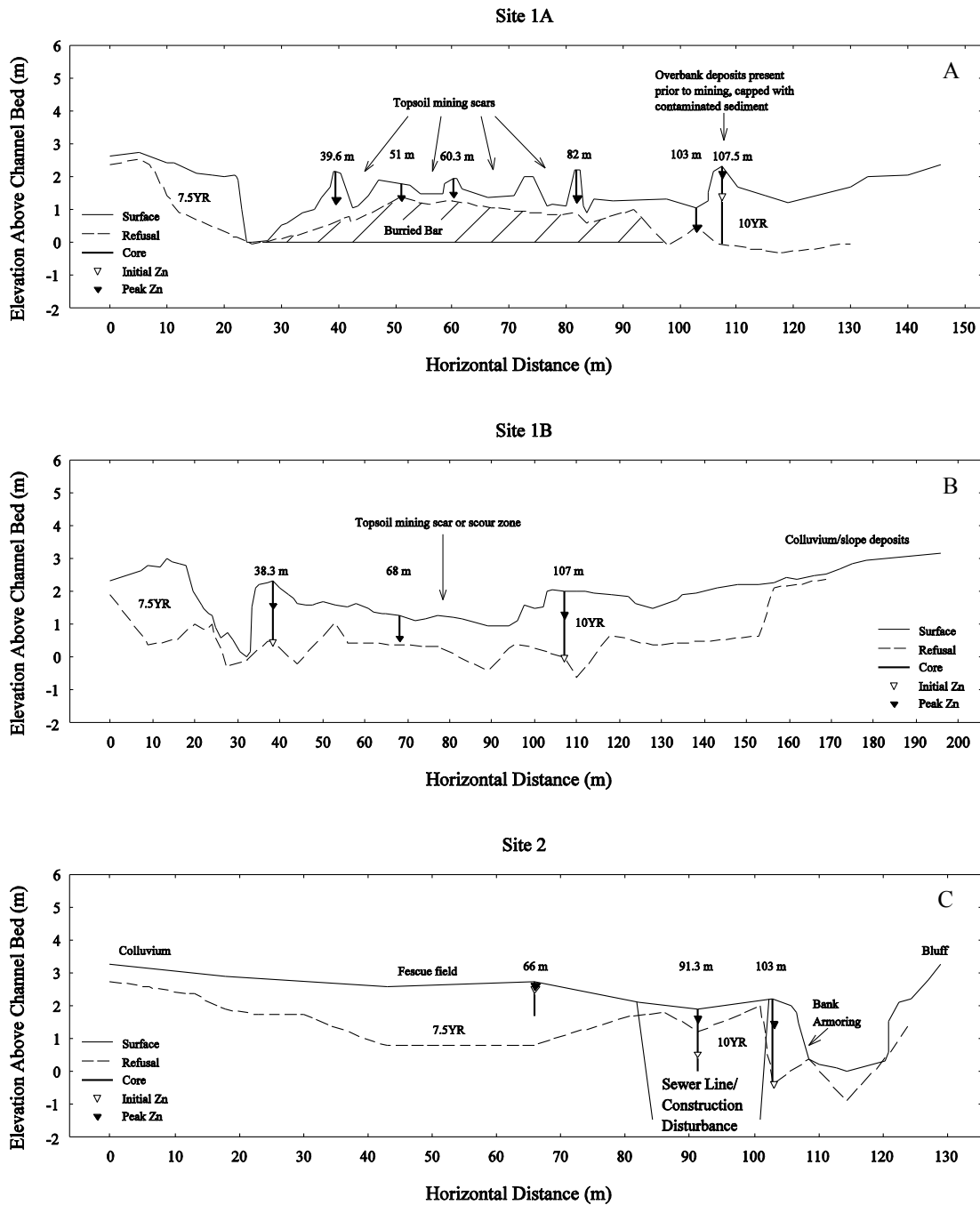


Figure 38. Cross-sections at (A) Site 1A, (B) Site 1B, and (C) Site 2. Figures are oriented looking downstream.

flooding deposited silty-material, increasing the height of the surface. Topsoil mining followed, removing much of this sediment.

Site 2 is located at 357 m on the longitudinal profile, downstream and around a meander from Site 1B. The channel here is relatively straight and pinned up against the bluff on the west side of the valley (Figure 13). Contaminated sediment east of the current channel indicates that the channel has migrated to the west since mining began (Figure 38C). A thin layer of contaminated sediment is present in the field, deposited during large flooding events since mining. Slope erosion of the bluff is contributing coarse material to the channel. However, the primary source of channel material appears to be from remobilized bar or splay deposits upstream. Colluvial slope deposits, notable by shallow refusal depths and 7.5YR sediment, are present on the east side of the valley (Figure 38C).

Site 3A is located 501 m on the longitudinal profile at the beginning of a large meander bend (Figure 13). The same fescue field at Site 2 is present on the east side of the valley at Site 3A (Figure 39A). Contamination is present in the top 1 meter of cores at 58 m, 91.5 m, and 108.5 m, indicating that 1 meter of sediment has been deposited since mining began. In addition, large refusal depths in the center of the channel indicate that the channel has aggraded as well. There is no evidence for horizontal channel activity due to the absence of contamination at or below the depth of the current channel bed elevation.

Sites 3B, 4A, and 4B, located at 579 m, 689 m and 717 m, respectively, have nearly identical geomorphic histories. Site 3B is oriented across the valley (east-west) and located just upstream of where the mining tributary enters Pearson Creek (Figure 13). Sites 4A and 4B are oriented along the valley (approximately north-

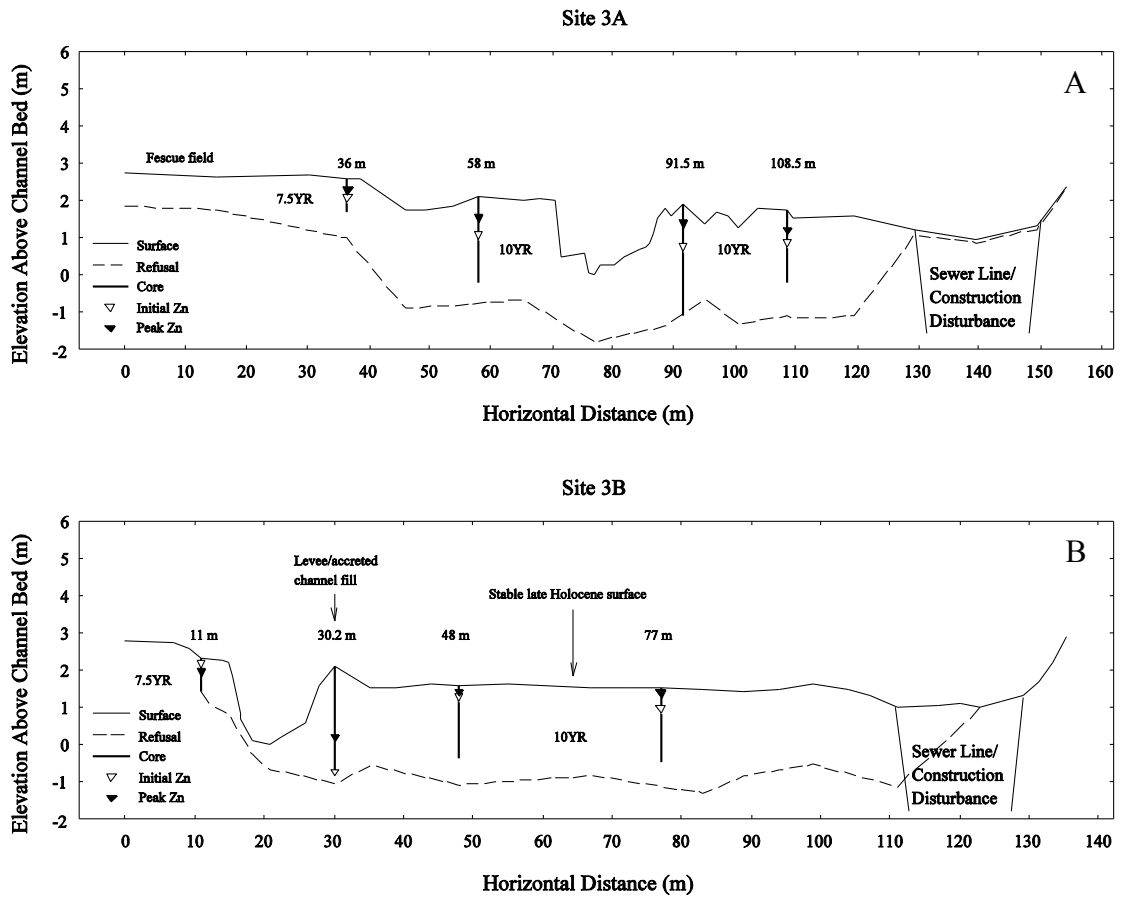


Figure 39. Cross-sections at (A) Site 3A and (B) Site 3B. Figures are oriented looking downstream.

south) just downstream of the mining tributary (Figure 13). All cross-sections dissect the same surface. The higher uncontaminated surface is an early to middle Holocene terrace at Site 3B and a late Holocene to historical terrace at Sites 4A and 4B (Figure 39B, Figure 40A, and Figure 40B). The lower surface in the center of each cross-section is late Holocene to historical in age and is contaminated near the top of the core profiles, indicating that the surface has encountered some vertical accretion. Cores located near the channel on the levees of all three sites indicate that some limited channel migration or contraction has occurred since mining began (as much as 7 m at Site 3B).

Site 4C is located at 742 m on the longitudinal profile up against the bluff. The geomorphic evolution here is similar to Site 3A with the exception that the channel here has migrated since mining ended. There is approximately 1 meter of contaminated sediment present on the east side of the channel, suggesting that it has been stable (Figure 40C). Contaminated bank samples from the west side of the channel indicate that it has been built since mining ceased. It is possible that the channel was located to the west of its current position and has migrated east since mining, filling-in with contaminated sediment as it did so.

Site 4D is located at 863 m on the longitudinal, just upstream of a large meander s-curve. The fescue field is present on the east side of the valley, followed by a very wide channel with a low bar, high bar, and floodplain (Figure 41A). A small tributary enters the channel just upstream and supplies a small amount of fresh gravel that forms small splays on top of Site 4Ds bar complex. The east side of the channel is currently being undercut and large woody debris in the channel has promoted scour upstream and shadow bar growth downstream. The west side of the valley is composed of another surface at a similar elevation to the fescue field. Both of these surfaces, represented

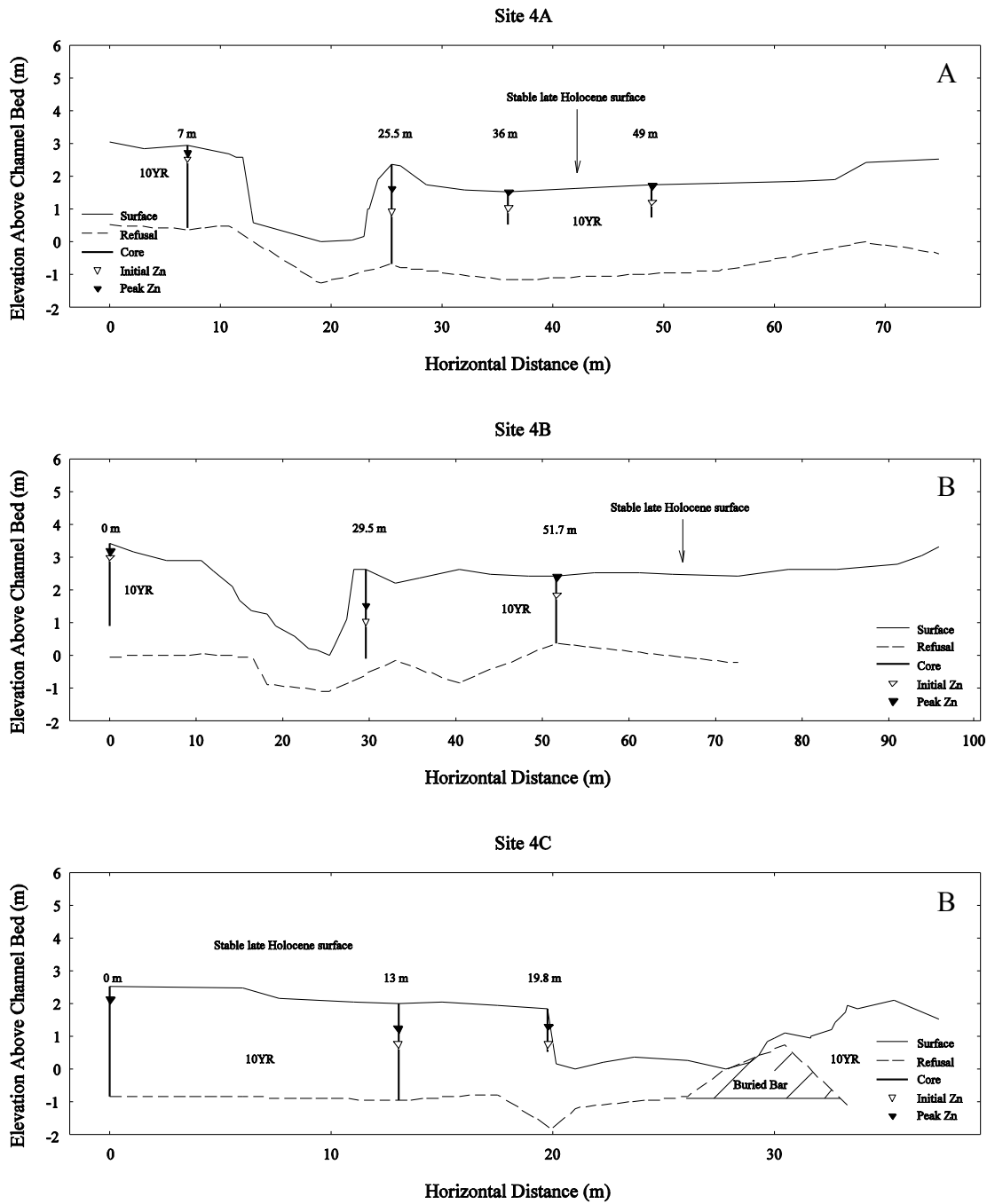


Figure 40. Cross-sections at (A) Site 4A, (B) Site 4B, and (C) Site 4C. Note the scale difference at Site 4C. Figures are oriented looking downstream.

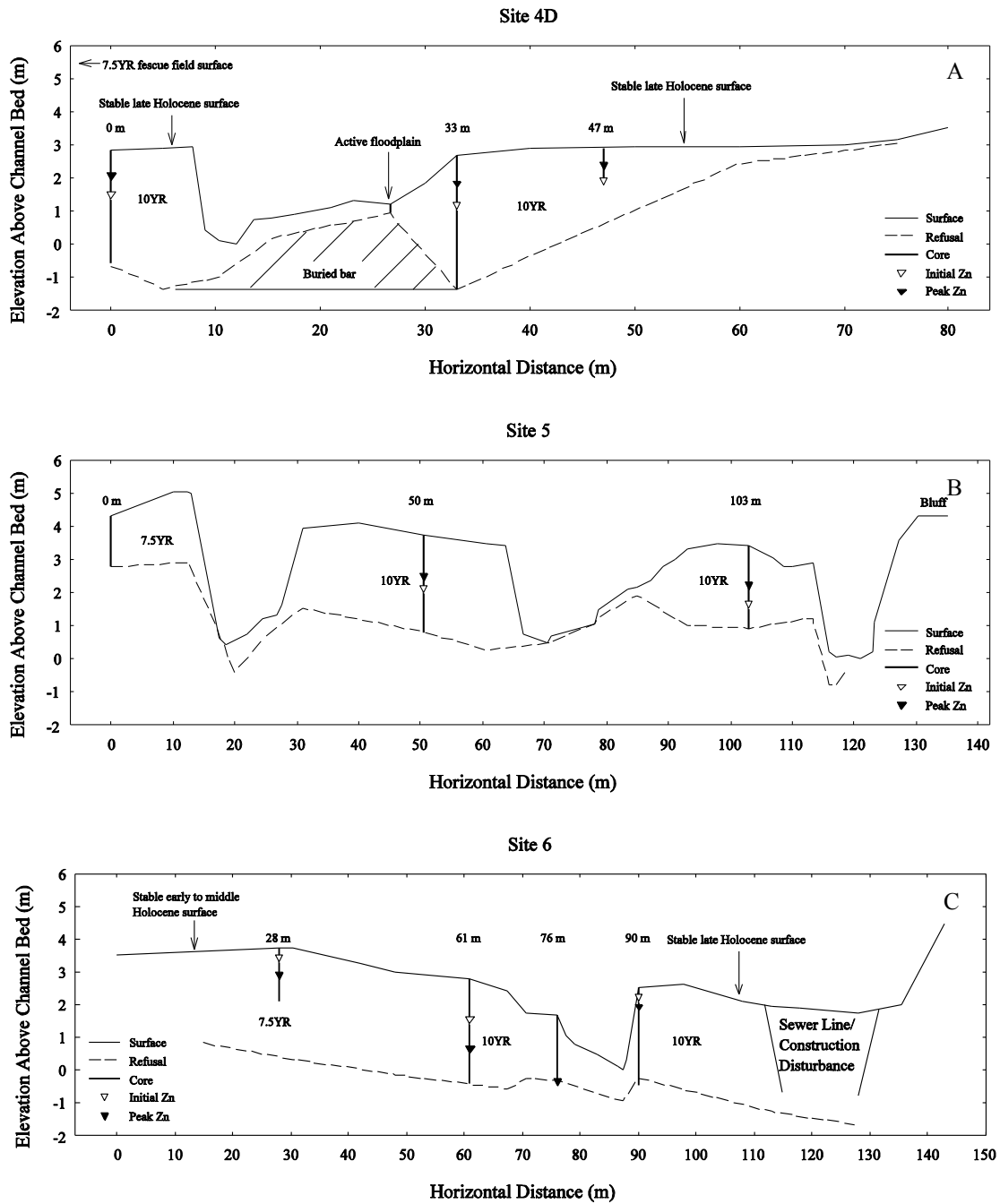


Figure 41. Cross-sections at (A) Site 4D, (B) Site 5, and (C) Site 6. Figures are oriented looking downstream (south).



by cores at 0 m and 47 m, are contaminated to a depth of approximately 1 meter, indicating that they were present prior to mining. The lower surface represented by the core at 33 m has a similar history and comparable amount of contaminated sediment on top of it, suggesting that it too was present prior to the mining period. At this site, approximately 1 meter of bed aggradation has occurred, evidenced by the ~1 m depth to refusal in the channel. It can be surmised, then that the channel configuration was similar prior to mining and simply increased in elevation.

Site 5 intersects the stream three times at 935 m, 1,103 m, and 1,147 on the longitudinal profile around a large meander s-curve (Figure 13). The fescue field is located on the east side of the valley, followed by two point bar complexes separated by channels, and a final channel pinned up against the bluff on the west side of the valley (Figure 41B). The point bar closest to the field terrace is building in the down-valley direction while the second is building in the up-valley direction. The fescue field surface is uncontaminated whereas the two other surfaces at 50 m and 103 m are contaminated to a depth of 1.5 m each.

Site 6 is located at 1,243 m on the longitudinal profile on the outside of a meander bend, just downstream of Site 5 (Figure 13). The fescue field on the east side of the valley is the highest surface present. From the field, two lower surfaces step down toward the channel (Figure 41C). High and low bars are located on the east side of the channel. A surface lower in elevation than the field, is located on the west side of the valley, extends to the bluff, and is currently being eroded and undercut. Cores in the field (28 m) and lower surface on the west side of the channel (91 m) are contaminated to a depth of 60 cm, indicating that the surfaces were present and stable prior to mining. The presence of 7.5YR sediment on the upper surface indicates that it is older (early to middle

Holocene) than the lower 10YR surface (late Holocene to historical). The core at 61 m is contaminated to a depth of 1.70 m whereas the core at 76.1 m is completely contaminated. The uncontaminated portion of the core at 61 m suggests that it was present prior to mining. However, the peak Zn concentration found in the core at 76.1 m is lower than in the core at 61 m, suggesting that the surface at core 76.1 m was constructed since mining ceased, likely due to lateral migration of the channel west.

**General Evolution Model.** Conceptual diagrams are used to show the arrangement of geo-stratigraphic assemblages and how they relate to the geomorphic evolution of Pearson Creek. The age of deposits and timing of geomorphic events is described as the pre-mining, mining, and post-mining periods. The pre-mining period (prior to 1885) involved sedimentation of uncontaminated (below background) sediment, soil development on higher surfaces, and narrower channels. During the mining period (1885-1912), sediment with Zn concentrations exceeding background was deposited, channels widened, and lateral migration began. However, it is likely that increased channel activity (widening and migration) would have begun just prior to mining due to the conversion of the watershed to agricultural land uses. Initial land use changes, occurring as early as the 1830s, would have increased the magnitude and frequency of floods and caused channel widening, alluviation, and bed aggradation (Knox, 1977; Lecce, 1997). The post-mining period (1912-present) signifies the time when Zn levels in sediment being deposited dropped below the peak concentration but were still above background. Sources of post-mining sediment could include: remobilized contaminated deposits, construction sites, industry, and eroding tailings piles. Following the development of conceptual diagrams, patterns between sites show that diagrams could be grouped into three dominant zones (Figure 42). It can be seen that these zones seem to

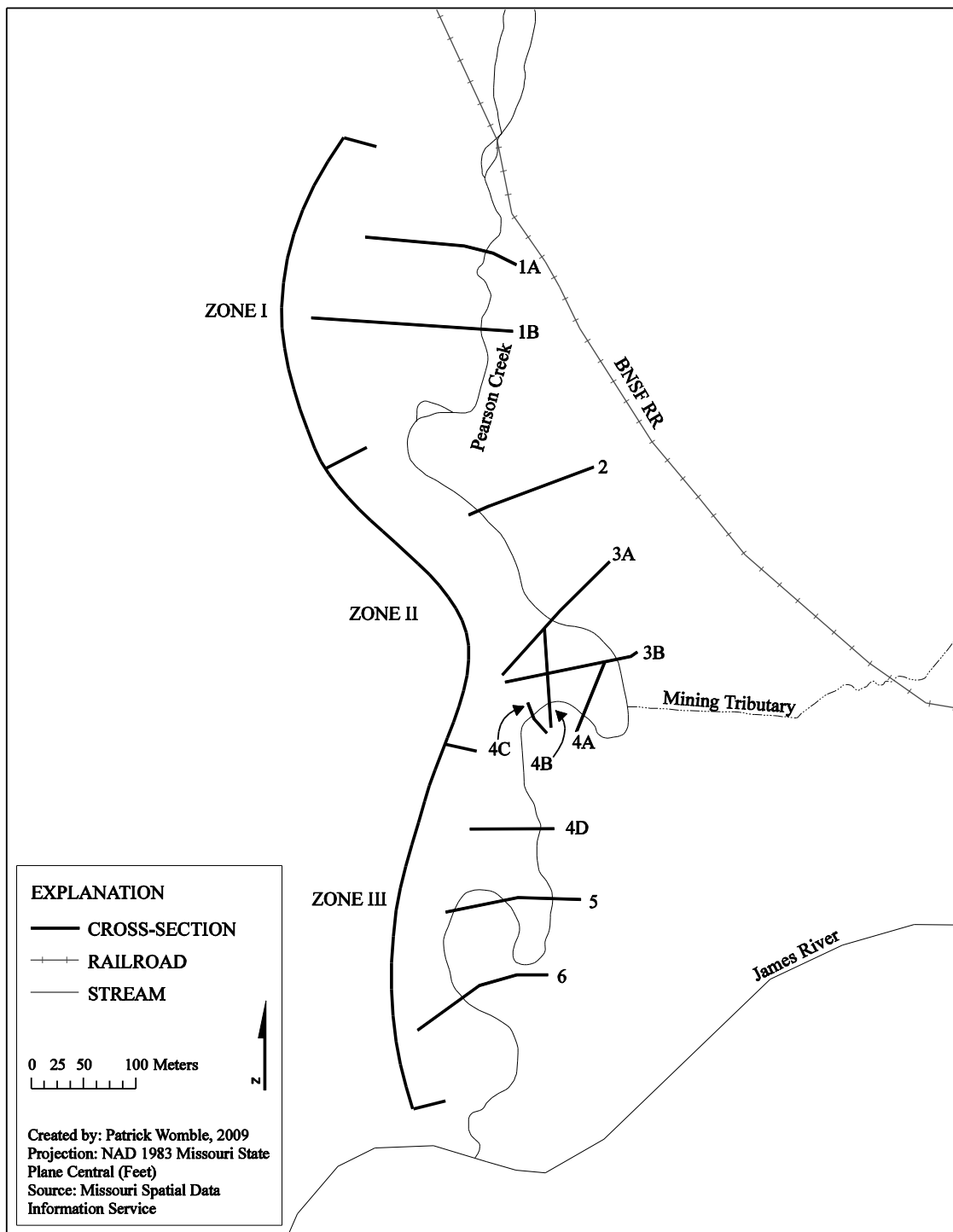


Figure 42. Distribution of zones determined from conceptual diagrams.

coincide with changes in the planform of Pearson Creek. The stream in Zone I is relatively straight (sinuosity= 1.1) whereas in Zones II and III, the stream is more meandering (sinuosity= 1.8). Conceptual diagrams from sites best representing each zone will be used to describe the general geomorphologic evolution of lower Pearson Creek.

Zone I. The conceptual diagram for Zone I, represented by Site 1B, shows a early to middle Holocene terrace veneer assemblage on the east side of the valley, a scoured and excavated channel fill assemblage in the middle of the valley, and a floodplain drape sediment assemblage on the west side of the valley (Figure 43A). The pre-mining period involved the construction of the 7.5YR terrace. During, or just prior to, the mining period, a disturbance (likely the result of increased sediment supply due to hillslope erosion caused by land use changes) caused the channel to fill in with sediment and push the site of the confluence between the small tributary near the railroad bridge and Pearson Creek closer to the bridge, transforming the west side of the valley into a backswamp. The channel fill assemblage confirms this. Some time following the mining period, the area was known to have undergone some limited topsoil mining in the channel fill assemblage sediment. Fully contaminated sediment and the presence of large trees on top of pendants left behind by topsoil mining suggest that the surface was stable following Zn mining and prior to soil removal. Gravel and fines are currently being deposited in this area as floods exploit the sites of excavation.

Zone II. The conceptual diagram for Zone II, represented by Site 3B, has terraces on both sides of the channel which imply that this area was relatively stable prior to and since the mining period (Figure 43B). The 7.5YR terrace veneer assemblage indicates that the surface was built during early to middle Holocene, while the lower 10YR terrace

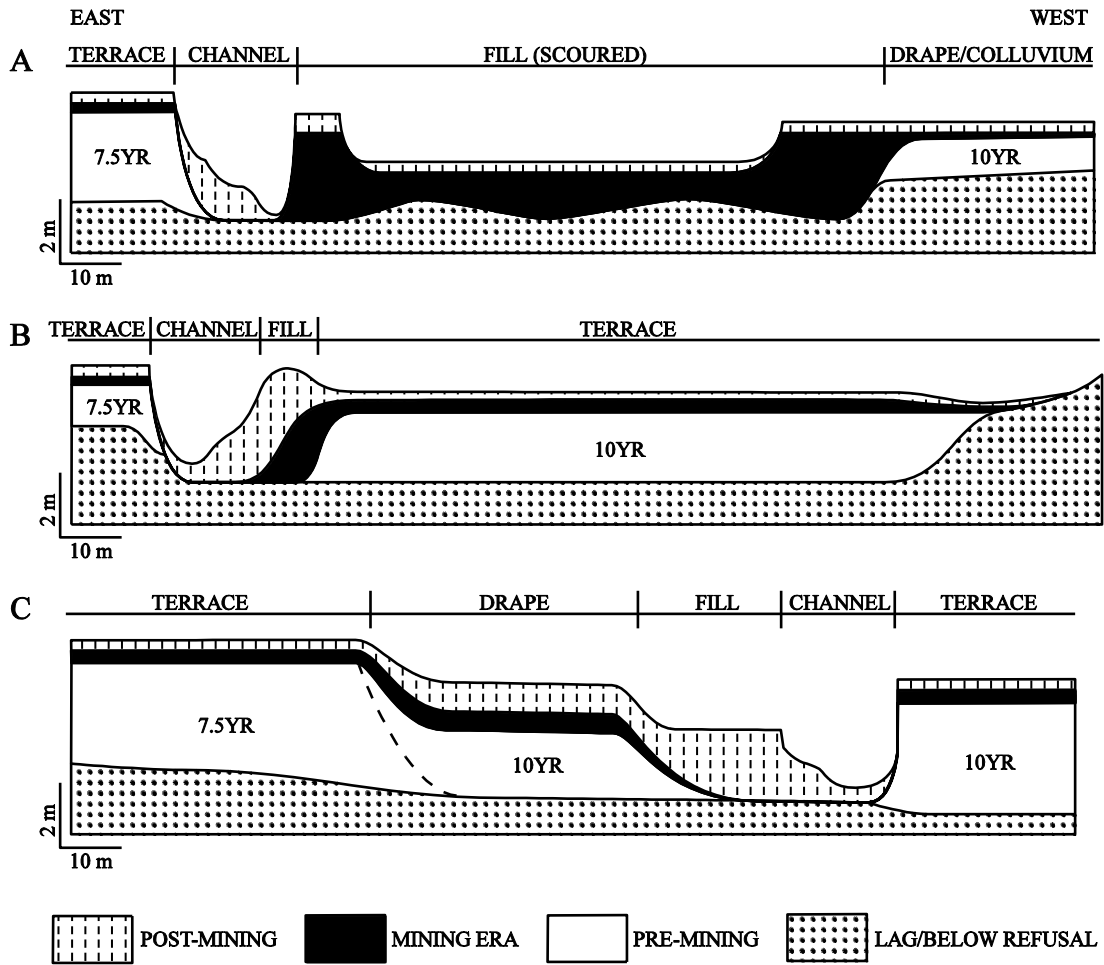


Figure 43. Floodplain models. Conceptual diagrams of (A) Zone I at Site 1B, (B) Zone II at Site 3B, and (C) Zone III at Site 6. Figures are oriented looking downstream.

on the west side of the valley indicates that lateral migration occurred at some point during the late Holocene. A thin channel fill assemblage on the west side of the channel indicates that the channel has contracted or migrated slightly to the east and subsequently filled in with sediment since mining began. This trend is observed at Sites 3B, 4A, and 4B. At Site 2, the channel has moved toward the west. As evidenced by the terrace assemblages, vertical accretion on overbank surfaces has dominated in this zone since mining began. Local variability is observed at Sites 3A and 4C and is related to where they are in relation to the meander bend. These sites saw no lateral migration during the mining period. However, similar to the other sites, vertical accretion has dominated since mining began.

Zone III. The conceptual diagram for Zone III, represented by Site 6, has all three assemblages present on the east side of the valley, stepping down in elevation towards the channel (Figure 43C). This zone has had a significant amount of both vertical and lateral accretion since mining began. During the early to middle Holocene, the 7.5YR terrace was constructed. Following this, during the late Holocene to historical period, the 10YR terrace was built. During the mining period, the floodplain drape sediment was deposited, responding to the increased sediment supply due to land use changes. Vertical accretion was dominant at this time. The post-mining period has seen primarily lateral migration at work, as evidenced by the large accumulation of post-mining sediment at Sites 4D and 6 and active point bars at Site 5. The thickness of post-mining sediment appears to be greater in the deposition zone than in other zones and could be the result of frequent backflooding from the James River. Where affected, backflooding creates an area of decreased velocity where flow from Pearson Creek collides with the stagnant backflood waters. The sudden decrease in velocity causes sediment to drop out of

suspension onto flooded surfaces. Therefore, more sedimentation would be present in areas that are more frequently subjected to backflooding, such as Sites 4D, 5, and 6 on Pearson Creek. Additionally, a decrease in slope, possibly due to a base level rise of the James River induced by land use change, would promote increased meandering of the stream and deposition of post-mining sediment in the channels.

A timeline of land use and geomorphic change is presented in Table 10. It reports the most prominent geomorphic changes and dominant sedimentation processes occurring during the pre-mining, mining, and post-mining periods in each zone as well as the land use history in the watershed. Pre-mining geomorphic processes were dominated by vertical accretion of uncontaminated sediment and the construction of 7.5 and 10YR terraces. Mining period geomorphic processes included channel adjustments (migration, widening), bed aggradation, and were dominated by both vertical and lateral accretion. Post-mining geomorphic processes have been dominated by vertical accretion with some limited lateral accretion in Zone II and a significant amount of lateral accretion in Zone III.

A lag exists between when land use changes begin and when the effects from them to appear downstream (Knox, 1977) and it is possible that when land use changes prior to mining occurred, the channel responded by getting wider and deeper. If the peak effects of land use change (increased sediment yield and runoff) coincided with mining, the input of sediment would have caused the channel to contract and the bed to aggrade. This is supported by the presence of contaminated sediment along the channel margins and below the current bed at the 103 m core at Site 2 and the 30.2 m core at Site 3B. A similar pattern, however in post-mining sediment, was found at Site 6. Aggradation at this site could be related to base level rise of the James River following the construction

Table 10. Timeline of land use history and geomorphic change.

| Zone      | Pre-Mining (Holocene to 1885)  | Mining Era (1885-1920)  | Post-Mining (1920-Present)   |
|-----------|--|---|--|
| Watershed | <ul style="list-style-type: none"> <li>– Land clearing for farming</li> <li>– Row-crop farming dominant</li> </ul>   | <ul style="list-style-type: none"> <li>– Row-crop on the decline, pasture farming on the rise</li> </ul>  | <ul style="list-style-type: none"> <li>– Pasture farming dominant</li> <li>– Soil conservation practices implemented</li> </ul>  |
| Zone I    | <ul style="list-style-type: none"> <li>– Early to middle Holocene construction of 7.5YR terrace</li> <li>– Disturbance-induced bar constructed in center of valley</li> <li>– Channel to or near its current position just prior to mining</li> <li>– Vertical accretion dominant</li> </ul> | <ul style="list-style-type: none"> <li>– Construction of floodplain on bar during high flows</li> <li>– Lateral migration dominant</li> </ul>   | <ul style="list-style-type: none"> <li>– Removal of sediment by scour or excavation</li> <li>– Erosion and migration toward the east bank</li> <li>– In-channel deposition dominant</li> </ul> |
| Zone II   | <ul style="list-style-type: none"> <li>– Early to middle Holocene construction of 7.5YR terrace</li> <li>– Lateral construction of late Holocene to historical 10YR terrace</li> <li>– Vertical and lateral accretion occurring</li> </ul>   | <ul style="list-style-type: none"> <li>– Little contamination deposited on surface</li> <li>– Limited channel widening</li> <li>– Channel bed aggradation (~1.5-2 meters)</li> <li>– Vertical accretion more dominant than lateral accretion</li> </ul> | <ul style="list-style-type: none"> <li>– Vertical accretion on stable terrace surfaces</li> <li>– Vertical accretion dominant early on</li> <li>– Lateral accretion more recent</li> </ul>     |
| Zone III  | <ul style="list-style-type: none"> <li>– Early to middle Holocene construction of 7.5YR terrace</li> <li>– Late Holocene to historical construction of 10YR terrace</li> <li>– Vertical accretion dominant</li> </ul>  | <ul style="list-style-type: none"> <li>– Vertical accretion of contaminated sediment on overbank surfaces</li> <li>– Channel bed aggradation (~1.5-2 meters)</li> <li>– Vertical accretion dominant</li> </ul>  | <ul style="list-style-type: none"> <li>– Formation and extension of point bars</li> <li>– In-filling of channels with post-mining sediment</li> <li>– Lateral accretion dominant</li> </ul>    |



of Lake Springfield or in-channel deposition from an increase in sediment supply due to land use changes.

### **Contaminant Storage in Floodplain Deposits**

In this section, the distribution of mass storage of contaminated sediment, Zn, and Pb is evaluated. Previous work showed that the concentration of Zn is dependent on elevation above the thalweg, distance from the thalweg, and distance downstream from mining sources (Figure 25; Figure 28). The lateral distribution of Zn concentrations along floodplain transects was explored by examining geo-stratigraphic assemblage trends (Table 8; Figure 34). These trends shed light on the intensity of Zn stored in alluvial deposits but not the total mass storage.

The first step to understanding the volume of storage involves the mapping of different geo-stratigraphic assemblages in the study area (Figure 44). The second step is to use core information to estimate the thickness of contamination for each assemblage by zone (Table 11). The third step involves the calculation of mass storage (Equations 1, 2; Table 11). Finally, spatial patterns of storage are plotted (Figure 45).

Storage of contaminated sediment, Zn, and Pb is similar between all three Zones (Table 11). In Zone I, Channel Fill assemblages store more contaminated sediment, Zn, and Pb than either Terrace Veneer or Floodplain Drape assemblages. Zinc and lead storage patterns in Zone II are similar to those found in Zone I, however at lower magnitudes. Storage of contaminated sediment in Floodplain Drape and Terrace Veneer assemblages is greater in magnitude than in Zone I. This is because Terrace Veneer assemblages on either side of the stream limit the amount of available storage by limiting the amount of lateral migration in the stream more than in Zone I or Zone III. Therefore,

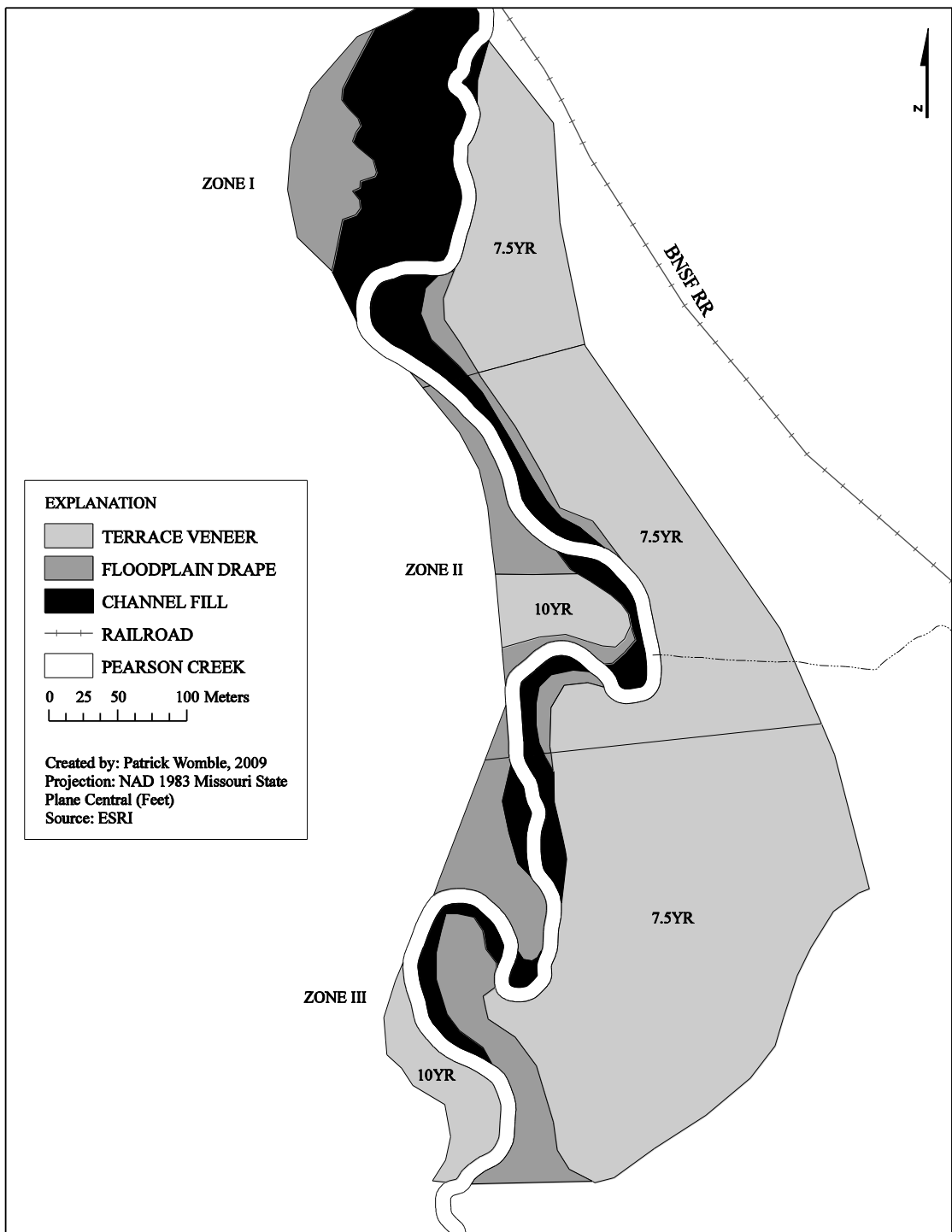


Figure 44. Spatial distribution of geo-stratigraphic assemblages.

Table 11. Summary of contaminated sediment, Zn, and Pb storage. TV=Terrace Veneer; FD= Floodplain Drape; CF= Channel Fill.

| Zone               | Assemblage   | Area<br>(m <sup>2</sup> ) | Contaminated Sediment |                             |                | Zinc                 |              | Lead                 |              |
|--------------------|--------------|---------------------------|-----------------------|-----------------------------|----------------|----------------------|--------------|----------------------|--------------|
|                    |              |                           | Depth<br>(m)          | Volume<br>(m <sup>3</sup> ) | Mass*<br>(Mg)  | Concentration<br>(%) | Mass<br>(Mg) | Concentration<br>(%) | Mass<br>(Mg) |
| I                  | TV           | 14,734                    | 0.38                  | 5,599                       | 7,278          | 0.016                | 1.1          | 0.005                | 0.4          |
|                    | FD           | 6,941                     | 0.91                  | 6,316                       | 8,211          | 0.033                | 2.7          | 0.009                | 0.7          |
|                    | CF           | 17,078                    | 0.86                  | 14,687                      | 19,093         | 0.156                | 29.8         | 0.031                | 5.9          |
|                    | <u>Total</u> | <u>38,752</u>             |                       | <u>26,602</u>               | <u>34,582</u>  |                      | <u>33.7</u>  |                      | <u>7.0</u>   |
| II                 | TV           | 32,293                    | 0.38                  | 12,271                      | 15,953         | 0.016                | 2.5          | 0.005                | 0.8          |
|                    | FD           | 6,525                     | 1.25                  | 8,124                       | 10,561         | 0.054                | 5.7          | 0.017                | 1.8          |
|                    | CF           | 4,167                     | 2.33                  | 9,696                       | 12,604         | 0.130                | 16.4         | 0.042                | 5.3          |
|                    | <u>Total</u> | <u>42,985</u>             |                       | <u>30,091</u>               | <u>39,118</u>  |                      | <u>24.6</u>  |                      | <u>7.9</u>   |
| III                | TV           | 61,245                    | 0.43                  | 26,540                      | 34,502         | 0.039                | 13.4         | 0.005                | 1.6          |
|                    | FD           | 11,647                    | 1.42                  | 16,500                      | 21,450         | 0.067                | 14.4         | 0.022                | 4.8          |
|                    | CF           | 4,319                     | 2.00                  | 8,639                       | 11,231         | 0.044                | 4.9          | 0.009                | 1.0          |
|                    | <u>Total</u> | <u>77,212</u>             |                       | <u>51,679</u>               | <u>67,183</u>  |                      | <u>32.7</u>  |                      | <u>7.4</u>   |
| <u>Grand Total</u> |              | <u>158,950</u>            |                       | <u>108,372</u>              | <u>140,883</u> |                      | <u>90.9</u>  |                      | <u>22.3</u>  |

\* See Equations 1 and 2 in Chapter 4.

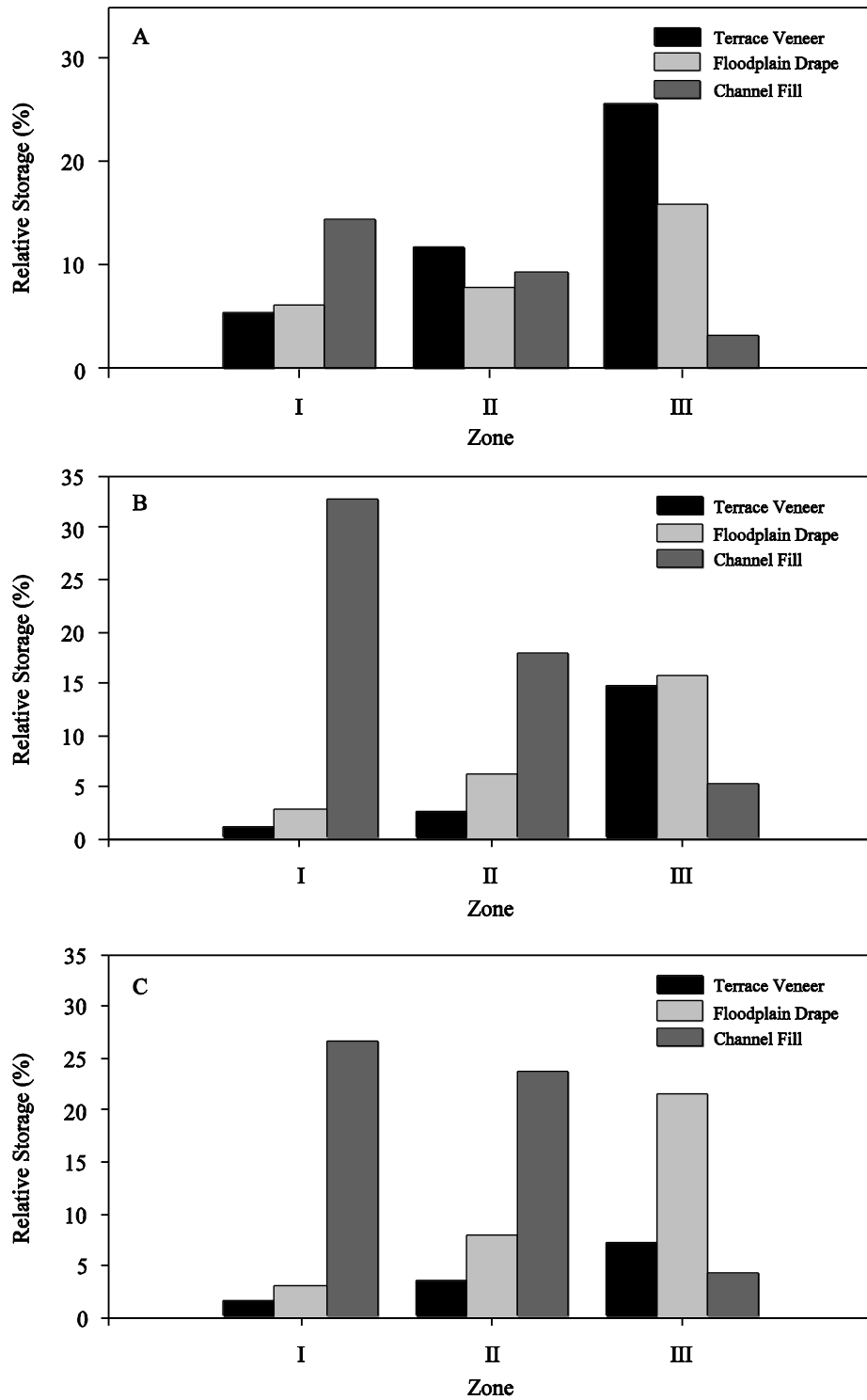


Figure 45. Relative storage by zone. (A) Contaminated sediment, (B) Zn, and (C) Pb relative storage. Relative Storage (%) = (Component Storage/Total Floodplain Storage)\*100.

contaminated sediment introduced by the mining tributary (Figure 13) would be washed downstream into Zone III and out into the James River. In Zone III, the Floodplain Drape assemblage is the site of the most storage (Figure 45).

In order to see how storage is distributed within geo-stratigraphic assemblages, the total mass storage of each component (contaminated sediment, Zn, Pb) within each assemblage was divided by the total mass storage of that component for the entire study area. The results indicate that for Zn and Pb storage increases from Terrace Veneer → Floodplain Drape → Channel Fill assemblages (Figure 46). In fact, Channel Fill assemblages store approximately 50% of the total Zn (51.1 Mg) and 55% of the Pb (12.2 Mg) in the study area. Furthermore, approximately 33% of the Zn (29.8 Mg) and 26% of the Pb (5.9 Mg) stored in the entire study area is located within the Channel Fill assemblage in Zone I alone. This is due to the low, wide floodplains present as a result of topsoil mining and subsequent scouring. For contaminated sediment, storage increases from Floodplain Drape to Channel Fill to Terrace Veneer. This likely skewed by the large area used for the Terrace Veneer assemblage in Zone III in the calculations.

Since the Channel Fill assemblage in Zone I was excavated during topsoil mining (sometime after mining ceased), it might be helpful to calculate the storage values of the area prior to topsoil mining. To do this, the maximum thickness of contamination in the Channel Fill assemblages within Zone I (1.83 m at Site 1B) was used. The resulting pre-topsoil mining storage calculation doubled the Channel Fill assemblage values for contaminated sediment, Zn, and, Pb. These results indicate that prior to topsoil mining, over half of the total Zn and nearly half of the total Pb in the study area would have been stored in the Channel Fill assemblage in Zone I. This is significant because this area would have been a large source of potential pollution if topsoil mining had not occurred.

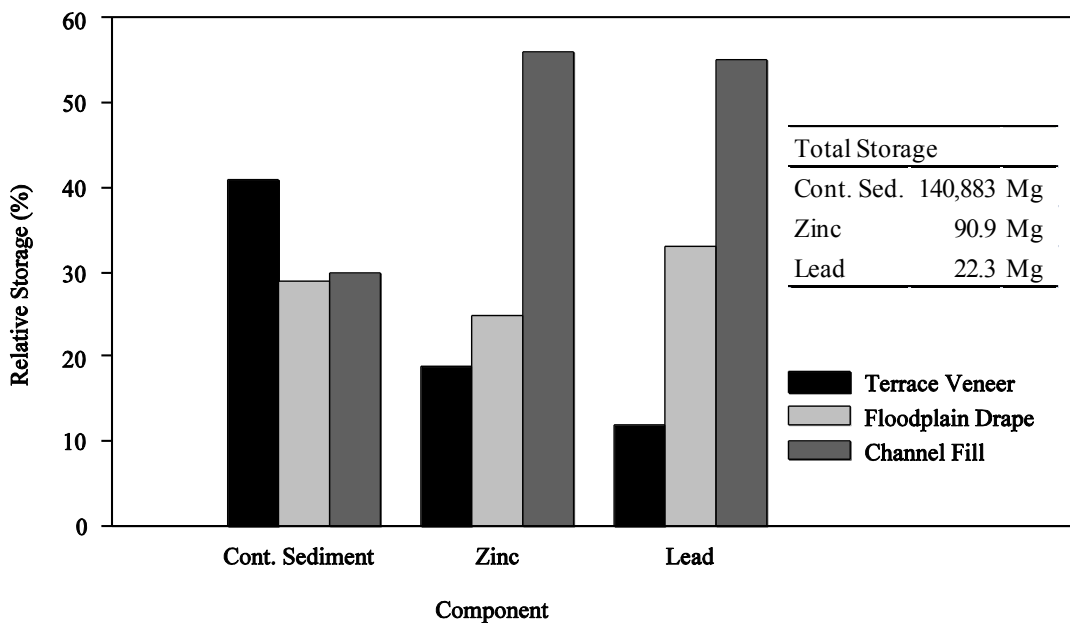


Figure 46. Distribution of relative storage by geo-stratigraphic assemblage for contaminated sediment, Zn, and Pb.

Storage values for the Terrace Veneer assemblage is unusually high in Zone III due to the large area that was mapped. The large areal extent of the Terrace Veneer assemblage within Zone III draws up the perceived storage value in Zone III higher than is likely present (Figure 46). The Terrace Veneer on the eastern side of the valley, closest to the James River, has not been cored to determine actual values of contaminant storage. Instead, to keep the calculations simple, it was assumed that this area was contaminated equally throughout. However, since contamination decreases with distance from Pearson Creek, it is likely that there is very little contamination on the eastern side of the valley, which would result in smaller storage values. This area could be further sampled to improve on these results.

Mass storage values can be used for determining what percent of the total mining production is stored in floodplain deposits. Total documented production in Pearson Creek for Zn was 21,150 Mg and for Pb was 5,229 Mg (Thomson, 1986). Results indicate that 0.43% of both Zn and Pb are currently stored in the study area. These values only represent a portion of the total storage in alluvial sediment in areas affected by the mines. For example, it is known that areas upstream of the current study area were affected by historical mining practices and that Zn is present in alluvial sediments along the James River downstream of Pearson Creek and in Lake Springfield. Incorporating these areas would provide a better estimate of the total amount of Pb and Zn introduced into alluvial sediment as a result of mining operations along Lower Pearson Creek.

## CHAPTER 7

### SUMMARY AND CONCLUSIONS

The purpose of this study was to develop a history of geomorphic responses to land use change along lower Pearson Creek by (1) determining the magnitude and across-valley distribution of mining-contaminated sediment; and (2) using floodplain sedimentology and trace-metal dating to determine recent and historical geomorphic changes. The broader goal was to increase the understanding of how streams in the Ozarks have responded to historical land use change and how they store mining-related sediment. To complete this study, soil cores were extracted from alluvial deposits along cross-sections and analyzed for physical and geochemical properties. Results of the analyses were used to correlate stratigraphic similarities and identify across-valley Zn trends.

The results of this study reveal that alluvial deposits along lower Pearson Creek are contaminated with Zn (Table 7) and were influenced by post-settlement land use change. The mean Zn concentration of all samples was 600 ppm while the median concentration was 193 ppm, ~8 and ~2.5 times background level, respectively. In general, the thickness of Zn contaminated sediment decreases with distance away from and height above the channel. Sedimentation rates from 1885 to 1912 ranged from 0 cm/yr to 4.79 cm/yr and from 1912 to 2008 ranged from 0 cm/yr to 2.08 cm/yr. High sedimentation rates during the mining period were probably due to combined impacts of mining operations and row crop farming. The reduction in post-mining sedimentation rates is likely due to better soil management practices and conversion from row crop farming to pasture farming.



Three unique geo-stratigraphic assemblages were identified during this study: terrace veneer, floodplain drape, and channel fill. Terrace veneer assemblages are characterized by <50 cm of slightly contaminated sediment overly uncontaminated (<77 ppm) 7.5YR (early to middle Holocene) or 10YR (late Holocene to historical) sediment and signify older floodplains that have since been abandoned by Pearson Creek. Floodplain drape assemblages consist of approximately 1 m of contaminated 10YR sediment overlying uncontaminated 10YR sediment. Channel fill assemblages are made of up fully contaminated 10YR sediment that has been deposited since mining began. They indicate sediment was deposited in the channel during channel migration or contraction of the channel margins. Terrace veneer assemblages are generally located farthest from and highest above the channel, while channel fill assemblages are located nearest to the channel in both elevation and distance (Figure 34). Zn concentrations increase from terrace veneer assemblages to channel fill assemblages (terrace veneer < floodplain drape < channel fill) (Table 8). Zinc concentrations also decrease in the downstream direction with a slight increase near where the mining tributary enters Pearson Creek (Figure 25).

Using floodplain assemblages, floodplain conceptual diagrams were developed and the geomorphic history of lower Pearson Creek was determined (Table 10). During the pre-mining period (prior to 1885), Holocene and post-Holocene terraces were being built and vertical accretion was the dominant form of sedimentation. The mining period was characterized by large inputs of sediment, channel instability, and both vertical and lateral accretion. Since mining ceased, the channel has undergone some recovery (contraction of the channel margins) and has been dominated by vertical accretion with

some limited lateral accretion in Zone II and significant amount of lateral accretion in Zone III.

The geomorphic form of lower Pearson Creek is influenced by three hydrologic controls: Pearson Creek dominated (Zone I); Transition zone (Zone II); James River dominated (Zone III). Increasing sediment thickness downstream indicates that bed aggradation and overbank sedimentation has occurred (Figure 35). Also, Pearson Creek changes from a relatively straight channel (sinuosity= 1.1) in Zone I to a more meandering channel (sinuosity=1.8) in Zone II and III (Figure 42). The change in sediment thickness and planform could be attributed a base level rise of the James River caused by in-channel aggradation. Flood waters would have been able to travel further up Pearson Creek and encourage deposition where the stream entered the backflooded areas and lost the ability to transport sediment.

### **Management Implications**

Past mining operations along lower Pearson Creek have introduced an extensive amount of metals into the floodplains, yet management practices have not been implemented. Geochemical data show the magnitude of Zn and geomorphic processes describe the distribution of Zn and its potential to be eroded. Suggested guidelines for determining harmful levels of pollutants in sediment are scattered throughout the literature. The Screening Quick Reference Tables (SQuiRTs) were developed from reviews of the literature in an attempt to set some consistent guidelines (Table 12). Target values are safe levels that mitigation should attempt to reach while Intervention values are levels at which mitigation should begin. MacDonald et al. (2000) is one source in the literature that provides similar guidelines (Table 12). Threshold Effect

Table 12. Guidelines for Zn concentration in freshwater sediment.

| Source        | Zinc (ppm) | Exceedance (%) | Pb (ppm) | Exceedance (%) |
|---------------|------------|----------------|----------|----------------|
| TEC*          | 121        | 57             | 35.8     | 58             |
| PEC*          | 459        | 33             | 128      | 28             |
| Target†       | 16         | 100            | 55       | 51             |
| Intervention† | 350        | 37             | 530      | 9              |

\*TEC and PEC values from MacDonald et al. (2000)

†Target and Intervention values from SQuiRTs (2008)

Concentrations (TEC) are “values below which effects are unlikely to occur,” or “non-toxic,” while Probable Effect Concentrations (PEC) are “values above which harmful effects are likely to be observed,” or “toxic.” At Pearson Creek, the Target value for Zn is exceeded by 100% of the samples and for Pb by 51% of the samples. The Intervention value for Zn is exceeded by 37% of the samples and for Pb by 9% of the samples. The TEC value for Zn is exceeded by 57% of the samples and for Pb by 58% of the samples. The PEC is for Zn is exceeded by 33% of the samples and for Pb by 28% of the samples. Target values for Zn are unrealistic in this area since the background concentration of Zn is greater the Target value. However, since Zn and Pb exceed the PEC and Intervention values, some remediation might be required, the specifics of which are beyond the scope of this thesis.

Based on the data presented here, any remediation that does take place should focus on the Channel Fill assemblages in Zone I (Figure 44, Figure 45). These areas contain the highest concentrations of Zn and Pb and make up only 11% of the total area yet they currently store approximately one third of the total amount of Zn and Pb in the study area. However, Channel Fill assemblages in each zone have high concentrations of Zn and Pb. The map of the distribution of assemblages for the study area could be used to guide managers to locations containing large amounts of both Zn and Pb (Figure 44).

### **Future Work**

This study focused on developing a timeline of the geomorphic evolution near the confluence of Pearson Creek and the James River using the stratigraphic distribution of mining pollutants along valley cross-sections. An important aspect not researched here is the mobility of the pollution. When studying pollutants in any natural system, identifying

their source(s) is important to developing remediation plans. Due to the presence of elevated Zn levels near the channel margins, floodplain reworking (bank erosion) could reintroduce Zn into Pearson Creek where it could be transported downstream and into the James River.

Also, a similar study along the James River, downstream of Pearson Creek, could help in understanding how larger Ozarks streams store sediment and how they have responded to post-settlement land use changes. Similarly, research in more heavily mined basins, such as the Spring River near Joplin, the Big River within the Old Lead Belt, and other parts of the country, would further increase the understanding of how mining has affected the fluvial geomorphic history of streams.

The biological impact of Zn in the sediment along lower Pearson Creek is unknown. Zn is essential for the healthy development of many plant and animal species, however, at the levels observed in this study, it could be toxic if present in a form that makes it readily bioavailable. A survey of Zn in biota present within and around the channels could help determine to what extent the system is being affected.

## **Conclusions**

Analysis of physical and geochemical data from floodplains along lower Pearson Creek yields the following final conclusions:

- (1) Historical mining practices have resulted in extensive Zn pollution. Zn is present in concentrations from 18 ppm up to 12,395 ppm, has a mean value of 600 ppm, and exceeds background levels in 70% of the samples. Over 33% of the floodplain samples evaluated are greater than 459 ppm, the Probable Effects Concentration determined by MacDonald et al. (2000). Approximately 90.9 Mg

of Zn, 22.3 Mg of Pb, and 140,883 Mg of contaminated sediment is stored along lower Pearson. Channel Fill assemblages are the site of the most storage with approximately 50% of the total Zn (51.1 Mg) and 55% of the total Pb (12.2 Mg) present within them. Furthermore, approximately 33% of the Zn (29.8 Mg) and 26% of the Pb (5.9 Mg) stored in the entire study area is located within the Channel Fill assemblage in Zone I alone.

- (2) Elevation and distance away from the channel and distance downstream are major controlling factors in the distribution of Zn in floodplains. An inverse relationship exists between Zn concentration and surface elevation above the thalweg. This indicates that flood frequency has limited the distribution of Zn.
- (3) Past land use changes elevated sedimentation rates along Pearson Creek. Sedimentation rates were highest during the mining period (mean= 2.20 cm/yr) and decreased during the post-mining period (mean= 0.64 cm/yr). Soil loss from agricultural fields magnified the mining signal by mixing with mining-related sediment, thereby creating the illusion that high sedimentation rates during the mining period were solely due to mining practices. Furthermore, the decreased sedimentation rates following the mining period are likely the combined result of land use change from row crop farming to pasture farming and the implementation of better soil management practices.

Pollutants introduced into streams are affected by hydrologic and geomorphologic processes that disperse contaminated sediment along channels and on floodplains. The impact of land use changes has been shown to increase upland erosion, sediment yields, and downstream channel and floodplain sedimentation. Pearson Creek has undergone

extensive sedimentation and channel changes since the mining period began and has incorporated mining-related metals into its floodplain deposits. The dynamic nature of fluvial systems warrants exploration into how these pollutants might be remobilized in the future. Further research is needed to better understand the source of the contamination and assess the potential threat to residents in the area.

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## APPENDICES

### Appendix A. Sample Attributes

Appendix A-1. Latitude and Longitude of locations.

| Site | Tape<br>(m) | Latitude<br>DD | Longitude<br>DD |
|------|-------------|----------------|-----------------|
| 1A   | 39.6        | 37.17145       | -93.19666       |
| 1A   | 51.0        | 37.17149       | -93.19684       |
| 1A   | 60.3        | 37.17149       | -93.19696       |
| 1A   | 82.0        | 37.17151       | -93.19719       |
| 1A   | 102.0       | 37.17152       | -93.19742       |
| 1A   | 107.5       | 37.17152       | -93.19744       |
| 1B   | 38.3        | 37.17077       | -93.19676       |
| 1B   | 68.0        | 37.17079       | -93.19710       |
| 1B   | 107.0       | 37.17081       | -93.19753       |
| 2    | 66.0        | 37.16937       | -93.19612       |
| 2    | 91.0        | 37.16928       | -93.19644       |
| 2    | 102.9       | 37.16924       | -93.19654       |
| 3A   | 36.4        | 37.16852       | -93.19555       |
| 3A   | 58.0        | 37.16838       | -93.19573       |
| 3A   | 91.5        | 37.16815       | -93.19598       |
| 3A   | 108.5       | 37.16804       | -93.19611       |
| 3B   | 11.0        | 37.16793       | -93.19507       |
| 3B   | 30.2        | 37.16789       | -93.19528       |
| 3B   | 48.0        | 37.16786       | -93.19549       |
| 3B   | 77.0        | 37.16781       | -93.19580       |
| 4A   | 7.0         | 37.16734       | -93.19558       |
| 4A   | 25.5        | 37.16750       | -93.19550       |
| 4A   | 36.0        | 37.16756       | -93.19539       |
| 4A   | 49.0        | 37.16768       | -93.19535       |
| 4B   | 29.5        | 37.16758       | -93.19591       |
| 4C   | 13.0        | 37.16735       | -93.19603       |
| 4D   | 0.0         | 37.16643       | -93.19584       |
| 4D   | 33.0        | 37.16643       | -93.19621       |
| 4D   | 47.0        | 37.16644       | -93.19636       |
| 5    | 0.0         | 37.16582       | -93.19555       |
| 5    | 50.0        | 37.16584       | -93.19612       |
| 5    | 103.0       | 37.16575       | -93.19671       |
| 6    | 28.0        | 37.16517       | -93.19620       |

Appendix A-1 Continued. Latitude and Longitude of locations.

| Site           | Tape<br>(m) | Latitude<br>DD | Longitude<br>DD |
|----------------|-------------|----------------|-----------------|
| 6              | 61.0        | 37.16509       | -93.19657       |
| 6              | 76.1        | 37.16502       | -93.19672       |
| BG1            | 2.3         | 37.23332       | -93.15394       |
| BG2            | 3           | 37.22263       | -93.17068       |
| BG3            | -           | 37.20719       | -93.19823       |
| Cutbank DS 1B  | -           | 37.16996       | -93.19711       |
| Drape DS 1B    | -           | 37.17060       | -93.19764       |
| ~5m US of 4B   | -           | 37.16755       | -93.19586       |
| Tailings Trib. | -           | 37.16822       | -93.19173       |
| Tailings Pile  | -           | 37.16825       | -93.19157       |

Appendix A-2. Sample properties.

| Sample | Site           | Tape<br>(m) | Depth (cm) |     | Munsell Color |
|--------|----------------|-------------|------------|-----|---------------|
|        |                |             | Min        | Max |               |
| PC 1   | 4C             | -           | 0          | 0   | -             |
| PC 2*  | 4C             | 13          | 0          | 12  | -             |
| PC 3*  | 4C             | 13          | 12         | 30  | -             |
| PC 4*  | 4C             | 13          | 30         | 45  | -             |
| PC 5*  | 4C             | 13          | 45         | 65  | -             |
| PC 6*  | 4C             | 13          | 65         | 80  | -             |
| PC 7*  | 4C             | 13          | 80         | 100 | -             |
| PC 8*  | 4C             | 13          | 100        | 120 | -             |
| PC 9   | ~5m US of 4B   | -           | 0          | 0   | -             |
| PC 10  | Tailings Trib. | -           | 0          | 0   | -             |
| PC 11  | Tailings Trib. | -           | 0          | 0   | -             |
| PC 12  | Tailings Pile  | -           | 0          | 0   | -             |
| PC 13  | Tailings Pile  | -           | 0          | 0   | -             |
| PC 14  | 1B             | 107         | 0          | 8   | 10 YR 3/2     |
| PC 15  | 1B             | 107         | 8          | 18  | 7.5 YR 3/3    |
| PC 16  | 1B             | 107         | 18         | 30  | 7.5 YR 3/3    |
| PC 17  | 1B             | 107         | 30         | 40  | 7.5 YR 3/3    |
| PC 18  | 1B             | 107         | 40         | 55  | 10 YR 3/2     |
| PC 19  | 1B             | 107         | 55         | 70  | 10 YR 3/2     |
| PC 20  | 1B             | 107         | 70         | 83  | 7.5 YR 3/3    |
| PC 21  | 1B             | 107         | 83         | 96  | 7.5 YR 3/3    |
| PC 22  | 1B             | 107         | 96         | 116 | 7.5 YR 3/3    |
| PC 23  | 1B             | 107         | 116        | 136 | 7.5 YR 3/3    |
| PC 24  | 1B             | 107         | 136        | 157 | 7.5 YR 3/3    |
| PC 25  | 1B             | 107         | 157        | 183 | Gleyed        |
| PC 26  | 1B             | 107         | 183        | 203 | Gleyed        |
| PC 27  | 1B             | 38.3        | 0          | 10  | 10 YR 3/3     |
| PC 28  | 1B             | 38.3        | 10         | 20  | 10 YR 3/3     |
| PC 29  | 1B             | 38.3        | 20         | 30  | 10 YR 3/3     |
| PC 30  | 1B             | 38.3        | 30         | 45  | 7.5 YR 3/3    |
| PC 31  | 1B             | 38.3        | 45         | 60  | 7.5 YR 3.3    |
| PC 32  | 1B             | 38.3        | 60         | 70  | 10 YR 4/3     |
| PC 33  | 1B             | 38.3        | 70         | 85  | 10 YR 3/3     |
| PC 34  | 1B             | 38.3        | 85         | 100 | 10 YR 3/3     |
| PC 35  | 1B             | 38.3        | 100        | 120 | 10 YR 3/3     |
| PC 36  | 1B             | 38.3        | 120        | 140 | 10 YR 3/3     |
| PC 37  | 1B             | 38.3        | 140        | 160 | 10 YR 3/3     |
| PC 38  | 1B             | 38.3        | 160        | 183 | 10 YR 3/3     |
| PC 39  | 2              | 66          | 0          | 10  | 10 YR 3/3     |

\* Not used in study



Appendix A-2 Continued. Sample properties.

| Sample | Site | Tape<br>(m) | Depth (cm) |     | Munsell Color |
|--------|------|-------------|------------|-----|---------------|
|        |      |             | Min        | Max |               |
| PC 40  | 2    | 66          | 10         | 20  | 10 YR 3/3     |
| PC 41  | 2    | 66          | 20         | 30  | 10 YR 3/3     |
| PC 42  | 2    | 66          | 30         | 50  | 7.5 YR 4/3    |
| PC 43  | 2    | 66          | 50         | 70  | 7.5 YR 4/4    |
| PC 44  | 2    | 66          | 70         | 90  | 7.5 YR 4/4    |
| PC 45  | 2    | 66          | 90         | 102 | 7.5 YR 4/4    |
| PC 46  | 2    | 102.9       | 0          | 7   |               |
| PC 47  | 2    | 102.9       | 7          | 20  |               |
| PC 48  | 2    | 102.9       | 20         | 35  |               |
| PC 49  | 2    | 102.9       | 35         | 50  |               |
| PC 50  | 2    | 102.9       | 50         | 62  |               |
| PC 51  | 2    | 102.9       | 62         | 74  |               |
| PC 52  | 2    | 102.9       | 74         | 86  |               |
| PC 53  | 2    | 102.9       | 86         | 98  |               |
| PC 54  | 2    | 102.9       | 98         | 110 |               |
| PC 55  | 2    | 102.9       | 110        | 135 |               |
| PC 56  | 2    | 102.9       | 135        | 160 |               |
| PC 57  | 2    | 102.9       | 160        | 193 |               |
| PC 58  | 2    | 102.9       | 193        | 226 |               |
| PC 59  | 2    | 102.9       | 226        | 256 |               |
| PC 60  | 5    | 0           | 0          | 15  | 10 YR 4/3     |
| PC 61  | 5    | 0           | 15         | 28  | 10 YR 4/3     |
| PC 62  | 5    | 0           | 28         | 50  | 10 YR 4/4     |
| PC 63  | 5    | 0           | 50         | 70  | 10 YR 4/4     |
| PC 64  | 5    | 0           | 70         | 85  | 10 YR 4/4     |
| PC 65  | 5    | 0           | 85         | 110 | 10 YR 4/4     |
| PC 66  | 5    | 0           | 110        | 132 | 10 YR 4/4     |
| PC 67  | 5    | 0           | 132        | 150 | Gravel        |
| PC 68  | 5    | 50          | 0          | 12  | 10 YR 3/2     |
| PC 69  | 5    | 50          | 12         | 22  | 10 YR 3/2     |
| PC 70  | 5    | 50          | 22         | 34  | 10 YR 3/3     |
| PC 71  | 5    | 50          | 34         | 45  | 10 YR 3/3     |
| PC 72  | 5    | 50          | 45         | 60  | 10 YR 3/3     |
| PC 73  | 5    | 50          | 60         | 80  | 10 YR 3/3     |
| PC 74  | 5    | 50          | 80         | 100 | 10 YR 3/3     |
| PC 75  | 5    | 50          | 100        | 115 | 10 YR 3/3     |
| PC 76  | 5    | 50          | 115        | 130 | 10 YR 3/3     |
| PC 77  | 5    | 50          | 130        | 150 | 10 YR 3/2     |
| PC 78  | 5    | 50          | 150        | 170 | 10 YR 3/2     |
| PC 79  | 5    | 50          | 170        | 190 | 7.5 YR 3/2    |

Appendix A-2 Continued. Sample properties.

| Sample | Site | Tape<br>(m) | Depth (cm) |     | Munsell Color |
|--------|------|-------------|------------|-----|---------------|
|        |      |             | Min        | Max |               |
| PC 80  | 5    | 50          | 190        | 220 | 7.5 YR 3/2    |
| PC 81  | 5    | 50          | 220        | 250 | Gleyed        |
| PC 82  | 5    | 50          | 250        | 270 | Gleyed        |
| PC 83  | 5    | 50          | 270        | 293 | Gleyed        |
| PC 84  | 5    | 103         | 0          | 10  |               |
| PC 85  | 5    | 103         | 10         | 20  |               |
| PC 86  | 5    | 103         | 20         | 39  |               |
| PC 87  | 5    | 103         | 39         | 63  |               |
| PC 88  | 5    | 103         | 63         | 76  |               |
| PC 89  | 5    | 103         | 76         | 90  |               |
| PC 90  | 5    | 103         | 90         | 105 |               |
| PC 91  | 5    | 103         | 105        | 120 |               |
| PC 92  | 5    | 103         | 120        | 130 |               |
| PC 93  | 5    | 103         | 130        | 150 |               |
| PC 94  | 5    | 103         | 150        | 170 |               |
| PC 95  | 5    | 103         | 170        | 190 |               |
| PC 96  | 5    | 103         | 190        | 210 |               |
| PC 97  | 5    | 103         | 210        | 225 |               |
| PC 98  | 1A   | 39.6        | 0          | 15  |               |
| PC 99  | 1A   | 39.6        | 15         | 30  |               |
| PC 100 | 1A   | 39.6        | 30         | 46  |               |
| PC 101 | 1A   | 107.5       | 0          | 15  |               |
| PC 102 | 1A   | 107.5       | 15         | 30  |               |
| PC 103 | 1A   | 107.5       | 30         | 45  |               |
| PC 104 | 1A   | 107.5       | 45         | 60  |               |
| PC 105 | 1A   | 107.5       | 60         | 75  |               |
| PC 106 | 1A   | 107.5       | 75         | 90  |               |
| PC 107 | 1A   | 107.5       | 90         | 105 |               |
| PC 108 | 1A   | 107.5       | 105        | 130 |               |
| PC 109 | 1A   | 107.5       | 130        | 150 |               |
| PC 110 | 1A   | 107.5       | 150        | 170 |               |
| PC 111 | 1A   | 107.5       | 170        | 190 |               |
| PC 112 | 1A   | 107.5       | 190        | 210 |               |
| PC 113 | 1A   | 107.5       | 210        | 235 |               |
| PC 114 | 3A   | 36.4        | 0          | 10  |               |
| PC 115 | 3A   | 36.4        | 10         | 25  |               |
| PC 116 | 3A   | 36.4        | 25         | 40  |               |
| PC 117 | 3A   | 36.4        | 40         | 55  |               |
| PC 118 | 3A   | 36.4        | 55         | 75  |               |
| PC 119 | 3A   | 36.4        | 75         | 90  |               |

Appendix A-2 Continued. Sample properties.

| Sample | Site | Tape<br>(m) | Depth (cm) |     | Munsell Color |
|--------|------|-------------|------------|-----|---------------|
|        |      |             | Min        | Max |               |
| PC 120 | 3A   | 58          | 0          | 10  |               |
| PC 121 | 3A   | 58          | 10         | 25  |               |
| PC 122 | 3A   | 58          | 25         | 40  |               |
| PC 123 | 3A   | 58          | 40         | 55  |               |
| PC 124 | 3A   | 58          | 55         | 70  |               |
| PC 125 | 3A   | 58          | 70         | 85  |               |
| PC 126 | 3A   | 58          | 85         | 100 |               |
| PC 127 | 3A   | 58          | 100        | 125 |               |
| PC 128 | 3A   | 58          | 125        | 140 |               |
| PC 129 | 3A   | 58          | 140        | 160 | Gleyed        |
| PC 130 | 3A   | 58          | 160        | 180 | Gleyed        |
| PC 131 | 3A   | 58          | 180        | 200 | Gleyed        |
| PC 132 | 3A   | 58          | 200        | 220 | Gleyed        |
| PC 133 | 3A   | 58          | 220        | 232 | Gleyed        |
| PC 134 | 3B   | 30.2        | 0          | 15  |               |
| PC 135 | 3B   | 30.2        | 15         | 30  |               |
| PC 136 | 3B   | 30.2        | 30         | 45  |               |
| PC 137 | 3B   | 30.2        | 45         | 66  |               |
| PC 138 | 3B   | 30.2        | 66         | 90  |               |
| PC 139 | 3B   | 30.2        | 90         | 110 |               |
| PC 140 | 3B   | 30.2        | 110        | 130 |               |
| PC 141 | 3B   | 30.2        | 130        | 152 |               |
| PC 142 | 3B   | 30.2        | 152        | 170 |               |
| PC 143 | 3B   | 30.2        | 170        | 185 |               |
| PC 144 | 3B   | 30.2        | 185        | 200 |               |
| PC 145 | 3B   | 30.2        | 200        | 217 |               |
| PC 146 | 3B   | 30.2        | 217        | 235 |               |
| PC 147 | 3B   | 30.2        | 235        | 255 |               |
| PC 148 | 3B   | 30.2        | 255        | 270 |               |
| PC 149 | 3B   | 30.2        | 270        | 285 |               |
| PC 150 | 3B   | 77          | 0          | 12  |               |
| PC 151 | 3B   | 77          | 12         | 35  |               |
| PC 152 | 3B   | 77          | 35         | 55  |               |
| PC 153 | 3B   | 77          | 55         | 75  |               |
| PC 154 | 3B   | 77          | 75         | 95  |               |
| PC 155 | 3B   | 77          | 95         | 115 |               |
| PC 156 | 3B   | 77          | 115        | 128 |               |
| PC 157 | 3B   | 77          | 128        | 140 |               |
| PC 158 | 3B   | 77          | 140        | 155 |               |
| PC 159 | 3B   | 77          | 155        | 175 |               |

Appendix A-2 Continued. Sample properties.

| Sample | Site | Tape<br>(m) | Depth (cm) |     | Munsell Color |
|--------|------|-------------|------------|-----|---------------|
|        |      |             | Min        | Max |               |
| PC 160 | 3B   | 77          | 175        | 201 |               |
| PC 161 | 4A   | 7           | 0          | 14  | 10YR 4/3      |
| PC 162 | 4A   | 7           | 14         | 30  | 10YR 4/3      |
| PC 163 | 4A   | 7           | 30         | 50  | 10YR 4/3      |
| PC 164 | 4A   | 7           | 50         | 70  | 10YR 4/3      |
| PC 165 | 4A   | 7           | 70         | 90  | 10YR 4/3      |
| PC 166 | 4A   | 7           | 90         | 110 | 10YR 4/3      |
| PC 167 | 4A   | 7           | 110        | 130 | 10YR 4/3      |
| PC 168 | 4A   | 7           | 130        | 158 | 10YR 4/3      |
| PC 169 | 4A   | 7           | 158        | 180 | 10YR 4/4      |
| PC 170 | 4A   | 7           | 180        | 205 | 10YR 4/4      |
| PC 171 | 4A   | 7           | 205        | 225 | 10YR 3/6      |
| PC 172 | 4A   | 7           | 225        | 248 | 10YR 3/6      |
| PC 173 | 4A   | 25.5        | 0          | 15  | 10YR 4/3      |
| PC 174 | 4A   | 25.5        | 15         | 25  | 10YR 4/4      |
| PC 175 | 4A   | 25.5        | 25         | 35  | 10YR 4/4      |
| PC 176 | 4A   | 25.5        | 35         | 45  | 10YR 4/4      |
| PC 177 | 4A   | 25.5        | 45         | 55  | 10YR 4/4      |
| PC 178 | 4A   | 25.5        | 55         | 74  | 10YR 4/4      |
| PC 179 | 4A   | 25.5        | 74         | 90  | 10YR 4/3      |
| PC 180 | 4A   | 25.5        | 90         | 110 | 10YR 4/3      |
| PC 181 | 4A   | 25.5        | 110        | 127 | 10YR 4/3      |
| PC 182 | 4A   | 25.5        | 127        | 145 | 10YR 3/3      |
| PC 183 | 4A   | 25.5        | 145        | 165 | 10YR 3/3      |
| PC 184 | 4A   | 25.5        | 165        | 185 | 10YR 3/3      |
| PC 185 | 4A   | 25.5        | 185        | 197 | 10YR 3/3      |
| PC 186 | 4A   | 25.5        | 197        | 225 | 10YR 3/1      |
| PC 187 | 4A   | 25.5        | 225        | 250 | 10YR 3/1      |
| PC 188 | 4A   | 25.5        | 250        | 275 | 10YR 3/1      |
| PC 189 | 4A   | 25.5        | 275        | 306 | 10YR 3/1      |
| PC 190 | 4B   | 29.5        | 0          | 14  | 10YR 3/3      |
| PC 191 | 4B   | 29.5        | 14         | 30  | 7.5YR 3/3     |
| PC 192 | 4B   | 29.5        | 30         | 45  | 7.5YR 3/3     |
| PC 193 | 4B   | 29.5        | 45         | 61  | 7.5YR 3/3     |
| PC 194 | 4B   | 29.5        | 61         | 80  | 7.5YR 3/3     |
| PC 195 | 4B   | 29.5        | 80         | 92  | 7.5YR 3/3     |
| PC 196 | 4B   | 29.5        | 92         | 107 | 7.5YR 3/3     |
| PC 197 | 4B   | 29.5        | 107        | 125 | 7.5YR 3/3     |
| PC 198 | 4B   | 29.5        | 125        | 140 | 7.5YR 3/3     |
| PC 199 | 4B   | 29.5        | 140        | 155 | 7.5YR 3/3     |

Appendix A-2 Continued. Sample properties.

| Sample | Site | Tape<br>(m) | Depth (cm) |     | Munsell Color     |
|--------|------|-------------|------------|-----|-------------------|
|        |      |             | Min        | Max |                   |
| PC 200 | 4B   | 29.5        | 155        | 170 | 7.5YR 3/3         |
| PC 201 | 4B   | 29.5        | 170        | 190 | 7.5YR 3/3         |
| PC 202 | 4B   | 29.5        | 190        | 210 | 7.5YR 4/3         |
| PC 203 | 4B   | 29.5        | 210        | 230 | 7.5YR 4/3         |
| PC 204 | 4B   | 29.5        | 230        | 275 | 7.5YR 4/3         |
| PC 205 | 4C   | 13          | 0          | 16  | 10YR 3/3          |
| PC 206 | 4C   | 13          | 16         | 26  | 7.5YR 3/3         |
| PC 207 | 4C   | 13          | 26         | 37  | 7.5YR 3/3         |
| PC 208 | 4C   | 13          | 37         | 49  | 7.5YR 4/2         |
| PC 209 | 4C   | 13          | 49         | 61  | 7.5YR 4/3         |
| PC 210 | 4C   | 13          | 61         | 74  | 7.5YR 4/3         |
| PC 211 | 4C   | 13          | 74         | 91  | 7.5YR 4/2         |
| PC 212 | 4C   | 13          | 91         | 105 | 7.5YR 3/3         |
| PC 213 | 4C   | 13          | 105        | 122 | 7.5YR 3/3         |
| PC 214 | 4C   | 13          | 122        | 140 | 10YR 3/2          |
| PC 215 | 4C   | 13          | 140        | 163 | 10YR 3/2          |
| PC 216 | 4C   | 13          | 163        | 180 | 7.5YR 3/2         |
| PC 217 | 4C   | 13          | 180        | 200 | 7.5YR 3/2         |
| PC 218 | 4C   | 13          | 200        | 234 | 7.5YR 3/2         |
| PC 219 | 4C   | 13          | 234        | 265 | Gleyed            |
| PC 220 | 4C   | 13          | 265        | 292 | Gleyed            |
| PC 221 | 6    | 28          | 0          | 13  | 10YR 3/2          |
| PC 222 | 6    | 28          | 13         | 30  | 10YR 3/3          |
| PC 223 | 6    | 28          | 30         | 45  | 10YR 3/3          |
| PC 224 | 6    | 28          | 45         | 60  | 10YR 3/3          |
| PC 225 | 6    | 28          | 60         | 80  | 10YR 3/3          |
| PC 226 | 6    | 28          | 80         | 100 | 10YR 3/3          |
| PC 227 | 6    | 28          | 100        | 120 | 10YR 3/3          |
| PC 228 | 6    | 28          | 120        | 137 | 10YR 3/3          |
| PC 229 | 6    | 28          | 137        | 162 | 7.5YR 3/3         |
| PC 230 | 6    | 61          | 0          | 16  | 10YR 3/3          |
| PC 231 | 6    | 61          | 16         | 30  | 10YR 3/3          |
| PC 232 | 6    | 61          | 30         | 45  | 10YR 3/3          |
| PC 233 | 6    | 61          | 45         | 60  | 10YR 3/3          |
| PC 234 | 6    | 61          | 60         | 75  | 10YR 3/3          |
| PC 235 | 6    | 61          | 75         | 90  | 10YR 3/3          |
| PC 236 | 6    | 61          | 90         | 110 | 10YR 3/3          |
| PC 237 | 6    | 61          | 110        | 120 | 10YR 4/2 10YR 3/3 |
| PC 238 | 6    | 61          | 120        | 130 | 10YR 4/2 10YR 3/3 |
| PC 239 | 6    | 61          | 130        | 142 | 10YR 4/2 10YR 3/3 |

Appendix A-2 Continued. Sample properties.

| Sample | Site | Tape<br>(m) | Depth (cm) |     | Munsell Color        |
|--------|------|-------------|------------|-----|----------------------|
|        |      |             | Min        | Max |                      |
| PC 240 | 6    | 61          | 142        | 155 | 10YR 3/3   4/6   2/2 |
| PC 241 | 6    | 61          | 155        | 170 | 10YR 3/3   4/6   2/2 |
| PC 242 | 6    | 61          | 170        | 190 | 10YR 3/3   4/6   2/2 |
| PC 243 | 6    | 61          | 190        | 210 | 10YR 3/3   4/6   2/2 |
| PC 244 | 6    | 61          | 210        | 230 | 10YR 3/3   4/6   2/2 |
| PC 245 | 6    | 61          | 230        | 250 | 10YR 3/3   4/6   2/2 |
| PC 246 | 6    | 61          | 250        | 262 | Gleyed               |
| PC 247 | 6    | 61          | 262        | 282 | Gleyed               |
| PC 248 | 6    | 61          | 282        | 302 | Gleyed               |
| PC 249 | 6    | 61          | 302        | 321 | Gleyed               |
| PC 250 | 6    | 76.1        | 0          | 10  | 10YR 3/2             |
| PC 251 | 6    | 76.1        | 10         | 25  | 10YR 3/3             |
| PC 252 | 6    | 76.1        | 25         | 40  | 10YR 3/3             |
| PC 253 | 6    | 76.1        | 40         | 55  | 10YR 3/3             |
| PC 254 | 6    | 76.1        | 55         | 67  | 10YR 3/3             |
| PC 255 | 6    | 76.1        | 67         | 90  | 10YR 3/3             |
| PC 256 | 6    | 76.1        | 90         | 110 | 10YR 3/3             |
| PC 257 | 6    | 76.1        | 110        | 125 | 10YR 3/3             |
| PC 258 | 6    | 76.1        | 125        | 140 | 10YR 3/3             |
| PC 259 | 4C   | -           | -          | -   | -                    |
| PC 260 | 1A   | 39.6        | 0          | 36  | 10YR 3/3             |
| PC 261 | 1A   | 39.6        | 36         | 88  | 10YR 3/3             |
| PC 262 | 1A   | 51          | 0          | 23  | 10YR 3/2             |
| PC 263 | 1A   | 51          | 23         | 43  | 10YR 3/2             |
| PC 264 | 1A   | 60.3        | 0          | 30  | 10YR 3/2             |
| PC 265 | 1A   | 60.3        | 30         | 48  | 10YR 3/2             |
| PC 266 | 1A   | 82          | 0          | 34  | 10YR 3/2             |
| PC 267 | 1A   | 82          | 34         | 66  | 10YR 3/2             |
| PC 268 | 1A   | 82          | 66         | 85  | 10YR 3/3             |
| PC 269 | 1A   | 102         | 0          | 24  | 10YR 3/3             |
| PC 270 | 1A   | 102         | 24         | 57  | 10YR 3/2             |
| PC 271 | 1B   | 68          | 0          | 15  | 10YR 3/2             |
| PC 272 | 1B   | 68          | 15         | 34  | 10YR 3/2             |
| PC 273 | 1B   | 68          | 34         | 50  | 10YR 3/3             |
| PC 274 | 1B   | 68          | 50         | 66  | 10YR 3/3             |
| PC 275 | 2    | 91          | 0          | 16  | 10YR 3/2             |
| PC 276 | 2    | 91          | 16         | 30  | 10YR 3/2             |
| PC 277 | 2    | 91          | 30         | 45  | 10YR 3/2             |
| PC 278 | 2    | 91          | 45         | 58  | 10YR 3/2             |
| PC 279 | 2    | 91          | 58         | 75  | 10YR 4/3             |

Appendix A-2 Continued. Sample properties.

| Sample | Site | Tape<br>(m) | Depth (cm) |     | Munsell Color |
|--------|------|-------------|------------|-----|---------------|
|        |      |             | Min        | Max |               |
| PC 280 | 2    | 91          | 75         | 90  | 10YR 4/3      |
| PC 281 | 2    | 91          | 90         | 105 | 10YR 4/3      |
| PC 282 | 2    | 91          | 105        | 120 | 10YR 4/3      |
| PC 283 | 2    | 91          | 120        | 137 | 10YR 4/3      |
| PC 284 | 2    | 91          | 137        | 165 | Gleyed        |
| PC 285 | 2    | 91          | 165        | 190 | Gleyed        |
| PC 286 | 3A   | 91.5        | 0          | 15  | 10YR 3/2      |
| PC 287 | 3A   | 91.5        | 15         | 30  | 10YR 3/3      |
| PC 288 | 3A   | 91.5        | 30         | 50  | 10YR 3/3      |
| PC 289 | 3A   | 91.5        | 50         | 70  | 10YR 3/2      |
| PC 290 | 3A   | 91.5        | 70         | 90  | 10YR 3/2      |
| PC 291 | 3A   | 91.5        | 90         | 110 | 10YR 3/2      |
| PC 292 | 3A   | 91.5        | 110        | 130 | 10YR 3/2      |
| PC 293 | 3A   | 91.5        | 130        | 160 | 10YR 3/2      |
| PC 294 | 3A   | 91.5        | 160        | 185 | 10YR 3/2      |
| PC 295 | 3A   | 91.5        | 185        | 215 | 10YR 3/2      |
| PC 296 | 3A   | 91.5        | 215        | 235 | 10YR 3/2      |
| PC 297 | 3A   | 91.5        | 235        | 255 | Gleyed        |
| PC 298 | 3A   | 91.5        | 255        | 275 | Gleyed        |
| PC 299 | 3A   | 91.5        | 275        | 299 | Gleyed        |
| PC 300 | 3A   | 108.5       | 0          | 15  | 10YR 3/2      |
| PC 301 | 3A   | 108.5       | 15         | 37  | 7.5YR 3/2     |
| PC 302 | 3A   | 108.5       | 37         | 63  | 7.5YR 3/2     |
| PC 303 | 3A   | 108.5       | 63         | 98  | 10YR 3/2      |
| PC 304 | 3A   | 108.5       | 98         | 130 | 10YR 3/2      |
| PC 305 | 3A   | 108.5       | 130        | 160 | 10YR 3/2      |
| PC 306 | 3A   | 108.5       | 160        | 191 | 10YR 3/2      |
| PC 307 | 3B   | 11          | 0          | 15  | 10YR 3/2      |
| PC 308 | 3B   | 11          | 15         | 33  | 10YR 3/2      |
| PC 309 | 3B   | 11          | 33         | 48  | 10YR 3/3      |
| PC 310 | 3B   | 11          | 48         | 66  | 7.5YR 4/3     |
| PC 311 | 3B   | 11          | 66         | 78  | 7.5YR 4/3     |
| PC 312 | 3B   | 11          | 78         | 90  | 7.5YR 4/3     |
| PC 313 | 3B   | 49          | 0          | 15  | 10YR 3/2      |
| PC 314 | 3B   | 49          | 15         | 30  | 10YR 3/2      |
| PC 315 | 3B   | 49          | 30         | 45  | 10YR 3/2      |
| PC 316 | 3B   | 49          | 45         | 60  | 10YR 3/2      |
| PC 317 | 3B   | 49          | 60         | 75  | 10YR 3/2      |
| PC 318 | 3B   | 49          | 75         | 90  | 10YR 3/2      |
| PC 319 | 3B   | 49          | 90         | 105 | 10YR 3/2      |

Appendix A-2 Continued. Sample properties.

| Sample | Site          | Tape<br>(m) | Depth (cm) |     | Munsell Color |
|--------|---------------|-------------|------------|-----|---------------|
|        |               |             | Min        | Max |               |
| PC 320 | 3B            | 49          | 105        | 120 | 10YR 3/2      |
| PC 321 | 3B            | 49          | 120        | 133 | 10YR 3/2      |
| PC 322 | 3B            | 49          | 133        | 158 | 10YR 3/2      |
| PC 323 | 3B            | 49          | 158        | 175 | 10YR 3/2      |
| PC 324 | 3B            | 49          | 175        | 191 | Gleyed        |
| PC 325 | Cutbank DS 1B | -           | 0          | 30  | -             |
| PC 326 | Cutbank DS 1B | -           | 30         | 45  | -             |
| PC 327 | Cutbank DS 1B | -           | 45         | 55  | -             |
| PC 328 | Cutbank DS 1B | -           | 55         | 70  | -             |
| PC 329 | Cutbank DS 1B | -           | 70         | 85  | -             |
| PC 330 | Cutbank DS 1B | -           | 85         | 100 | -             |
| PC 331 | Cutbank DS 1B | -           | 100        | 115 | -             |
| PC 332 | Drape DS 1B   | -           | 0          | 10  | 10YR 3/2      |
| PC 333 | Drape DS 1B   | -           | 10         | 25  | 7.5YR 3/2     |
| PC 334 | Drape DS 1B   | -           | 25         | 40  | 7.5YR 3/2     |
| PC 335 | Drape DS 1B   | -           | 40         | 60  | 7.5YR 3/2     |
| PC 336 | Drape DS 1B   | -           | 60         | 85  | 10YR 3/2      |
| PC 337 | Drape DS 1B   | -           | 85         | 110 | 10YR 3/2      |
| PC 338 | Drape DS 1B   | -           | 110        | 130 | Gleyed        |
| PC 339 | Drape DS 1B   | -           | 130        | 160 | Gleyed        |
| PC 340 | Drape DS 1B   | -           | 160        | 192 | Gleyed        |
| PC 341 | 4A            | 36          | 0          | 25  | 7.5YR 3/2     |
| PC 342 | 4A            | 36          | 25         | 50  | 7.5YR 3/2     |
| PC 343 | 4A            | 36          | 50         | 75  | 10YR 4/1      |
| PC 344 | 4A            | 36          | 75         | 100 | 10YR 4/1      |
| PC 345 | 4A            | 49          | 0          | 25  | 7.5YR 3/2     |
| PC 346 | 4A            | 49          | 25         | 50  | 10YR 3/2      |
| PC 347 | 4A            | 49          | 50         | 75  | 10YR 3/2      |
| PC 348 | 4A            | 49          | 75         | 100 | 10YR 3/2      |
| PC 349 | 4D            | 0           | 0          | 15  | 10YR 3/2      |
| PC 350 | 4D            | 0           | 15         | 30  | 7.5/10YR 3/2  |
| PC 351 | 4D            | 0           | 30         | 45  | 7.5/10YR 3/2  |
| PC 352 | 4D            | 0           | 45         | 60  | 7.5/10YR 3/2  |
| PC 353 | 4D            | 0           | 60         | 75  | 7.5/10YR 3/2  |
| PC 354 | 4D            | 0           | 75         | 90  | 7.5/10YR 3/2  |
| PC 355 | 4D            | 0           | 90         | 105 | 7.5/10YR 3/2  |
| PC 356 | 4D            | 0           | 105        | 120 | 7.5/10YR 3/2  |
| PC 357 | 4D            | 0           | 120        | 135 | 7.5/10YR 3/2  |
| PC 358 | 4D            | 0           | 135        | 160 | 7.5/10YR 3/2  |
| PC 359 | 4D            | 0           | 160        | 185 | 7.5/10YR 3/2  |



Appendix A-2 Continued. Sample properties.

| Sample | Site | Tape<br>(m) | Depth (cm) |     | Munsell Color |
|--------|------|-------------|------------|-----|---------------|
|        |      |             | Min        | Max |               |
| PC 360 | 4D   | 0           | 185        | 210 | 7.5/10YR 3/2  |
| PC 361 | 4D   | 0           | 210        | 235 | 7.5/10YR 3/2  |
| PC 362 | 4D   | 0           | 235        | 260 | 7.5/10YR 3/2  |
| PC 363 | 4D   | 0           | 260        | 285 | 7.5/10YR 3/2  |
| PC 364 | 4D   | 0           | 285        | 316 | 7.5/10YR 3/2  |
| PC 365 | 4D   | 0           | 316        | 340 | Gleyed        |
| PC 366 | 4D   | 26.6        | 0          | 30  | -             |
| PC 367 | 4D   | 33          | 0          | 25  | 7.5YR 3/2     |
| PC 368 | 4D   | 33          | 25         | 40  | 7.5YR 3/2     |
| PC 369 | 4D   | 33          | 40         | 55  | 7.5YR 3/2     |
| PC 370 | 4D   | 33          | 55         | 70  | 7.5YR 3/2     |
| PC 371 | 4D   | 33          | 70         | 85  | 7.5YR 3/2     |
| PC 372 | 4D   | 33          | 85         | 100 | 7.5YR 3/2     |
| PC 373 | 4D   | 33          | 100        | 122 | 7.5YR 3/2     |
| PC 374 | 4D   | 33          | 122        | 130 | 10YR 3/2      |
| PC 375 | 4D   | 33          | 130        | 150 | 10YR 3/2      |
| PC 376 | 4D   | 33          | 150        | 170 | 10YR 3/2      |
| PC 377 | 4D   | 33          | 170        | 190 | 10YR 3/2      |
| PC 378 | 4D   | 33          | 190        | 220 | 10YR 2/2      |
| PC 379 | 4D   | 33          | 220        | 250 | 10YR 2/2      |
| PC 380 | 4D   | 33          | 250        | 285 | 10YR 2/2      |
| PC 381 | 4D   | 33          | 285        | 305 | 10YR 3/1      |
| PC 382 | 4D   | 33          | 305        | 335 | 10YR 3/1      |
| PC 383 | 4D   | 33          | 335        | 365 | Gleyed        |
| PC 384 | 4D   | 33          | 365        | 405 | Gleyed        |
| PC 385 | 4D   | 47          | 0          | 35  | 10YR 4/3      |
| PC 386 | 4D   | 47          | 35         | 50  | 10YR 4/3      |
| PC 387 | 4D   | 47          | 50         | 65  | 10YR 3/3      |
| PC 388 | 4D   | 47          | 65         | 80  | 10YR 3/2      |
| PC 389 | 4D   | 47          | 80         | 98  | 7.5YR 3/2     |
| PC 390 | BG1  | 2.3         | 0          | 20  | 10YR 4/3      |
| PC 391 | BG1  | 2.3         | 20         | 35  | 10YR 4/3      |
| PC 392 | BG1  | 2.3         | 35         | 50  | 10YR 4/3      |
| PC 393 | BG2  | 3           | 0          | 15  | 10YR 3/2      |
| PC 394 | BG2  | 3           | 15         | 30  | 10YR 3/2      |
| PC 395 | BG2  | 3           | 30         | 45  | 10YR 3/2      |
| PC 396 | BG3  | -           | 0          | 10  | 10YR 4/3      |
| PC 397 | BG3  | -           | 10         | 25  | 10YR 4/3      |
| PC 398 | BG3  | -           | 25         | 40  | 10YR 3/2      |

## Appendix B. Textural Data

Appendix B. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>(<3.9 $\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 1   | 19.30                                      | 63.22                                     | 17.47                                 | 61.9                      | 2.1                                  | 20.4                                 | 199.6                                |
| PC 2*  | 2.97                                       | 75.92                                     | 21.11                                 | 19.38                     | 1.72                                 | 14.79                                | 43.37                                |
| PC 3*  | 3.51                                       | 75.39                                     | 21.10                                 | 19.90                     | 1.72                                 | 15.14                                | 44.73                                |
| PC 4*  | 5.37                                       | 75.30                                     | 19.33                                 | 22.23                     | 1.89                                 | 16.61                                | 50.64                                |
| PC 5*  | 5.32                                       | 77.03                                     | 17.65                                 | 23.05                     | 2.02                                 | 18.56                                | 49.73                                |
| PC 6*  | 24.90                                      | 59.78                                     | 15.31                                 | 73.20                     | 2.44                                 | 26.91                                | 225.08                               |
| PC 7*  | 5.84                                       | 74.13                                     | 20.03                                 | 22.53                     | 1.82                                 | 16.56                                | 50.98                                |
| PC 8*  | 4.80                                       | 73.86                                     | 21.33                                 | 21.12                     | 1.69                                 | 15.46                                | 46.48                                |
| PC 9   | 16.13                                      | 73.68                                     | 10.19                                 | 38.70                     | 3.77                                 | 34.85                                | 74.24                                |
| PC 10  | 53.21                                      | 36.68                                     | 10.11                                 | 428.66                    | 3.82                                 | 90.96                                | 1,128.92                             |
| PC 11  | 64.50                                      | 27.84                                     | 7.65                                  | 533.64                    | 5.55                                 | 518.14                               | 1,249.27                             |
| PC 12  | 28.19                                      | 63.53                                     | 8.28                                  | 65.37                     | 5.03                                 | 42.29                                | 119.62                               |
| PC 13  | 37.34                                      | 53.41                                     | 9.26                                  | 112.67                    | 4.27                                 | 46.64                                | 307.65                               |
| PC 14  | 9.90                                       | 70.28                                     | 19.82                                 | 29.85                     | 1.90                                 | 15.69                                | 62.91                                |
| PC 15  | 4.39                                       | 73.97                                     | 21.65                                 | 20.66                     | 1.73                                 | 13.75                                | 43.26                                |
| PC 16  | 2.07                                       | 74.88                                     | 23.05                                 | 17.58                     | 1.63                                 | 13.11                                | 39.73                                |
| PC 17  | 5.89                                       | 71.71                                     | 22.40                                 | 23.71                     | 1.62                                 | 14.17                                | 47.62                                |
| PC 18  | 1.88                                       | 75.01                                     | 23.11                                 | 17.67                     | 1.56                                 | 13.00                                | 41.14                                |
| PC 19  | 7.31                                       | 71.48                                     | 21.21                                 | 24.01                     | 1.72                                 | 14.34                                | 50.57                                |
| PC 20  | 6.75                                       | 70.43                                     | 22.82                                 | 23.14                     | 1.59                                 | 12.96                                | 49.84                                |
| PC 21  | 4.83                                       | 72.14                                     | 23.03                                 | 20.35                     | 1.59                                 | 12.16                                | 42.96                                |
| PC 22  | 6.53                                       | 72.24                                     | 21.23                                 | 23.55                     | 1.69                                 | 13.12                                | 50.02                                |
| PC 23  | 7.42                                       | 71.93                                     | 20.64                                 | 26.18                     | 1.68                                 | 13.01                                | 52.94                                |
| PC 24  | 7.75                                       | 71.20                                     | 21.05                                 | 24.37                     | 1.62                                 | 12.86                                | 50.44                                |
| PC 25  | 8.34                                       | 71.40                                     | 20.26                                 | 24.75                     | 1.71                                 | 13.70                                | 53.85                                |
| PC 26  | 3.17                                       | 72.73                                     | 24.10                                 | 18.27                     | 1.50                                 | 13.18                                | 41.13                                |
| PC 27  | 14.73                                      | 63.68                                     | 21.59                                 | 45.96                     | 1.76                                 | 15.96                                | 104.87                               |
| PC 28  | 13.92                                      | 63.80                                     | 22.28                                 | 44.71                     | 1.67                                 | 15.65                                | 99.49                                |
| PC 29  | 17.69                                      | 60.80                                     | 21.51                                 | 66.98                     | 1.72                                 | 16.96                                | 211.28                               |
| PC 30  | 16.59                                      | 62.25                                     | 21.16                                 | 55.23                     | 1.73                                 | 17.74                                | 139.65                               |
| PC 31  | 17.09                                      | 63.95                                     | 18.96                                 | 51.77                     | 1.93                                 | 19.58                                | 126.49                               |
| PC 32  | 17.08                                      | 65.46                                     | 17.46                                 | 38.35                     | 2.12                                 | 21.73                                | 94.26                                |
| PC 33  | 9.36                                       | 73.17                                     | 17.46                                 | 26.21                     | 2.07                                 | 19.17                                | 61.48                                |
| PC 34  | 4.85                                       | 75.81                                     | 19.35                                 | 21.13                     | 1.86                                 | 15.95                                | 45.44                                |
| PC 35  | 10.61                                      | 69.98                                     | 19.40                                 | 29.50                     | 1.89                                 | 17.50                                | 66.52                                |
| PC 36  | 6.25                                       | 71.44                                     | 22.30                                 | 24.23                     | 1.63                                 | 14.09                                | 47.87                                |

\* Not used in study

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 37  | 6.28                                       | 69.28                                     | 24.43                                 | 23.54                     | 1.53                                 | 12.32                                | 48.38                                |
| PC 38  | 10.03                                      | 70.42                                     | 19.55                                 | 31.09                     | 1.81                                 | 15.34                                | 63.62                                |
| PC 39  | 5.77                                       | 73.91                                     | 20.33                                 | 20.90                     | 1.87                                 | 14.40                                | 46.62                                |
| PC 40  | 5.24                                       | 74.44                                     | 20.33                                 | 20.46                     | 1.81                                 | 14.15                                | 44.40                                |
| PC 41  | 3.87                                       | 75.56                                     | 20.58                                 | 19.23                     | 1.75                                 | 12.97                                | 41.03                                |
| PC 42  | 3.51                                       | 76.62                                     | 19.87                                 | 18.41                     | 1.73                                 | 12.50                                | 38.85                                |
| PC 43  | 1.53                                       | 76.65                                     | 21.81                                 | 17.10                     | 1.60                                 | 13.66                                | 36.76                                |
| PC 44  | 1.89                                       | 76.40                                     | 21.71                                 | 17.29                     | 1.62                                 | 13.46                                | 36.55                                |
| PC 45  | 1.50                                       | 75.69                                     | 22.80                                 | 16.92                     | 1.55                                 | 12.56                                | 35.03                                |
| PC 46  | 11.24                                      | 70.98                                     | 17.78                                 | 31.70                     | 2.12                                 | 18.27                                | 69.76                                |
| PC 47  | 3.93                                       | 74.34                                     | 21.73                                 | 20.07                     | 1.70                                 | 14.83                                | 45.46                                |
| PC 48  | 3.64                                       | 75.36                                     | 21.00                                 | 20.53                     | 1.70                                 | 16.06                                | 45.38                                |
| PC 49  | 4.98                                       | 74.58                                     | 20.43                                 | 21.22                     | 1.76                                 | 15.82                                | 47.44                                |
| PC 50  | 11.25                                      | 70.96                                     | 17.79                                 | 32.39                     | 2.10                                 | 18.41                                | 69.57                                |
| PC 51  | 7.72                                       | 73.50                                     | 18.78                                 | 24.25                     | 1.95                                 | 17.61                                | 56.74                                |
| PC 52  | 8.54                                       | 73.56                                     | 17.90                                 | 25.81                     | 2.05                                 | 19.59                                | 59.49                                |
| PC 53  | 6.93                                       | 74.53                                     | 18.54                                 | 23.69                     | 1.97                                 | 17.48                                | 54.08                                |
| PC 54  | 5.31                                       | 75.26                                     | 19.43                                 | 21.39                     | 1.86                                 | 15.83                                | 48.55                                |
| PC 55  | 11.85                                      | 70.09                                     | 18.06                                 | 30.16                     | 2.05                                 | 20.05                                | 69.42                                |
| PC 56  | 10.29                                      | 69.19                                     | 20.52                                 | 27.24                     | 1.76                                 | 17.10                                | 64.58                                |
| PC 57  | 9.41                                       | 68.66                                     | 21.93                                 | 27.54                     | 1.66                                 | 16.02                                | 60.89                                |
| PC 58  | 4.76                                       | 70.85                                     | 24.39                                 | 19.71                     | 1.55                                 | 13.16                                | 45.24                                |
| PC 59  | 12.41                                      | 65.69                                     | 21.90                                 | 46.36                     | 1.73                                 | 16.05                                | 84.59                                |
| PC 60  | 3.59                                       | 79.98                                     | 16.43                                 | 22.43                     | 2.18                                 | 19.24                                | 45.10                                |
| PC 61  | 2.81                                       | 80.68                                     | 16.51                                 | 21.69                     | 2.17                                 | 18.84                                | 43.85                                |
| PC 62  | 3.61                                       | 80.88                                     | 15.51                                 | 23.66                     | 2.26                                 | 21.13                                | 46.90                                |
| PC 63  | 6.88                                       | 78.25                                     | 14.87                                 | 29.67                     | 2.38                                 | 22.30                                | 52.62                                |
| PC 64  | 13.48                                      | 72.74                                     | 13.78                                 | 42.74                     | 2.60                                 | 24.39                                | 97.57                                |
| PC 65  | 24.68                                      | 62.68                                     | 12.64                                 | 68.66                     | 2.87                                 | 28.29                                | 218.59                               |
| PC 66  | 36.65                                      | 51.81                                     | 11.54                                 | 103.77                    | 3.21                                 | 35.10                                | 296.36                               |
| PC 67  | 43.19                                      | 45.87                                     | 10.94                                 | 141.16                    | 3.44                                 | 40.97                                | 404.49                               |
| PC 68  | 7.38                                       | 71.50                                     | 21.13                                 | 25.72                     | 1.83                                 | 14.41                                | 51.63                                |
| PC 69  | 3.67                                       | 74.39                                     | 21.94                                 | 19.74                     | 1.70                                 | 14.04                                | 42.15                                |
| PC 70  | 5.03                                       | 74.82                                     | 20.15                                 | 22.60                     | 1.81                                 | 16.12                                | 46.52                                |
| PC 71  | 6.74                                       | 73.21                                     | 20.04                                 | 24.98                     | 1.85                                 | 16.06                                | 50.40                                |
| PC 72  | 5.30                                       | 75.30                                     | 19.39                                 | 23.23                     | 1.86                                 | 16.39                                | 46.76                                |
| PC 73  | 4.66                                       | 75.42                                     | 19.92                                 | 20.92                     | 1.82                                 | 15.12                                | 45.78                                |
| PC 74  | 3.57                                       | 76.05                                     | 20.38                                 | 19.80                     | 1.77                                 | 14.33                                | 44.25                                |

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 75  | 3.71                                       | 75.72                                     | 20.57                                 | 19.89                     | 1.74                                 | 14.28                                | 45.20                                |
| PC 76  | 3.56                                       | 74.67                                     | 21.77                                 | 18.89                     | 1.61                                 | 13.10                                | 42.11                                |
| PC 77  | 3.63                                       | 75.22                                     | 21.14                                 | 19.50                     | 1.65                                 | 12.74                                | 43.43                                |
| PC 78  | 15.19                                      | 66.55                                     | 18.26                                 | 41.56                     | 1.95                                 | 17.78                                | 168.35                               |
| PC 79  | 6.85                                       | 72.64                                     | 20.51                                 | 21.77                     | 1.71                                 | 14.46                                | 47.30                                |
| PC 80  | 10.55                                      | 70.34                                     | 19.11                                 | 30.39                     | 1.82                                 | 15.52                                | 84.29                                |
| PC 81  | 14.64                                      | 66.74                                     | 18.62                                 | 33.48                     | 1.90                                 | 17.63                                | 95.05                                |
| PC 82  | 4.61                                       | 74.18                                     | 21.21                                 | 23.02                     | 1.73                                 | 16.69                                | 46.35                                |
| PC 83  | 3.00                                       | 74.58                                     | 22.42                                 | 19.77                     | 1.63                                 | 15.50                                | 43.57                                |
| PC 84  | 3.88                                       | 74.00                                     | 22.12                                 | 19.49                     | 1.72                                 | 13.92                                | 44.46                                |
| PC 85  | 1.98                                       | 74.13                                     | 23.89                                 | 17.55                     | 1.57                                 | 12.98                                | 39.94                                |
| PC 86  | 4.77                                       | 72.62                                     | 22.61                                 | 22.16                     | 1.60                                 | 14.56                                | 45.43                                |
| PC 87  | 7.52                                       | 73.76                                     | 18.71                                 | 26.25                     | 1.95                                 | 18.23                                | 56.03                                |
| PC 88  | 9.84                                       | 71.49                                     | 18.66                                 | 28.09                     | 1.96                                 | 19.22                                | 62.99                                |
| PC 89  | 15.84                                      | 68.74                                     | 15.43                                 | 34.83                     | 2.37                                 | 25.80                                | 78.75                                |
| PC 90  | 9.71                                       | 70.49                                     | 19.81                                 | 26.72                     | 1.87                                 | 18.59                                | 62.69                                |
| PC 91  | 7.77                                       | 70.52                                     | 21.70                                 | 24.08                     | 1.72                                 | 15.87                                | 56.49                                |
| PC 92  | 7.25                                       | 71.03                                     | 21.73                                 | 23.87                     | 1.70                                 | 15.85                                | 54.39                                |
| PC 93  | 5.57                                       | 71.76                                     | 22.67                                 | 22.44                     | 1.63                                 | 15.19                                | 48.32                                |
| PC 94  | 3.28                                       | 72.69                                     | 24.03                                 | 18.71                     | 1.53                                 | 12.86                                | 40.67                                |
| PC 95  | 3.98                                       | 71.91                                     | 24.11                                 | 20.01                     | 1.53                                 | 13.13                                | 42.66                                |
| PC 96  | 3.69                                       | 69.28                                     | 27.03                                 | 18.61                     | 1.40                                 | 10.37                                | 39.38                                |
| PC 97  | 7.24                                       | 70.64                                     | 22.11                                 | 25.76                     | 1.75                                 | 14.67                                | 50.69                                |
| PC 98  | 5.00                                       | 74.15                                     | 20.84                                 | 21.11                     | 1.76                                 | 15.43                                | 46.91                                |
| PC 99  | 6.22                                       | 72.64                                     | 21.14                                 | 23.54                     | 1.74                                 | 15.62                                | 49.90                                |
| PC 100 | 23.42                                      | 60.16                                     | 16.42                                 | 101.89                    | 2.26                                 | 22.96                                | 440.02                               |
| PC 101 | 4.07                                       | 75.76                                     | 20.17                                 | 20.38                     | 1.81                                 | 15.43                                | 44.03                                |
| PC 102 | 3.80                                       | 75.32                                     | 20.88                                 | 19.78                     | 1.75                                 | 14.71                                | 43.03                                |
| PC 103 | 3.95                                       | 75.13                                     | 20.92                                 | 20.04                     | 1.76                                 | 14.75                                | 43.22                                |
| PC 104 | 3.23                                       | 74.55                                     | 22.22                                 | 18.89                     | 1.67                                 | 13.76                                | 41.14                                |
| PC 105 | 3.59                                       | 73.91                                     | 22.49                                 | 19.41                     | 1.64                                 | 13.49                                | 41.51                                |
| PC 106 | 3.04                                       | 74.39                                     | 22.57                                 | 18.60                     | 1.63                                 | 13.37                                | 40.63                                |
| PC 107 | 3.55                                       | 74.36                                     | 22.09                                 | 19.48                     | 1.67                                 | 13.63                                | 41.47                                |
| PC 108 | 3.17                                       | 74.61                                     | 22.21                                 | 18.86                     | 1.65                                 | 13.48                                | 40.26                                |
| PC 109 | 2.95                                       | 75.10                                     | 21.95                                 | 18.67                     | 1.67                                 | 13.61                                | 39.48                                |
| PC 110 | 2.87                                       | 75.24                                     | 21.90                                 | 18.53                     | 1.68                                 | 13.52                                | 38.97                                |
| PC 111 | 2.75                                       | 74.81                                     | 22.44                                 | 18.11                     | 1.64                                 | 13.06                                | 38.05                                |
| PC 112 | 2.62                                       | 74.89                                     | 22.50                                 | 17.84                     | 1.64                                 | 12.91                                | 37.48                                |

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 113 | 2.78                                       | 74.66                                     | 22.56                                 | 18.21                     | 1.62                                 | 13.13                                | 38.26                                |
| PC 114 | 5.48                                       | 75.71                                     | 18.82                                 | 22.80                     | 1.95                                 | 15.69                                | 45.55                                |
| PC 115 | 2.89                                       | 77.15                                     | 19.96                                 | 19.23                     | 1.81                                 | 14.69                                | 39.32                                |
| PC 116 | 2.82                                       | 77.04                                     | 20.14                                 | 19.04                     | 1.80                                 | 14.47                                | 38.90                                |
| PC 117 | 2.23                                       | 76.14                                     | 21.63                                 | 17.83                     | 1.69                                 | 13.44                                | 36.94                                |
| PC 118 | 1.94                                       | 76.23                                     | 21.83                                 | 17.37                     | 1.68                                 | 13.14                                | 36.00                                |
| PC 119 | 1.91                                       | 75.93                                     | 22.16                                 | 17.12                     | 1.66                                 | 12.92                                | 35.76                                |
| PC 120 | 4.55                                       | 74.95                                     | 20.50                                 | 21.38                     | 1.79                                 | 14.42                                | 43.06                                |
| PC 121 | 4.92                                       | 73.69                                     | 21.40                                 | 21.37                     | 1.72                                 | 14.51                                | 44.92                                |
| PC 122 | 4.65                                       | 76.03                                     | 19.33                                 | 22.28                     | 1.86                                 | 16.07                                | 45.33                                |
| PC 123 | 3.61                                       | 76.74                                     | 19.65                                 | 19.83                     | 1.85                                 | 15.10                                | 43.74                                |
| PC 124 | 3.60                                       | 76.79                                     | 19.61                                 | 20.35                     | 1.84                                 | 15.18                                | 43.10                                |
| PC 125 | 1.38                                       | 78.56                                     | 20.07                                 | 17.29                     | 1.79                                 | 14.32                                | 36.38                                |
| PC 126 | 3.02                                       | 75.10                                     | 21.88                                 | 18.57                     | 1.69                                 | 13.88                                | 41.21                                |
| PC 127 | 2.99                                       | 76.17                                     | 20.84                                 | 19.15                     | 1.75                                 | 14.95                                | 41.28                                |
| PC 128 | 3.72                                       | 74.33                                     | 21.95                                 | 19.68                     | 1.68                                 | 14.69                                | 43.21                                |
| PC 129 | 3.31                                       | 73.02                                     | 23.67                                 | 18.30                     | 1.56                                 | 13.05                                | 40.74                                |
| PC 130 | 3.76                                       | 76.98                                     | 19.26                                 | 20.59                     | 1.88                                 | 16.03                                | 43.76                                |
| PC 131 | 3.77                                       | 76.15                                     | 20.07                                 | 20.36                     | 1.81                                 | 15.58                                | 43.64                                |
| PC 132 | 4.14                                       | 76.59                                     | 19.27                                 | 21.14                     | 1.89                                 | 16.27                                | 45.00                                |
| PC 133 | 4.71                                       | 76.42                                     | 18.87                                 | 21.94                     | 1.92                                 | 16.80                                | 46.69                                |
| PC 134 | 6.93                                       | 73.28                                     | 19.78                                 | 24.64                     | 1.85                                 | 16.14                                | 51.39                                |
| PC 135 | 4.12                                       | 75.67                                     | 20.21                                 | 20.75                     | 1.78                                 | 15.09                                | 43.40                                |
| PC 136 | 4.08                                       | 75.39                                     | 20.53                                 | 20.91                     | 1.77                                 | 15.56                                | 44.01                                |
| PC 137 | 4.68                                       | 75.52                                     | 19.80                                 | 21.89                     | 1.83                                 | 16.45                                | 46.64                                |
| PC 138 | 4.04                                       | 76.54                                     | 19.41                                 | 21.00                     | 1.85                                 | 15.76                                | 44.64                                |
| PC 139 | 2.99                                       | 78.00                                     | 19.01                                 | 20.01                     | 1.88                                 | 15.73                                | 42.39                                |
| PC 140 | 3.87                                       | 77.73                                     | 18.39                                 | 21.16                     | 1.93                                 | 16.49                                | 43.85                                |
| PC 141 | 5.47                                       | 76.25                                     | 18.28                                 | 23.33                     | 1.96                                 | 17.95                                | 49.33                                |
| PC 142 | 12.34                                      | 76.53                                     | 11.13                                 | 35.00                     | 3.37                                 | 31.77                                | 67.78                                |
| PC 143 | 13.01                                      | 75.41                                     | 11.59                                 | 34.80                     | 3.21                                 | 28.42                                | 70.80                                |
| PC 144 | 14.72                                      | 73.15                                     | 12.13                                 | 35.97                     | 3.06                                 | 29.54                                | 74.23                                |
| PC 145 | 8.85                                       | 73.06                                     | 18.09                                 | 26.58                     | 2.05                                 | 18.84                                | 60.65                                |
| PC 146 | 8.61                                       | 73.07                                     | 18.32                                 | 26.49                     | 2.02                                 | 18.58                                | 59.77                                |
| PC 147 | 6.57                                       | 73.81                                     | 19.62                                 | 23.94                     | 1.86                                 | 16.33                                | 51.79                                |
| PC 148 | 2.15                                       | 75.89                                     | 21.96                                 | 18.23                     | 1.68                                 | 13.83                                | 41.59                                |
| PC 149 | 2.39                                       | 74.88                                     | 22.73                                 | 18.28                     | 1.64                                 | 13.56                                | 42.12                                |
| PC 150 | 3.41                                       | 76.76                                     | 19.83                                 | 20.20                     | 1.84                                 | 15.87                                | 44.63                                |

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 151 | 2.57                                       | 76.55                                     | 20.88                                 | 19.07                     | 1.74                                 | 15.03                                | 42.04                                |
| PC 152 | 2.22                                       | 76.58                                     | 21.20                                 | 18.24                     | 1.73                                 | 14.24                                | 40.19                                |
| PC 153 | 0.73                                       | 77.86                                     | 21.41                                 | 17.17                     | 1.73                                 | 13.86                                | 37.87                                |
| PC 154 | 1.53                                       | 78.66                                     | 19.81                                 | 18.61                     | 1.82                                 | 15.45                                | 39.88                                |
| PC 155 | 1.45                                       | 78.77                                     | 19.78                                 | 18.54                     | 1.82                                 | 15.41                                | 39.70                                |
| PC 156 | 2.08                                       | 76.14                                     | 21.79                                 | 18.06                     | 1.67                                 | 14.16                                | 39.46                                |
| PC 157 | 2.48                                       | 76.77                                     | 20.75                                 | 18.77                     | 1.74                                 | 14.84                                | 40.30                                |
| PC 158 | 3.06                                       | 76.19                                     | 20.75                                 | 19.32                     | 1.76                                 | 14.86                                | 41.40                                |
| PC 159 | 3.78                                       | 75.67                                     | 20.56                                 | 20.09                     | 1.77                                 | 14.93                                | 42.89                                |
| PC 160 | 8.09                                       | 71.85                                     | 20.06                                 | 28.39                     | 1.84                                 | 15.81                                | 53.54                                |
| PC 161 | 3.41                                       | 79.50                                     | 17.09                                 | 21.46                     | 2.08                                 | 17.72                                | 43.24                                |
| PC 162 | 3.02                                       | 80.65                                     | 16.33                                 | 21.64                     | 2.15                                 | 18.53                                | 43.13                                |
| PC 163 | 4.39                                       | 79.88                                     | 15.74                                 | 24.52                     | 2.24                                 | 19.66                                | 45.96                                |
| PC 164 | 4.24                                       | 80.63                                     | 15.12                                 | 24.11                     | 2.33                                 | 20.54                                | 46.84                                |
| PC 165 | 4.96                                       | 79.56                                     | 15.48                                 | 26.14                     | 2.29                                 | 20.28                                | 47.57                                |
| PC 166 | 4.40                                       | 79.47                                     | 16.13                                 | 24.72                     | 2.19                                 | 19.31                                | 45.97                                |
| PC 167 | 5.32                                       | 77.40                                     | 17.28                                 | 26.65                     | 2.06                                 | 17.80                                | 46.01                                |
| PC 168 | 6.88                                       | 74.71                                     | 18.42                                 | 29.40                     | 1.95                                 | 16.29                                | 47.68                                |
| PC 169 | 15.86                                      | 66.15                                     | 17.98                                 | 62.77                     | 2.03                                 | 17.01                                | 241.17                               |
| PC 170 | 24.44                                      | 59.25                                     | 16.31                                 | 90.83                     | 2.25                                 | 19.92                                | 332.16                               |
| PC 171 | 48.73                                      | 40.32                                     | 10.95                                 | 201.67                    | 3.47                                 | 51.43                                | 544.77                               |
| PC 172 | 72.03                                      | 22.01                                     | 5.96                                  | 321.48                    | 9.16                                 | 265.90                               | 756.73                               |
| PC 173 | 5.53                                       | 75.46                                     | 19.01                                 | 22.81                     | 1.91                                 | 16.05                                | 46.57                                |
| PC 174 | 2.91                                       | 77.54                                     | 19.55                                 | 19.32                     | 1.82                                 | 15.29                                | 39.88                                |
| PC 175 | 3.26                                       | 77.43                                     | 19.31                                 | 20.26                     | 1.86                                 | 16.14                                | 42.77                                |
| PC 176 | 3.18                                       | 77.39                                     | 19.43                                 | 20.00                     | 1.84                                 | 15.82                                | 41.92                                |
| PC 177 | 3.45                                       | 78.11                                     | 18.44                                 | 20.83                     | 1.93                                 | 16.64                                | 43.37                                |
| PC 178 | 6.43                                       | 77.73                                     | 15.84                                 | 25.23                     | 2.27                                 | 19.81                                | 54.02                                |
| PC 179 | 5.81                                       | 77.14                                     | 17.06                                 | 24.11                     | 2.11                                 | 18.00                                | 50.70                                |
| PC 180 | 2.37                                       | 79.02                                     | 18.61                                 | 19.93                     | 1.91                                 | 16.09                                | 40.71                                |
| PC 181 | 1.64                                       | 78.94                                     | 19.42                                 | 19.00                     | 1.85                                 | 16.04                                | 40.18                                |
| PC 182 | 3.95                                       | 75.37                                     | 20.67                                 | 21.12                     | 1.77                                 | 15.76                                | 45.66                                |
| PC 183 | 5.53                                       | 73.99                                     | 20.48                                 | 22.97                     | 1.79                                 | 16.43                                | 47.36                                |
| PC 184 | 4.66                                       | 74.99                                     | 20.35                                 | 22.15                     | 1.78                                 | 16.24                                | 46.49                                |
| PC 185 | 4.41                                       | 73.20                                     | 22.39                                 | 20.99                     | 1.66                                 | 14.43                                | 44.19                                |
| PC 186 | 4.28                                       | 74.16                                     | 21.56                                 | 20.96                     | 1.71                                 | 14.67                                | 44.08                                |
| PC 187 | 5.21                                       | 74.12                                     | 20.66                                 | 23.20                     | 1.78                                 | 14.98                                | 45.88                                |
| PC 188 | 96.79                                      | 1.95                                      | 1.26                                  | 26.12                     | 1.98                                 | 17.54                                | 52.04                                |

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 189 | 100.00                                     | 0.00                                      | 0.00                                  | 56.15                     | 2.13                                 | 18.98                                | 161.20                               |
| PC 190 | 4.13                                       | 75.75                                     | 20.13                                 | 20.52                     | 1.81                                 | 15.52                                | 44.79                                |
| PC 191 | 3.85                                       | 74.81                                     | 21.34                                 | 19.90                     | 1.72                                 | 14.75                                | 43.51                                |
| PC 192 | 3.87                                       | 76.13                                     | 20.00                                 | 20.16                     | 1.82                                 | 15.15                                | 43.66                                |
| PC 193 | 2.34                                       | 76.58                                     | 21.08                                 | 19.07                     | 1.72                                 | 15.08                                | 42.31                                |
| PC 194 | 4.38                                       | 78.13                                     | 17.49                                 | 21.91                     | 2.05                                 | 17.41                                | 46.80                                |
| PC 195 | 3.78                                       | 77.44                                     | 18.78                                 | 20.24                     | 1.90                                 | 15.61                                | 43.63                                |
| PC 196 | 3.25                                       | 80.07                                     | 16.68                                 | 21.51                     | 2.11                                 | 18.40                                | 42.79                                |
| PC 197 | 7.89                                       | 74.17                                     | 17.94                                 | 25.38                     | 2.04                                 | 18.18                                | 57.43                                |
| PC 198 | 3.82                                       | 73.91                                     | 22.27                                 | 19.52                     | 1.67                                 | 13.54                                | 42.13                                |
| PC 199 | 4.37                                       | 74.75                                     | 20.88                                 | 20.75                     | 1.76                                 | 15.29                                | 44.62                                |
| PC 200 | 3.82                                       | 74.96                                     | 21.22                                 | 20.78                     | 1.73                                 | 15.17                                | 43.96                                |
| PC 201 | 5.60                                       | 73.18                                     | 21.22                                 | 23.22                     | 1.73                                 | 15.37                                | 47.44                                |
| PC 202 | 3.85                                       | 74.77                                     | 21.38                                 | 20.17                     | 1.72                                 | 14.65                                | 43.01                                |
| PC 203 | 2.72                                       | 74.79                                     | 22.48                                 | 17.98                     | 1.65                                 | 12.69                                | 38.11                                |
| PC 204 | 9.66                                       | 72.69                                     | 17.65                                 | 33.68                     | 2.07                                 | 18.18                                | 61.65                                |
| PC 205 | 6.48                                       | 73.50                                     | 20.02                                 | 24.68                     | 1.82                                 | 15.88                                | 50.09                                |
| PC 206 | 7.51                                       | 72.86                                     | 19.63                                 | 27.33                     | 1.86                                 | 16.74                                | 53.94                                |
| PC 207 | 6.72                                       | 74.74                                     | 18.53                                 | 24.86                     | 1.97                                 | 17.69                                | 53.73                                |
| PC 208 | 8.76                                       | 75.43                                     | 15.81                                 | 28.78                     | 2.30                                 | 21.10                                | 60.26                                |
| PC 209 | 5.91                                       | 76.26                                     | 17.83                                 | 24.08                     | 2.01                                 | 18.13                                | 51.11                                |
| PC 210 | 11.61                                      | 70.06                                     | 18.33                                 | 35.45                     | 1.99                                 | 18.80                                | 72.17                                |
| PC 211 | 14.73                                      | 68.50                                     | 16.77                                 | 48.81                     | 2.20                                 | 20.84                                | 96.63                                |
| PC 212 | 6.38                                       | 74.87                                     | 18.76                                 | 24.50                     | 1.95                                 | 17.37                                | 52.07                                |
| PC 213 | 6.66                                       | 73.91                                     | 19.43                                 | 24.82                     | 1.88                                 | 16.93                                | 51.07                                |
| PC 214 | 3.31                                       | 75.81                                     | 20.88                                 | 20.00                     | 1.76                                 | 15.00                                | 42.65                                |
| PC 215 | 5.43                                       | 77.09                                     | 17.48                                 | 24.54                     | 2.07                                 | 18.34                                | 47.91                                |
| PC 216 | 6.08                                       | 78.01                                     | 15.91                                 | 27.16                     | 2.25                                 | 20.33                                | 50.40                                |
| PC 217 | 6.56                                       | 76.98                                     | 16.47                                 | 28.09                     | 2.18                                 | 19.89                                | 51.20                                |
| PC 218 | 9.04                                       | 74.14                                     | 16.82                                 | 34.26                     | 2.14                                 | 19.79                                | 58.44                                |
| PC 219 | 9.42                                       | 72.08                                     | 18.51                                 | 35.27                     | 1.98                                 | 17.19                                | 59.83                                |
| PC 220 | 7.50                                       | 73.11                                     | 19.39                                 | 28.48                     | 1.91                                 | 15.78                                | 50.80                                |
| PC 221 | 2.02                                       | 79.09                                     | 18.89                                 | 18.98                     | 1.91                                 | 15.53                                | 40.18                                |
| PC 222 | 2.41                                       | 80.88                                     | 16.70                                 | 21.22                     | 2.14                                 | 17.82                                | 42.32                                |
| PC 223 | 2.05                                       | 81.08                                     | 16.87                                 | 20.85                     | 2.11                                 | 17.69                                | 41.81                                |
| PC 224 | 1.52                                       | 81.37                                     | 17.12                                 | 20.16                     | 2.07                                 | 17.27                                | 40.41                                |
| PC 225 | 2.11                                       | 80.46                                     | 17.43                                 | 19.89                     | 2.03                                 | 16.85                                | 40.31                                |
| PC 226 | 0.59                                       | 81.60                                     | 17.81                                 | 18.54                     | 2.00                                 | 16.30                                | 38.39                                |

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 227 | 0.44                                       | 80.64                                     | 18.92                                 | 17.60                     | 1.88                                 | 15.11                                | 37.02                                |
| PC 228 | 0.41                                       | 79.69                                     | 19.90                                 | 16.80                     | 1.81                                 | 14.05                                | 35.85                                |
| PC 229 | 0.44                                       | 78.92                                     | 20.64                                 | 16.29                     | 1.75                                 | 13.33                                | 35.19                                |
| PC 230 | 2.45                                       | 77.09                                     | 20.46                                 | 18.42                     | 1.77                                 | 14.41                                | 38.97                                |
| PC 231 | 2.89                                       | 78.61                                     | 18.50                                 | 21.20                     | 1.93                                 | 17.20                                | 42.97                                |
| PC 232 | 2.55                                       | 78.54                                     | 18.91                                 | 20.21                     | 1.90                                 | 16.89                                | 42.73                                |
| PC 233 | 2.97                                       | 77.39                                     | 19.64                                 | 20.41                     | 1.85                                 | 15.54                                | 41.94                                |
| PC 234 | 2.12                                       | 77.72                                     | 20.16                                 | 18.74                     | 1.80                                 | 14.41                                | 39.43                                |
| PC 235 | 2.38                                       | 76.16                                     | 21.45                                 | 18.34                     | 1.73                                 | 13.46                                | 40.30                                |
| PC 236 | 3.69                                       | 77.82                                     | 18.50                                 | 21.49                     | 1.97                                 | 17.35                                | 46.52                                |
| PC 237 | 5.31                                       | 76.46                                     | 18.23                                 | 23.00                     | 2.01                                 | 16.99                                | 50.73                                |
| PC 238 | 3.91                                       | 79.28                                     | 16.82                                 | 23.23                     | 2.16                                 | 19.55                                | 50.42                                |
| PC 239 | 2.66                                       | 76.59                                     | 20.75                                 | 19.69                     | 1.78                                 | 14.77                                | 46.32                                |
| PC 240 | 1.20                                       | 75.88                                     | 22.92                                 | 16.91                     | 1.64                                 | 12.84                                | 37.51                                |
| PC 241 | 2.84                                       | 75.20                                     | 21.95                                 | 18.53                     | 1.69                                 | 13.72                                | 40.45                                |
| PC 242 | 1.85                                       | 75.85                                     | 22.30                                 | 17.36                     | 1.66                                 | 13.20                                | 38.93                                |
| PC 243 | 0.64                                       | 75.33                                     | 24.03                                 | 15.86                     | 1.53                                 | 12.06                                | 36.03                                |
| PC 244 | 0.29                                       | 75.13                                     | 24.59                                 | 15.22                     | 1.53                                 | 11.44                                | 35.10                                |
| PC 245 | 0.19                                       | 75.24                                     | 24.57                                 | 14.62                     | 1.52                                 | 11.05                                | 33.29                                |
| PC 246 | 0.81                                       | 77.01                                     | 22.19                                 | 16.60                     | 1.67                                 | 13.09                                | 36.82                                |
| PC 247 | 1.81                                       | 74.54                                     | 23.65                                 | 16.49                     | 1.59                                 | 11.72                                | 35.90                                |
| PC 248 | 2.09                                       | 76.81                                     | 21.09                                 | 18.34                     | 1.75                                 | 14.22                                | 40.79                                |
| PC 249 | 7.69                                       | 73.94                                     | 18.37                                 | 26.25                     | 2.02                                 | 17.63                                | 54.51                                |
| PC 250 | 3.17                                       | 77.14                                     | 19.69                                 | 19.71                     | 1.85                                 | 15.43                                | 43.13                                |
| PC 251 | 4.27                                       | 75.07                                     | 20.66                                 | 20.40                     | 1.76                                 | 14.89                                | 43.89                                |
| PC 252 | 2.58                                       | 76.14                                     | 21.28                                 | 18.71                     | 1.72                                 | 14.39                                | 41.60                                |
| PC 253 | 3.82                                       | 75.59                                     | 20.58                                 | 20.06                     | 1.75                                 | 15.32                                | 42.90                                |
| PC 254 | 5.02                                       | 73.31                                     | 21.67                                 | 20.69                     | 1.70                                 | 14.66                                | 46.15                                |
| PC 255 | 3.93                                       | 73.86                                     | 22.21                                 | 19.34                     | 1.67                                 | 13.83                                | 43.23                                |
| PC 256 | 3.30                                       | 72.50                                     | 24.21                                 | 17.90                     | 1.56                                 | 12.31                                | 41.09                                |
| PC 257 | 5.43                                       | 72.04                                     | 22.52                                 | 23.92                     | 1.65                                 | 13.54                                | 45.43                                |
| PC 258 | 6.15                                       | 72.19                                     | 21.65                                 | 24.74                     | 1.71                                 | 14.65                                | 47.94                                |
| PC 259 | 2.23                                       | 71.48                                     | 26.29                                 | 15.51                     | 1.39                                 | 10.43                                | 35.77                                |
| PC 260 | 11.06                                      | 69.71                                     | 19.23                                 | 34.88                     | 1.89                                 | 17.73                                | 69.45                                |
| PC 261 | 12.55                                      | 69.70                                     | 17.74                                 | 60.66                     | 2.06                                 | 19.22                                | 75.62                                |
| PC 262 | 9.93                                       | 70.49                                     | 19.59                                 | 34.25                     | 1.85                                 | 16.84                                | 63.06                                |
| PC 263 | 12.45                                      | 68.21                                     | 19.35                                 | 55.87                     | 1.88                                 | 17.32                                | 87.98                                |
| PC 264 | 4.08                                       | 75.39                                     | 20.53                                 | 20.56                     | 1.77                                 | 15.69                                | 46.04                                |



Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 265 | 4.11                                       | 75.56                                     | 20.33                                 | 20.58                     | 1.78                                 | 15.70                                | 46.45                                |
| PC 266 | 4.40                                       | 73.55                                     | 22.05                                 | 21.44                     | 1.68                                 | 14.24                                | 45.51                                |
| PC 267 | 7.24                                       | 70.24                                     | 22.53                                 | 27.38                     | 1.64                                 | 14.42                                | 52.04                                |
| PC 268 | 10.49                                      | 68.28                                     | 21.23                                 | 36.27                     | 1.74                                 | 15.95                                | 66.72                                |
| PC 269 | 2.40                                       | 75.96                                     | 21.64                                 | 18.69                     | 1.70                                 | 14.40                                | 41.83                                |
| PC 270 | 8.16                                       | 69.53                                     | 22.31                                 | 26.73                     | 1.67                                 | 14.38                                | 54.06                                |
| PC 271 | 13.52                                      | 68.36                                     | 18.12                                 | 36.40                     | 2.07                                 | 18.39                                | 90.56                                |
| PC 272 | 3.75                                       | 74.85                                     | 21.40                                 | 20.16                     | 1.71                                 | 15.25                                | 45.84                                |
| PC 273 | 2.08                                       | 73.52                                     | 24.40                                 | 17.25                     | 1.53                                 | 12.42                                | 39.81                                |
| PC 274 | 3.69                                       | 71.90                                     | 24.41                                 | 19.98                     | 1.54                                 | 12.58                                | 42.73                                |
| PC 275 | 3.32                                       | 76.53                                     | 20.16                                 | 20.11                     | 1.82                                 | 15.60                                | 45.14                                |
| PC 276 | 3.71                                       | 75.92                                     | 20.37                                 | 20.47                     | 1.80                                 | 15.72                                | 46.25                                |
| PC 277 | 1.74                                       | 74.61                                     | 23.65                                 | 17.44                     | 1.59                                 | 12.90                                | 40.00                                |
| PC 278 | 1.53                                       | 74.49                                     | 23.98                                 | 17.09                     | 1.57                                 | 12.64                                | 39.21                                |
| PC 279 | 1.70                                       | 76.26                                     | 22.03                                 | 17.91                     | 1.68                                 | 13.94                                | 39.93                                |
| PC 280 | 2.86                                       | 75.68                                     | 21.46                                 | 19.22                     | 1.72                                 | 14.63                                | 43.49                                |
| PC 281 | 2.17                                       | 76.96                                     | 20.87                                 | 18.83                     | 1.76                                 | 14.79                                | 41.96                                |
| PC 282 | 2.90                                       | 75.57                                     | 21.52                                 | 19.80                     | 1.69                                 | 15.33                                | 45.30                                |
| PC 283 | 6.93                                       | 71.11                                     | 21.97                                 | 26.53                     | 1.68                                 | 15.18                                | 51.53                                |
| PC 284 | 6.12                                       | 72.95                                     | 20.93                                 | 23.56                     | 1.77                                 | 15.57                                | 49.61                                |
| PC 285 | 4.59                                       | 71.46                                     | 23.94                                 | 20.31                     | 1.53                                 | 12.86                                | 43.35                                |
| PC 286 | 8.19                                       | 72.07                                     | 19.74                                 | 28.54                     | 1.84                                 | 16.54                                | 55.61                                |
| PC 287 | 5.81                                       | 73.27                                     | 20.92                                 | 24.39                     | 1.73                                 | 15.37                                | 48.30                                |
| PC 288 | 6.37                                       | 73.04                                     | 20.59                                 | 25.25                     | 1.75                                 | 16.03                                | 50.71                                |
| PC 289 | 2.06                                       | 77.50                                     | 20.45                                 | 18.64                     | 1.74                                 | 14.67                                | 41.75                                |
| PC 290 | 1.80                                       | 76.11                                     | 22.09                                 | 18.29                     | 1.64                                 | 14.40                                | 41.04                                |
| PC 291 | 1.20                                       | 76.75                                     | 22.05                                 | 17.70                     | 1.71                                 | 14.16                                | 39.17                                |
| PC 292 | 0.99                                       | 78.29                                     | 20.72                                 | 18.10                     | 1.71                                 | 15.01                                | 39.30                                |
| PC 293 | 0.67                                       | 77.99                                     | 21.34                                 | 17.35                     | 1.67                                 | 14.30                                | 37.91                                |
| PC 294 | 0.47                                       | 77.90                                     | 21.63                                 | 17.03                     | 1.66                                 | 13.95                                | 37.40                                |
| PC 295 | 0.93                                       | 76.68                                     | 22.40                                 | 17.14                     | 1.69                                 | 13.65                                | 38.07                                |
| PC 296 | 1.28                                       | 77.38                                     | 21.33                                 | 17.83                     | 1.69                                 | 14.33                                | 39.21                                |
| PC 297 | 1.22                                       | 77.30                                     | 21.48                                 | 17.65                     | 1.71                                 | 14.09                                | 38.97                                |
| PC 298 | 0.89                                       | 77.47                                     | 21.63                                 | 17.12                     | 1.72                                 | 13.64                                | 37.89                                |
| PC 299 | 0.79                                       | 76.86                                     | 22.35                                 | 16.59                     | 1.67                                 | 13.02                                | 36.94                                |
| PC 300 | 12.07                                      | 69.95                                     | 17.98                                 | 33.79                     | 2.06                                 | 19.15                                | 74.07                                |
| PC 301 | 9.60                                       | 70.52                                     | 19.87                                 | 32.25                     | 1.83                                 | 17.32                                | 61.69                                |
| PC 302 | 2.97                                       | 74.57                                     | 22.46                                 | 19.28                     | 1.64                                 | 14.58                                | 43.75                                |

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 303 | 0.94                                       | 75.87                                     | 23.18                                 | 16.88                     | 1.61                                 | 13.28                                | 37.78                                |
| PC 304 | 0.91                                       | 77.27                                     | 21.82                                 | 17.42                     | 1.70                                 | 14.12                                | 38.40                                |
| PC 305 | 0.74                                       | 76.77                                     | 22.49                                 | 16.84                     | 1.66                                 | 13.46                                | 37.40                                |
| PC 306 | 0.58                                       | 76.43                                     | 22.99                                 | 16.52                     | 1.62                                 | 13.02                                | 36.97                                |
| PC 307 | 3.83                                       | 75.63                                     | 20.54                                 | 19.48                     | 1.81                                 | 13.75                                | 39.54                                |
| PC 308 | 2.68                                       | 75.87                                     | 21.45                                 | 17.88                     | 1.73                                 | 13.22                                | 37.54                                |
| PC 309 | 2.08                                       | 76.22                                     | 21.70                                 | 16.97                     | 1.71                                 | 12.93                                | 35.81                                |
| PC 310 | 1.29                                       | 74.61                                     | 24.10                                 | 15.13                     | 1.57                                 | 11.25                                | 33.24                                |
| PC 311 | 0.16                                       | 74.82                                     | 25.03                                 | 13.78                     | 1.56                                 | 10.35                                | 31.24                                |
| PC 312 | 0.02                                       | 74.93                                     | 25.05                                 | 13.52                     | 1.55                                 | 10.29                                | 30.73                                |
| PC 313 | 2.16                                       | 76.75                                     | 21.10                                 | 18.30                     | 1.73                                 | 14.23                                | 40.80                                |
| PC 314 | 0.56                                       | 78.57                                     | 20.87                                 | 17.40                     | 1.73                                 | 14.37                                | 38.04                                |
| PC 315 | 0.43                                       | 77.06                                     | 22.51                                 | 16.52                     | 1.64                                 | 13.26                                | 36.64                                |
| PC 316 | 1.07                                       | 79.34                                     | 19.58                                 | 18.76                     | 1.82                                 | 15.98                                | 39.98                                |
| PC 317 | 1.32                                       | 79.19                                     | 19.48                                 | 19.06                     | 1.83                                 | 16.23                                | 40.62                                |
| PC 318 | 2.89                                       | 77.95                                     | 19.16                                 | 21.24                     | 1.86                                 | 16.62                                | 42.61                                |
| PC 319 | 3.62                                       | 76.97                                     | 19.41                                 | 21.25                     | 1.84                                 | 16.36                                | 43.25                                |
| PC 320 | 3.68                                       | 76.16                                     | 20.16                                 | 21.04                     | 1.79                                 | 15.80                                | 43.12                                |
| PC 321 | 3.99                                       | 74.42                                     | 21.59                                 | 20.93                     | 1.67                                 | 15.11                                | 43.47                                |
| PC 322 | 3.80                                       | 73.97                                     | 22.23                                 | 19.88                     | 1.63                                 | 14.63                                | 42.95                                |
| PC 323 | 4.05                                       | 74.61                                     | 21.34                                 | 20.20                     | 1.71                                 | 14.90                                | 43.44                                |
| PC 324 | 4.11                                       | 75.25                                     | 20.63                                 | 20.36                     | 1.77                                 | 15.17                                | 43.67                                |
| PC 325 | 20.66                                      | 61.11                                     | 18.22                                 | 75.23                     | 2.04                                 | 21.01                                | 246.41                               |
| PC 326 | 23.21                                      | 62.76                                     | 14.04                                 | 45.39                     | 2.66                                 | 29.73                                | 103.21                               |
| PC 327 | 27.58                                      | 58.15                                     | 14.28                                 | 90.95                     | 2.60                                 | 27.83                                | 262.68                               |
| PC 328 | 11.92                                      | 69.45                                     | 18.63                                 | 41.29                     | 1.97                                 | 18.66                                | 72.21                                |
| PC 329 | 9.83                                       | 72.40                                     | 17.77                                 | 28.91                     | 2.06                                 | 21.59                                | 63.04                                |
| PC 330 | 16.54                                      | 66.50                                     | 16.96                                 | 37.00                     | 2.16                                 | 23.76                                | 84.29                                |
| PC 331 | 3.38                                       | 75.57                                     | 21.05                                 | 20.31                     | 1.76                                 | 15.90                                | 44.99                                |
| PC 332 | 2.27                                       | 76.30                                     | 21.43                                 | 17.99                     | 1.72                                 | 13.72                                | 39.77                                |
| PC 333 | 1.83                                       | 74.75                                     | 23.42                                 | 17.25                     | 1.60                                 | 12.80                                | 39.25                                |
| PC 334 | 2.74                                       | 73.53                                     | 23.74                                 | 18.01                     | 1.55                                 | 12.95                                | 41.27                                |
| PC 335 | 2.59                                       | 76.07                                     | 21.34                                 | 18.72                     | 1.70                                 | 14.41                                | 41.56                                |
| PC 336 | 2.27                                       | 75.56                                     | 22.16                                 | 17.72                     | 1.65                                 | 13.38                                | 39.20                                |
| PC 337 | 1.29                                       | 76.86                                     | 21.85                                 | 17.20                     | 1.69                                 | 13.49                                | 38.13                                |
| PC 338 | 1.50                                       | 76.56                                     | 21.94                                 | 17.23                     | 1.69                                 | 13.27                                | 38.36                                |
| PC 339 | 1.74                                       | 75.83                                     | 22.42                                 | 17.34                     | 1.65                                 | 13.15                                | 38.83                                |
| PC 340 | 1.95                                       | 75.16                                     | 22.89                                 | 17.43                     | 1.62                                 | 12.98                                | 39.45                                |

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 341 | 4.75                                       | 73.15                                     | 22.10                                 | 20.89                     | 1.67                                 | 13.29                                | 42.43                                |
| PC 342 | 3.53                                       | 76.39                                     | 20.08                                 | 20.43                     | 1.79                                 | 15.43                                | 41.83                                |
| PC 343 | 3.93                                       | 75.89                                     | 20.18                                 | 20.81                     | 1.78                                 | 15.78                                | 42.96                                |
| PC 344 | 3.95                                       | 72.67                                     | 23.39                                 | 19.12                     | 1.58                                 | 12.96                                | 40.68                                |
| PC 345 | 5.26                                       | 73.94                                     | 20.80                                 | 22.74                     | 1.75                                 | 14.49                                | 44.36                                |
| PC 346 | 3.81                                       | 76.48                                     | 19.71                                 | 21.14                     | 1.83                                 | 16.06                                | 43.25                                |
| PC 347 | 4.06                                       | 77.78                                     | 18.16                                 | 22.22                     | 1.96                                 | 17.78                                | 45.46                                |
| PC 348 | 4.37                                       | 77.29                                     | 18.34                                 | 22.54                     | 1.96                                 | 17.73                                | 45.90                                |
| PC 349 | 0.99                                       | 79.37                                     | 19.64                                 | 17.70                     | 1.84                                 | 14.64                                | 37.96                                |
| PC 350 | 3.03                                       | 78.68                                     | 18.30                                 | 20.62                     | 1.96                                 | 16.83                                | 43.49                                |
| PC 351 | 2.92                                       | 79.93                                     | 17.15                                 | 21.62                     | 2.07                                 | 18.62                                | 44.56                                |
| PC 352 | 1.74                                       | 78.02                                     | 20.24                                 | 18.47                     | 1.79                                 | 14.88                                | 40.13                                |
| PC 353 | 3.90                                       | 76.79                                     | 19.31                                 | 21.26                     | 1.87                                 | 16.83                                | 46.30                                |
| PC 354 | 1.76                                       | 77.14                                     | 21.10                                 | 17.92                     | 1.73                                 | 14.09                                | 39.09                                |
| PC 355 | 1.54                                       | 77.07                                     | 21.38                                 | 17.58                     | 1.70                                 | 13.86                                | 38.46                                |
| PC 356 | 0.57                                       | 75.09                                     | 24.33                                 | 16.01                     | 1.55                                 | 12.10                                | 36.56                                |
| PC 357 | 1.34                                       | 76.93                                     | 21.73                                 | 17.76                     | 1.68                                 | 14.32                                | 38.92                                |
| PC 358 | 1.66                                       | 76.41                                     | 21.93                                 | 17.94                     | 1.66                                 | 14.27                                | 39.30                                |
| PC 359 | 2.13                                       | 77.42                                     | 20.45                                 | 19.00                     | 1.77                                 | 15.38                                | 40.98                                |
| PC 360 | 2.29                                       | 79.16                                     | 18.54                                 | 20.58                     | 1.94                                 | 17.54                                | 43.13                                |
| PC 361 | 1.96                                       | 78.71                                     | 19.33                                 | 19.65                     | 1.87                                 | 16.45                                | 41.84                                |
| PC 362 | 2.34                                       | 78.47                                     | 19.19                                 | 20.00                     | 1.88                                 | 16.68                                | 42.46                                |
| PC 363 | 3.29                                       | 78.10                                     | 18.61                                 | 21.23                     | 1.92                                 | 17.64                                | 44.64                                |
| PC 364 | 3.77                                       | 78.32                                     | 17.90                                 | 22.04                     | 1.99                                 | 18.41                                | 46.01                                |
| PC 365 | 6.43                                       | 75.97                                     | 17.60                                 | 27.10                     | 2.05                                 | 18.73                                | 50.99                                |
| PC 366 | 9.21                                       | 70.94                                     | 19.85                                 | 28.97                     | 1.85                                 | 17.17                                | 60.18                                |
| PC 367 | 3.51                                       | 76.50                                     | 19.99                                 | 20.19                     | 1.82                                 | 15.77                                | 44.16                                |
| PC 368 | 3.17                                       | 75.42                                     | 21.41                                 | 19.44                     | 1.72                                 | 14.81                                | 43.21                                |
| PC 369 | 4.39                                       | 76.53                                     | 19.08                                 | 21.66                     | 1.91                                 | 16.96                                | 47.91                                |
| PC 370 | 3.77                                       | 77.67                                     | 18.56                                 | 21.12                     | 1.94                                 | 16.80                                | 46.43                                |
| PC 371 | 6.92                                       | 75.03                                     | 18.05                                 | 24.34                     | 2.01                                 | 18.73                                | 55.40                                |
| PC 372 | 5.08                                       | 75.41                                     | 19.51                                 | 22.07                     | 1.88                                 | 16.82                                | 49.92                                |
| PC 373 | 3.60                                       | 75.77                                     | 20.62                                 | 20.9                      | 1.8                                  | 15.1                                 | 42.7                                 |
| PC 374 | 5.09                                       | 74.99                                     | 19.92                                 | 22.69                     | 1.81                                 | 16.20                                | 46.12                                |
| PC 375 | 4.22                                       | 75.96                                     | 19.82                                 | 21.68                     | 1.82                                 | 16.20                                | 44.62                                |
| PC 376 | 3.64                                       | 76.35                                     | 20.01                                 | 20.74                     | 1.81                                 | 15.55                                | 42.90                                |
| PC 377 | 3.07                                       | 76.35                                     | 20.58                                 | 19.82                     | 1.77                                 | 14.95                                | 41.35                                |
| PC 378 | 2.77                                       | 76.19                                     | 21.04                                 | 19.06                     | 1.72                                 | 14.33                                | 39.99                                |

Appendix B Continued. Textural data used in this study.

| Sample | Percent Sand<br>(2000-62.5 $\mu\text{m}$ ) | Percent Silt<br>(62.5-3.9 $\mu\text{m}$ ) | Percent Clay<br>( $<3.9\mu\text{m}$ ) | Mean<br>( $\mu\text{m}$ ) | d <sub>10</sub><br>( $\mu\text{m}$ ) | d <sub>50</sub><br>( $\mu\text{m}$ ) | d <sub>90</sub><br>( $\mu\text{m}$ ) |
|--------|--|---|---------------------------------------|---------------------------|--------------------------------------|--------------------------------------|--------------------------------------|
| PC 379 | 2.49                                       | 75.72                                     | 21.79                                 | 18.12                     | 1.67                                 | 13.44                                | 38.25                                |
| PC 380 | 2.25                                       | 75.76                                     | 21.99                                 | 17.64                     | 1.65                                 | 13.05                                | 36.95                                |
| PC 381 | 2.43                                       | 76.12                                     | 21.45                                 | 18.06                     | 1.67                                 | 13.63                                | 37.76                                |
| PC 382 | 2.35                                       | 76.03                                     | 21.62                                 | 17.72                     | 1.67                                 | 13.41                                | 37.24                                |
| PC 383 | 3.12                                       | 77.33                                     | 19.56                                 | 19.43                     | 1.87                                 | 14.77                                | 40.20                                |
| PC 384 | 3.47                                       | 77.59                                     | 18.95                                 | 20.21                     | 1.93                                 | 15.44                                | 41.90                                |
| PC 385 | 5.42                                       | 74.72                                     | 19.87                                 | 22.81                     | 1.84                                 | 15.88                                | 46.92                                |
| PC 386 | 4.33                                       | 76.39                                     | 19.29                                 | 21.50                     | 1.89                                 | 15.66                                | 44.00                                |
| PC 387 | 3.33                                       | 76.02                                     | 20.65                                 | 19.90                     | 1.80                                 | 15.28                                | 42.60                                |
| PC 388 | 4.36                                       | 76.57                                     | 19.07                                 | 21.68                     | 1.92                                 | 16.82                                | 46.28                                |
| PC 389 | 2.96                                       | 74.77                                     | 22.27                                 | 18.63                     | 1.69                                 | 13.92                                | 40.38                                |
| PC 390 | 0.00                                       | 78.79                                     | 21.21                                 | 13.47                     | 1.78                                 | 11.99                                | 27.63                                |
| PC 391 | 3.14                                       | 73.67                                     | 23.19                                 | 17.84                     | 1.62                                 | 12.58                                | 38.84                                |
| PC 392 | 4.69                                       | 73.91                                     | 21.40                                 | 20.16                     | 1.73                                 | 13.86                                | 42.62                                |
| PC 393 | 81.26                                      | 13.77                                     | 4.97                                  | 587.16                    | 13.12                                | 572.87                               | 1170.89                              |
| PC 394 | 43.97                                      | 42.53                                     | 13.50                                 | 226.16                    | 2.80                                 | 39.49                                | 703.49                               |
| PC 395 | 74.61                                      | 18.57                                     | 6.82                                  | 659.28                    | 7.11                                 | 603.07                               | 1454.39                              |
| PC 396 | 16.51                                      | 65.27                                     | 18.21                                 | 54.92                     | 2.03                                 | 19.75                                | 126.79                               |
| PC 397 | 16.57                                      | 62.57                                     | 20.86                                 | 75.04                     | 1.79                                 | 16.71                                | 300.44                               |
| PC 398 | 15.44                                      | 62.13                                     | 22.43                                 | 69.29                     | 1.66                                 | 15.47                                | 218.70                               |

## Appendix C. Geochemical Data

Appendix C-1. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 1   | 159       | 1,097     | 20,313    | 1,209     | 46,961    |
| PC 2*  | 96        | 427       | 18,617    | 1,232     | 16,050    |
| PC 3*  | 254       | 1,538     | 18,892    | 1,235     | 19,024    |
| PC 4*  | 572       | 2,019     | 19,208    | 1,241     | 43,412    |
| PC 5*  | 408       | 1,964     | 18,111    | 1,255     | 27,502    |
| PC 6*  | 1,702     | 4,517     | 21,440    | 1,204     | 85,626    |
| PC 7*  | 366       | 2,714     | 20,960    | 1,464     | 38,427    |
| PC 8*  | 119       | 957       | 16,758    | 1,218     | 13,861    |
| PC 9   | 1,263     | 1,793     | 24,392    | 1,143     | 134,569   |
| PC 10  | 722       | 3,624     | 20,559    | 1,250     | 135,587   |
| PC 11  | 890       | 3,120     | 19,200    | 1,435     | 123,281   |
| PC 12  | 4,768     | 4,608     | 21,442    | 927       | 181,893   |
| PC 13  | 1,594     | 7,596     | 20,996    | 915       | 178,657   |
| PC 14  | 51        | 195       | 17,348    | 1,173     | 11,007    |
| PC 15  | 61        | 170       | 18,171    | 1,262     | 4,874     |
| PC 16  | 61        | 267       | 17,426    | 1,291     | 3,399     |
| PC 17  | 73        | 440       | 17,716    | 1,370     | 4,468     |
| PC 18  | 142       | 675       | 16,914    | 1,379     | 5,699     |
| PC 19  | 285       | 829       | 17,245    | 1,305     | 9,761     |
| PC 20  | 192       | 829       | 19,240    | 1,424     | 7,230     |
| PC 21  | 32        | 145       | 17,996    | 1,189     | 3,229     |
| PC 22  | 35        | 127       | 18,724    | 1,123     | 4,397     |
| PC 23  | 29        | 95        | 19,559    | 1,236     | 3,590     |
| PC 24  | 30        | 90        | 19,982    | 971       | 2,995     |
| PC 25  | 22        | 69        | 19,305    | 279       | 2,619     |
| PC 26  | 25        | 99        | 21,568    | 537       | 3,758     |
| PC 27  | 129       | 697       | 19,887    | 1,403     | 17,035    |
| PC 28  | 131       | 818       | 19,830    | 1,409     | 14,604    |
| PC 29  | 127       | 912       | 20,185    | 1,545     | 16,712    |
| PC 30  | 220       | 1,639     | 19,650    | 1,601     | 13,449    |
| PC 31  | 533       | 3,999     | 20,216    | 1,481     | 30,174    |
| PC 32  | 1,142     | 6,386     | 19,779    | 1,252     | 57,868    |
| PC 33  | 553       | 2,254     | 17,750    | 1,380     | 41,914    |
| PC 34  | 279       | 1,714     | 14,782    | 1,110     | 14,306    |
| PC 35  | 398       | 2,247     | 17,844    | 1,365     | 24,541    |
| PC 36  | 30        | 216       | 19,466    | 1,256     | 9,410     |

ND Below detection  
\* Not used in study

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 37  | 51        | 343       | 22,911    | 2,475     | 8,724     |
| PC 38  | 39        | 241       | 19,466    | 465       | 5,659     |
| PC 39  | 37        | 148       | 14,327    | 1,104     | 6,181     |
| PC 40  | 33        | 133       | 13,991    | 1,286     | 2,739     |
| PC 41  | 22        | 61        | 14,454    | 1,217     | 2,178     |
| PC 42  | 18        | 44        | 15,155    | 1,011     | 1,413     |
| PC 43  | ND        | 61        | 16,330    | 642       | 2,049     |
| PC 44  | 25        | 55        | 19,647    | 597       | 1,773     |
| PC 45  | 25        | 52        | 20,004    | 411       | 1,604     |
| PC 46  | 81        | 341       | 17,432    | 1,061     | 24,932    |
| PC 47  | 97        | 324       | 18,747    | 1,187     | 13,901    |
| PC 48  | 115       | 535       | 16,348    | 1,302     | 9,503     |
| PC 49  | 233       | 1,180     | 16,753    | 1,225     | 16,810    |
| PC 50  | 148       | 668       | 16,647    | 1,133     | 33,148    |
| PC 51  | 1,015     | 2,606     | 18,835    | 1,195     | 56,875    |
| PC 52  | 576       | 2,919     | 19,227    | 1,353     | 61,404    |
| PC 53  | 437       | 1,878     | 17,690    | 1,208     | 34,620    |
| PC 54  | 337       | 1,620     | 15,978    | 1,328     | 20,132    |
| PC 55  | 888       | 2,001     | 19,792    | 1,391     | 47,669    |
| PC 56  | 451       | 1,524     | 20,345    | 2,584     | 46,997    |
| PC 57  | 138       | 473       | 19,734    | 1,926     | 18,913    |
| PC 58  | 72        | 274       | 18,812    | 874       | 29,551    |
| PC 59  | 57        | 182       | 22,102    | 770       | 33,385    |
| PC 60  | 24        | 47        | 13,424    | 862       | 1,661     |
| PC 61  | ND        | 49        | 12,683    | 970       | 1,319     |
| PC 62  | 23        | 25        | 15,532    | 532       | 1,722     |
| PC 63  | ND        | 28        | 15,181    | 343       | 1,206     |
| PC 64  | ND        | 19        | 14,936    | 222       | 1,496     |
| PC 65  | 21        | 25        | 14,786    | 232       | 1,359     |
| PC 66  | ND        | 18        | 15,737    | 506       | 1,107     |
| PC 67  | 19        | 18        | 15,089    | 520       | 1,231     |
| PC 68  | 64        | 233       | 17,853    | 1,198     | 11,776    |
| PC 69  | 63        | 227       | 15,832    | 1,064     | 6,119     |
| PC 70  | 90        | 485       | 16,228    | 1,108     | 6,666     |
| PC 71  | 97        | 536       | 15,416    | 993       | 7,775     |
| PC 72  | 109       | 525       | 17,586    | 1,189     | 7,647     |
| PC 73  | 161       | 772       | 16,803    | 1,094     | 11,585    |
| PC 74  | 204       | 719       | 18,065    | 1,204     | 15,445    |

ND Below detection

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm       | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------------|-----------|-----------|-----------|-----------|
| PC 75  | 137             | 379       | 16,365    | 1,172     | 12,791    |
| PC 76  | 32              | 86        | 17,570    | 1,266     | 11,666    |
| PC 77  | 29              | 68        | 17,181    | 1,066     | 9,051     |
| PC 78  | 26              | 50        | 16,639    | 1,041     | 26,120    |
| PC 79  | ND              | 83        | 18,399    | 1,080     | 13,234    |
| PC 80  | ND              | 79        | 19,269    | 1,320     | 13,867    |
| PC 81  | 25              | 68        | 20,090    | 705       | 4,646     |
| PC 82  | 25              | 66        | 20,463    | 277       | 3,671     |
| PC 83  | 29              | 84        | 20,660    | 249       | 3,982     |
| PC 84  | 72              | 352       | 17,570    | 1,132     | 19,128    |
| PC 85  | 74              | 290       | 17,877    | 1,138     | 12,129    |
| PC 86  | 103             | 497       | 17,553    | 1,173     | 7,017     |
| PC 87  | 606             | 1,830     | 18,273    | 1,127     | 39,879    |
| PC 88  | 734             | 2,328     | 20,197    | 1,302     | 61,779    |
| PC 89  | 1,185           | 1,584     | 20,089    | 1,232     | 83,805    |
| PC 90  | 596             | 1,989     | 20,041    | 1,370     | 53,244    |
| PC 91  | 220             | 1,639     | 19,391    | 1,411     | 43,918    |
| PC 92  | 292             | 880       | 18,150    | 1,291     | 34,999    |
| PC 93  | 31              | 99        | 16,548    | 1,378     | 10,190    |
| PC 94  | 38              | 71        | 18,419    | 1,382     | 11,295    |
| PC 95  | 23              | 47        | 18,607    | 1,184     | 9,243     |
| PC 96  | 29              | 67        | 18,520    | 673       | 6,990     |
| PC 97  | 30              | 88        | 16,786    | 455       | 11,728    |
| PC 98  | 106             | 545       | 18,580    | 1,320     | 8,299     |
| PC 99  | 95              | 535       | 18,778    | 1,519     | 9,986     |
| PC 100 | 246             | 2,298     | 20,326    | 1,312     | 45,350    |
| PC 101 | 69              | 295       | 15,623    | 1,079     | 3,940     |
| PC 102 | 154             | 574       | 17,177    | 1,411     | 3,406     |
| PC 103 | 81              | 350       | 14,640    | 1,190     | 3,705     |
| PC 104 | 27              | 74        | 15,240    | 1,181     | 1,704     |
| PC 105 | 38              | 91        | 17,390    | 1,091     | 2,495     |
| PC 106 | 41              | 126       | 17,898    | 908       | 2,585     |
| PC 107 | 26              | 58        | 18,284    | 791       | 1,942     |
| PC 108 | 26              | 61        | 19,133    | 858       | 2,035     |
| PC 109 | ND              | 59        | 19,389    | 819       | 1,809     |
| PC 110 | 23              | 48        | 19,756    | 757       | 1,517     |
| PC 111 | 23              | 55        | 20,062    | 929       | 1,642     |
| PC 112 | ND              | 50        | 20,761    | 911       | 1,879     |
| ND     | Below detection |           |           |           |           |

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm       | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------------|-----------|-----------|-----------|-----------|
| PC 113 | ND              | 57        | 20,783    | 1,275     | 2,112     |
| PC 114 | 34              | 112       | 14,264    | 1,055     | 4,653     |
| PC 115 | 36              | 111       | 15,089    | 1,125     | 2,225     |
| PC 116 | 29              | 113       | 13,636    | 1,030     | 2,268     |
| PC 117 | 28              | 84        | 14,660    | 990       | 2,568     |
| PC 118 | 23              | 41        | 17,453    | 816       | 2,025     |
| PC 119 | 23              | 47        | 19,376    | 643       | 2,243     |
| PC 120 | 59              | 169       | 16,821    | 1,114     | 9,398     |
| PC 121 | 60              | 240       | 17,797    | 1,310     | 4,954     |
| PC 122 | 105             | 367       | 15,135    | 1,105     | 6,187     |
| PC 123 | 335             | 1,106     | 17,012    | 1,238     | 21,322    |
| PC 124 | 252             | 1,049     | 17,160    | 1,257     | 20,199    |
| PC 125 | 151             | 476       | 16,016    | 1,303     | 9,683     |
| PC 126 | 108             | 241       | 16,245    | 1,488     | 13,870    |
| PC 127 | ND              | 58        | 16,082    | 1,558     | 8,317     |
| PC 128 | 32              | 70        | 19,764    | 5,870     | 10,823    |
| PC 129 | 28              | 67        | 24,455    | 3,731     | 17,028    |
| PC 130 | 23              | 68        | 18,298    | 204       | 10,015    |
| PC 131 | 22              | 73        | 19,706    | 314       | 14,453    |
| PC 132 | ND              | 73        | 17,919    | 250       | 11,236    |
| PC 133 | 22              | 69        | 17,817    | 194       | 13,543    |
| PC 134 | 70              | 345       | 17,666    | 1,240     | 14,963    |
| PC 135 | 51              | 179       | 17,643    | 1,239     | 5,607     |
| PC 136 | 61              | 204       | 16,048    | 1,255     | 6,361     |
| PC 137 | 130             | 401       | 16,865    | 1,342     | 12,030    |
| PC 138 | 289             | 934       | 17,161    | 1,187     | 19,937    |
| PC 139 | 276             | 733       | 16,844    | 1,116     | 28,482    |
| PC 140 | 240             | 743       | 15,802    | 1,118     | 18,394    |
| PC 141 | 350             | 1,642     | 17,429    | 1,443     | 28,915    |
| PC 142 | 1,085           | 1,518     | 25,560    | 1,620     | 137,172   |
| PC 143 | 1,496           | 2,573     | 19,226    | 1,085     | 105,030   |
| PC 144 | 2,270           | 3,151     | 19,628    | 1,168     | 117,698   |
| PC 145 | 489             | 1,237     | 18,503    | 1,121     | 71,355    |
| PC 146 | 632             | 1,083     | 18,924    | 912       | 67,354    |
| PC 147 | 266             | 334       | 17,075    | 843       | 28,721    |
| PC 148 | 157             | 387       | 16,768    | 808       | 18,435    |
| PC 149 | 125             | 320       | 18,421    | 600       | 20,907    |
| PC 150 | 71              | 270       | 18,763    | 1,228     | 31,139    |
| ND     | Below detection |           |           |           |           |



Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm       | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------------|-----------|-----------|-----------|-----------|
| PC 151 | 80              | 227       | 18,229    | 1,260     | 19,301    |
| PC 152 | 53              | 164       | 17,360    | 1,182     | 15,038    |
| PC 153 | ND              | 59        | 18,420    | 993       | 4,862     |
| PC 154 | 30              | 65        | 19,305    | 989       | 4,828     |
| PC 155 | 21              | 70        | 20,151    | 937       | 3,773     |
| PC 156 | 36              | 78        | 20,319    | 3,863     | 4,095     |
| PC 157 | 25              | 58        | 22,074    | 1,017     | 3,562     |
| PC 158 | ND              | 79        | 23,037    | 3,426     | 4,648     |
| PC 159 | 25              | 83        | 18,607    | 681       | 3,338     |
| PC 160 | 27              | 81        | 18,495    | 564       | 2,813     |
| PC 161 | 64              | 205       | 15,169    | 1,011     | 4,542     |
| PC 162 | 86              | 246       | 14,655    | 1,000     | 3,682     |
| PC 163 | ND              | 131       | 13,933    | 917       | 2,742     |
| PC 164 | 26              | 57        | 13,853    | 843       | 2,493     |
| PC 165 | ND              | 51        | 14,640    | 829       | 1,549     |
| PC 166 | 16              | 55        | 15,478    | 797       | 1,739     |
| PC 167 | ND              | 47        | 16,219    | 778       | 1,705     |
| PC 168 | ND              | 61        | 17,452    | 942       | 1,880     |
| PC 169 | 19              | 65        | 18,236    | 996       | 1,527     |
| PC 170 | 19              | 69        | 19,240    | 836       | 2,408     |
| PC 171 | 19              | 49        | 16,844    | 763       | 2,303     |
| PC 172 | 11              | 30        | 13,615    | 443       | 1,431     |
| PC 173 | 61              | 189       | 17,788    | 1,141     | 13,374    |
| PC 174 | 55              | 139       | 16,953    | 1,106     | 3,871     |
| PC 175 | 43              | 115       | 15,086    | 1,110     | 3,169     |
| PC 176 | 81              | 218       | 16,465    | 1,266     | 5,990     |
| PC 177 | 156             | 397       | 15,470    | 1,207     | 11,752    |
| PC 178 | 524             | 1,256     | 17,641    | 1,100     | 45,576    |
| PC 179 | 396             | 1,230     | 17,416    | 1,134     | 32,864    |
| PC 180 | 157             | 392       | 15,774    | 1,133     | 12,462    |
| PC 181 | 158             | 213       | 16,214    | 1,104     | 10,954    |
| PC 182 | 114             | 233       | 17,968    | 1,174     | 21,363    |
| PC 183 | 27              | 70        | 15,381    | 1,347     | 9,006     |
| PC 184 | ND              | 43        | 16,363    | 1,571     | 9,714     |
| PC 185 | ND              | 40        | 20,815    | 3,554     | 8,062     |
| PC 186 | 24              | 54        | 15,797    | 256       | 12,555    |
| PC 187 | 21              | 70        | 16,821    | 223       | 25,297    |
| PC 188 | 23              | 71        | 16,242    | 231       | 19,832    |
| ND     | Below detection |           |           |           |           |

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm       | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------------|-----------|-----------|-----------|-----------|
| PC 189 | 19              | 75        | 16,139    | 277       | 38,750    |
| PC 190 | 57              | 224       | 17,263    | 1,221     | 13,045    |
| PC 191 | 76              | 303       | 18,403    | 1,314     | 4,849     |
| PC 192 | 110             | 697       | 18,028    | 1,351     | 7,236     |
| PC 193 | 231             | 992       | 16,475    | 1,293     | 14,528    |
| PC 194 | 355             | 830       | 15,915    | 1,013     | 23,563    |
| PC 195 | 228             | 555       | 16,756    | 1,157     | 23,332    |
| PC 196 | 219             | 1,101     | 15,670    | 1,212     | 11,379    |
| PC 197 | 1,097           | 1,274     | 19,081    | 1,272     | 52,161    |
| PC 198 | 64              | 800       | 16,303    | 1,321     | 7,279     |
| PC 199 | 52              | 141       | 16,914    | 1,371     | 11,789    |
| PC 200 | 47              | 123       | 17,526    | 1,381     | 13,831    |
| PC 201 | 23              | 48        | 18,551    | 867       | 17,018    |
| PC 202 | 23              | 54        | 17,201    | 442       | 19,107    |
| PC 203 | 26              | 72        | 18,451    | 219       | 28,344    |
| PC 204 | 18              | 63        | 18,435    | 220       | 27,104    |
| PC 205 | 89              | 848       | 17,813    | 1,160     | 16,782    |
| PC 206 | 272             | 1,360     | 18,962    | 1,312     | 20,576    |
| PC 207 | 520             | 1,547     | 19,564    | 1,235     | 33,162    |
| PC 208 | 737             | 1,793     | 18,237    | 1,003     | 54,704    |
| PC 209 | 474             | 1,864     | 17,687    | 1,218     | 31,566    |
| PC 210 | 511             | 2,051     | 17,344    | 1,136     | 30,144    |
| PC 211 | 1,015           | 3,539     | 19,903    | 1,325     | 52,738    |
| PC 212 | 171             | 2,105     | 17,419    | 1,145     | 22,975    |
| PC 213 | 75              | 481       | 15,578    | 1,070     | 9,336     |
| PC 214 | 22              | 61        | 16,429    | 717       | 16,681    |
| PC 215 | 46              | 123       | 17,722    | 300       | 11,686    |
| PC 216 | ND              | 58        | 17,799    | 261       | 2,643     |
| PC 217 | 22              | 69        | 16,872    | 975       | 2,453     |
| PC 218 | 34              | 127       | 19,270    | 411       | 3,247     |
| PC 219 | 20              | 81        | 20,785    | ND        | 3,881     |
| PC 220 | 26              | 80        | 15,907    | 34        | 3,732     |
| PC 221 | 44              | 142       | 15,310    | 948       | 4,098     |
| PC 222 | 49              | 189       | 14,749    | 946       | 2,655     |
| PC 223 | 55              | 200       | 14,847    | 910       | 2,816     |
| PC 224 | 39              | 113       | 15,388    | 860       | 2,304     |
| PC 225 | 31              | 75        | 16,581    | 921       | 1,883     |
| PC 226 | 28              | 58        | 17,141    | 875       | 2,071     |
| ND     | Below detection |           |           |           |           |

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm       | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------------|-----------|-----------|-----------|-----------|
| PC 227 | ND              | 59        | 17,723    | 933       | 1,858     |
| PC 228 | 30              | 66        | 18,064    | 941       | 2,213     |
| PC 229 | 24              | 64        | 19,157    | 1,004     | 2,239     |
| PC 230 | 52              | 137       | 19,388    | 1,108     | 5,092     |
| PC 231 | 49              | 143       | 16,466    | 1,079     | 2,736     |
| PC 232 | 69              | 228       | 15,998    | 1,055     | 4,792     |
| PC 233 | 144             | 431       | 16,326    | 1,170     | 8,323     |
| PC 234 | 190             | 440       | 16,415    | 1,051     | 11,641    |
| PC 235 | 272             | 749       | 17,190    | 1,206     | 14,036    |
| PC 236 | 254             | 863       | 16,639    | 1,152     | 23,396    |
| PC 237 | 765             | 755       | 18,526    | 1,180     | 51,630    |
| PC 238 | 550             | 877       | 18,823    | 1,292     | 65,689    |
| PC 239 | 238             | 677       | 19,717    | 1,383     | 46,128    |
| PC 240 | 88              | 268       | 18,946    | 1,600     | 22,716    |
| PC 241 | 69              | 116       | 16,361    | 1,434     | 9,939     |
| PC 242 | ND              | 77        | 21,024    | 1,374     | 9,633     |
| PC 243 | 39              | 71        | 22,130    | 1,171     | 9,039     |
| PC 244 | 30              | 42        | 18,966    | 693       | 7,840     |
| PC 245 | 30              | 68        | 23,665    | 928       | 11,133    |
| PC 246 | 23              | 53        | 16,596    | 627       | 13,570    |
| PC 247 | 24              | 50        | 18,868    | 813       | 15,236    |
| PC 248 | 22              | 55        | 16,796    | 511       | 17,956    |
| PC 249 | ND              | 53        | 14,555    | 347       | 13,096    |
| PC 250 | 69              | 270       | 18,197    | 1,065     | 22,028    |
| PC 251 | 65              | 298       | 18,206    | 1,166     | 16,716    |
| PC 252 | 82              | 298       | 19,542    | 1,222     | 13,258    |
| PC 253 | 78              | 259       | 18,118    | 1,192     | 12,076    |
| PC 254 | 100             | 535       | 18,680    | 1,189     | 13,447    |
| PC 255 | 99              | 434       | 18,438    | 1,217     | 14,725    |
| PC 256 | 88              | 467       | 18,977    | 1,149     | 10,920    |
| PC 257 | 92              | 628       | 19,145    | 1,215     | 13,064    |
| PC 258 | 105             | 732       | 19,100    | 1,170     | 18,306    |
| PC 259 | 76              | 365       | 19,356    | 383       | 31,485    |
| PC 260 | 101             | 563       | 18,336    | 1,435     | 15,148    |
| PC 261 | 759             | 2,894     | 18,607    | 1,226     | 47,435    |
| PC 262 | 176             | 466       | 19,516    | 1,185     | 19,367    |
| PC 263 | 222             | 2,067     | 19,772    | 1,329     | 23,606    |
| PC 264 | 115             | 440       | 18,666    | 1,224     | 22,392    |
| ND     | Below detection |           |           |           |           |

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm       | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------------|-----------|-----------|-----------|-----------|
| PC 265 | 325             | 1,053     | 19,183    | 1,189     | 29,297    |
| PC 266 | 109             | 695       | 17,910    | 1,274     | 14,661    |
| PC 267 | 110             | 614       | 18,713    | 1,580     | 11,496    |
| PC 268 | 126             | 836       | 19,269    | 1,577     | 15,239    |
| PC 269 | 98              | 396       | 16,824    | 1,324     | 12,090    |
| PC 270 | 127             | 569       | 19,060    | 1,956     | 9,309     |
| PC 271 | 86              | 350       | 18,057    | 1,294     | 33,335    |
| PC 272 | 130             | 475       | 18,419    | 1,157     | 24,747    |
| PC 273 | 84              | 708       | 19,285    | 1,283     | 9,901     |
| PC 274 | 99              | 808       | 19,264    | 1,582     | 8,916     |
| PC 275 | 204             | 855       | 16,674    | 1,146     | 24,306    |
| PC 276 | 301             | 1,232     | 17,927    | 1,303     | 24,842    |
| PC 277 | 62              | 266       | 18,046    | 1,240     | 9,433     |
| PC 278 | 80              | 291       | 18,349    | 1,194     | 6,934     |
| PC 279 | 159             | 550       | 17,501    | 1,221     | 9,355     |
| PC 280 | 598             | 988       | 17,656    | 1,358     | 26,965    |
| PC 281 | 315             | 865       | 17,126    | 1,347     | 21,514    |
| PC 282 | 272             | 501       | 20,194    | 1,105     | 25,163    |
| PC 283 | 101             | 249       | 20,631    | 1,015     | 12,613    |
| PC 284 | 33              | 76        | 16,918    | 529       | 10,395    |
| PC 285 | 26              | 78        | 17,667    | 379       | 15,470    |
| PC 286 | 91              | 460       | 17,186    | 1,150     | 15,336    |
| PC 287 | 118             | 564       | 17,883    | 1,305     | 10,338    |
| PC 288 | 159             | 800       | 17,407    | 1,293     | 10,122    |
| PC 289 | 335             | 790       | 17,516    | 1,222     | 19,064    |
| PC 290 | 66              | 196       | 17,001    | 1,131     | 9,125     |
| PC 291 | 24              | 91        | 19,286    | 1,024     | 4,699     |
| PC 292 | ND              | 71        | 19,812    | 883       | 3,123     |
| PC 293 | 20              | 67        | 20,052    | 962       | 3,091     |
| PC 294 | 30              | 74        | 20,218    | 1,154     | 4,185     |
| PC 295 | 30              | 83        | 23,161    | 1,549     | 3,673     |
| PC 296 | 23              | 87        | 20,888    | 197       | 2,806     |
| PC 297 | 28              | 77        | 20,213    | 158       | 2,467     |
| PC 298 | 24              | 80        | 19,347    | 448       | 2,647     |
| PC 299 | 19              | 83        | 20,520    | 117       | 2,836     |
| PC 300 | 88              | 677       | 19,156    | 1,189     | 38,953    |
| PC 301 | 86              | 875       | 19,138    | 1,142     | 21,625    |
| PC 302 | 82              | 366       | 18,378    | 1,235     | 13,435    |
| ND     | Below detection |           |           |           |           |

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm       | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------------|-----------|-----------|-----------|-----------|
| PC 303 | ND              | 85        | 19,451    | 1,228     | 7,081     |
| PC 304 | 23              | 139       | 19,391    | 1,244     | 4,064     |
| PC 305 | ND              | 68        | 21,444    | 1,445     | 4,074     |
| PC 306 | ND              | 71        | 21,105    | 1,972     | 2,843     |
| PC 307 | 47              | 121       | 14,735    | 1,359     | 3,735     |
| PC 308 | 41              | 106       | 15,794    | 1,404     | 1,724     |
| PC 309 | 28              | 60        | 15,303    | 1,310     | 1,715     |
| PC 310 | 27              | 55        | 18,949    | 824       | 2,064     |
| PC 311 | 35              | 60        | 23,992    | 393       | 1,636     |
| PC 312 | 31              | 60        | 23,814    | 546       | 1,676     |
| PC 313 | 58              | 202       | 18,371    | 1,166     | 15,517    |
| PC 314 | 45              | 113       | 17,892    | 1,219     | 5,463     |
| PC 315 | 29              | 64        | 19,340    | 1,076     | 6,719     |
| PC 316 | 28              | 71        | 19,896    | 1,094     | 3,924     |
| PC 317 | 23              | 67        | 19,457    | 1,012     | 3,373     |
| PC 318 | ND              | 75        | 19,860    | 1,089     | 3,003     |
| PC 319 | ND              | 73        | 20,080    | 1,069     | 3,258     |
| PC 320 | 26              | 66        | 19,722    | 1,186     | 2,577     |
| PC 321 | 28              | 68        | 21,312    | 4,172     | 3,080     |
| PC 322 | 25              | 74        | 21,288    | 4,958     | 3,281     |
| PC 323 | 28              | 79        | 21,607    | 2,007     | 3,725     |
| PC 324 | 26              | 85        | 19,226    | 462       | 2,889     |
| PC 325 | 188             | 1,485     | 20,526    | 1,433     | 24,857    |
| PC 326 | 3,236           | 12,395    | 23,918    | 1,219     | 106,690   |
| PC 327 | 824             | 5,822     | 20,555    | 1,280     | 54,481    |
| PC 328 | 716             | 5,803     | 18,476    | 1,271     | 34,746    |
| PC 329 | 1,071           | 5,010     | 22,170    | 1,489     | 65,412    |
| PC 330 | 1,004           | 5,487     | 21,662    | 1,351     | 57,465    |
| PC 331 | 33              | 322       | 17,117    | 1,174     | 15,210    |
| PC 332 | 50              | 207       | 16,130    | 1,124     | 6,954     |
| PC 333 | 94              | 517       | 19,285    | 1,505     | 4,737     |
| PC 334 | 137             | 1,027     | 23,655    | 1,670     | 9,929     |
| PC 335 | 219             | 609       | 16,316    | 1,214     | 8,971     |
| PC 336 | 64              | 190       | 18,481    | 1,221     | 5,245     |
| PC 337 | 26              | 77        | 18,756    | 1,150     | 3,099     |
| PC 338 | 28              | 75        | 19,448    | 1,017     | 2,113     |
| PC 339 | 21              | 84        | 20,281    | 826       | 2,774     |
| PC 340 | 28              | 80        | 21,137    | 724       | 2,400     |
| ND     | Below detection |           |           |           |           |

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 341 | 76        | 203       | 18,702    | 1,298     | 13,784    |
| PC 342 | 56        | 120       | 16,714    | 1,225     | 5,162     |
| PC 343 | 24        | 40        | 16,855    | 1,364     | 7,141     |
| PC 344 | 31        | 64        | 20,655    | 1,081     | 9,905     |
| PC 345 | 78        | 235       | 18,115    | 1,244     | 11,516    |
| PC 346 | 36        | 105       | 17,781    | 1,075     | 3,983     |
| PC 347 | 22        | 72        | 18,977    | 892       | 2,853     |
| PC 348 | 23        | 67        | 19,028    | 1,141     | 2,799     |
| PC 349 | 46        | 119       | 16,803    | 1,023     | 6,552     |
| PC 350 | 47        | 173       | 14,883    | 937       | 1,506     |
| PC 351 | 71        | 230       | 14,424    | 967       | 2,666     |
| PC 352 | 157       | 410       | 16,361    | 1,105     | 9,262     |
| PC 353 | 184       | 542       | 16,985    | 1,206     | 12,678    |
| PC 354 | 88        | 241       | 16,147    | 1,097     | 4,576     |
| PC 355 | 88        | 138       | 15,207    | 1,189     | 4,406     |
| PC 356 | 73        | 136       | 17,144    | 1,262     | 6,488     |
| PC 357 | 39        | 81        | 16,347    | 1,288     | 5,518     |
| PC 358 | ND        | 53        | 17,151    | 1,355     | 6,430     |
| PC 359 | 25        | 56        | 16,893    | 1,195     | 7,715     |
| PC 360 | 21        | 52        | 16,049    | 1,129     | 4,558     |
| PC 361 | 21        | 62        | 18,075    | 906       | 3,992     |
| PC 362 | 28        | 72        | 20,736    | 1,328     | 3,560     |
| PC 363 | 24        | 68        | 20,702    | 813       | 3,100     |
| PC 364 | 31        | 70        | 19,816    | 344       | 3,567     |
| PC 365 | 21        | 75        | 14,957    | ND        | 4,572     |
| PC 366 | 106       | 661       | 19,205    | 1,346     | 36,861    |
| PC 367 | 74        | 323       | 18,484    | 1,274     | 17,365    |
| PC 368 | 115       | 737       | 19,447    | 1,543     | 11,724    |
| PC 369 | 358       | 1,522     | 18,110    | 1,355     | 29,874    |
| PC 370 | 379       | 1,567     | 17,329    | 1,265     | 26,887    |
| PC 371 | 627       | 1,905     | 18,679    | 1,288     | 45,826    |
| PC 372 | 239       | 1,439     | 18,126    | 1,231     | 30,960    |
| PC 373 | ND        | 134       | 18,070    | 1,124     | 7,227     |
| PC 374 | ND        | 193       | 19,125    | 944       | 4,528     |
| PC 375 | 23        | 89        | 19,560    | 973       | 3,692     |
| PC 376 | 33        | 112       | 19,474    | 997       | 3,499     |
| PC 377 | 30        | 78        | 20,070    | 975       | 4,292     |
| PC 378 | ND        | 80        | 20,494    | 1,027     | 3,541     |

ND Below detection

Appendix C-1 Continued. Pb, Zn, Fe, Mn, and Ca geochemical data used in this study.

| Sample | Pb<br>ppm | Zn<br>ppm | Fe<br>ppm | Mn<br>ppm | Ca<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 379 | 25        | 84        | 21,099    | 922       | 3,493     |
| PC 380 | 25        | 111       | 20,973    | 1,081     | 2,913     |
| PC 381 | 28        | 73        | 22,849    | 487       | 2,717     |
| PC 382 | 23        | 78        | 24,092    | 268       | 3,574     |
| PC 383 | 18        | 69        | 13,778    | ND        | 3,273     |
| PC 384 | 22        | 78        | 13,975    | ND        | 3,427     |
| PC 385 | 128       | 481       | 17,186    | 1,316     | 8,563     |
| PC 386 | 217       | 1,003     | 16,306    | 1,283     | 12,741    |
| PC 387 | 143       | 301       | 16,831    | 1,203     | 10,533    |
| PC 388 | 192       | 488       | 17,296    | 1,296     | 14,949    |
| PC 389 | ND        | 64        | 17,449    | 1,368     | 4,242     |
| PC 390 | 23        | 43        | 15,250    | 1,276     | 1,885     |
| PC 391 | ND        | 36        | 15,342    | 1,493     | 1,907     |
| PC 392 | 18        | 32        | 14,312    | 1,365     | 1,202     |
| PC 393 | ND        | 62        | 17,716    | 977       | 12,806    |
| PC 394 | ND        | 78        | 19,783    | 1,669     | 19,624    |
| PC 395 | 19        | 60        | 17,590    | 702       | 11,054    |
| PC 396 | 31        | 64        | 19,360    | 1,235     | 12,888    |
| PC 397 | 28        | 54        | 22,201    | 1,284     | 3,809     |
| PC 398 | 21        | 54        | 20,828    | 956       | 3,748     |

ND Below detection

Appendix C-2. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 1   | 4,962     | ND        | 58        | 514       | 23        |
| PC 2*  | 4,541     | 24        | 65        | 609       | 29        |
| PC 3*  | 5,029     | 65        | 66        | 616       | 34        |
| PC 4*  | 4,221     | 24        | 63        | 509       | 29        |
| PC 5*  | 4,123     | ND        | 61        | 603       | 34        |
| PC 6*  | 3,367     | 11        | 62        | 327       | 33        |
| PC 7*  | 4,667     | ND        | 73        | 545       | 30        |
| PC 8*  | 5,150     | ND        | 65        | 687       | 33        |
| PC 9   | 1,567     | 8         | 60        | 191       | 28        |
| PC 10  | 2,851     | 139       | 85        | 217       | 30        |
| PC 11  | 3,022     | 33        | 123       | 227       | 23        |
| PC 12  | 536       | 161       | 90        | 116       | 23        |
| PC 13  | 490       | 81        | 94        | 122       | 21        |
| PC 14  | 4,330     | 43        | 64        | 537       | 28        |
| PC 15  | 5,151     | 37        | 67        | 587       | 33        |
| PC 16  | 5,379     | 13        | 59        | 620       | 29        |
| PC 17  | 5,314     | 66        | 63        | 667       | 25        |
| PC 18  | 5,266     | 0         | 59        | 607       | 33        |
| PC 19  | 4,632     | 62        | 62        | 594       | 24        |
| PC 20  | 5,563     | ND        | 66        | 597       | 25        |
| PC 21  | 5,144     | 27        | 61        | 583       | 31        |
| PC 22  | 5,423     | 24        | 66        | 612       | 33        |
| PC 23  | 5,891     | 104       | 66        | 593       | 28        |
| PC 24  | 5,497     | 30        | 58        | 596       | 24        |
| PC 25  | 5,162     | 16        | 64        | 612       | 28        |
| PC 26  | 5,749     | 71        | 64        | 597       | 30        |
| PC 27  | 4,501     | 30        | 60        | 564       | 34        |
| PC 28  | 4,172     | ND        | 55        | 588       | 31        |
| PC 29  | 4,762     | ND        | 63        | 545       | 32        |
| PC 30  | 4,643     | 11        | 62        | 607       | 28        |
| PC 31  | 4,230     | 40        | 72        | 562       | 28        |
| PC 32  | 3,547     | 17        | 72        | 486       | 28        |
| PC 33  | 3,463     | 11        | 65        | 520       | 32        |
| PC 34  | 4,387     | 26        | 63        | 548       | 37        |
| PC 35  | 4,213     | ND        | 59        | 537       | 27        |
| PC 36  | 5,636     | 48        | 70        | 665       | 28        |
| PC 37  | 4,744     | 32        | 63        | 590       | 28        |
| PC 38  | 4,676     | 1         | 58        | 608       | 35        |

ND Below detection

\* Not used in study



Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 39  | 4,989     | 11        | 61        | 639       | 28        |
| PC 40  | 5,234     | 46        | 68        | 664       | 34        |
| PC 41  | 5,326     | 20        | 67        | 624       | 26        |
| PC 42  | 5,718     | ND        | 73        | 640       | 26        |
| PC 43  | 5,303     | 8         | 72        | 607       | 26        |
| PC 44  | 5,954     | 7         | 70        | 613       | 25        |
| PC 45  | 5,813     | 91        | 71        | 562       | 26        |
| PC 46  | 3,779     | 17        | 62        | 577       | 30        |
| PC 47  | 4,645     | 7         | 58        | 612       | 27        |
| PC 48  | 4,694     | 69        | 66        | 687       | 29        |
| PC 49  | 4,312     | ND        | 59        | 581       | 29        |
| PC 50  | 3,441     | 14        | 66        | 617       | 24        |
| PC 51  | 3,258     | 24        | 67        | 455       | 26        |
| PC 52  | 3,489     | 18        | 68        | 531       | 29        |
| PC 53  | 3,982     | 35        | 65        | 494       | 33        |
| PC 54  | 4,119     | 11        | 65        | 561       | 28        |
| PC 55  | 3,140     | ND        | 62        | 424       | 28        |
| PC 56  | 3,618     | 2         | 62        | 470       | 28        |
| PC 57  | 4,446     | ND        | 55        | 573       | 23        |
| PC 58  | 4,475     | ND        | 57        | 539       | 23        |
| PC 59  | 4,378     | 44        | 54        | 570       | 26        |
| PC 60  | 4,847     | 14        | 54        | 692       | 29        |
| PC 61  | 4,844     | 36        | 56        | 684       | 33        |
| PC 62  | 4,801     | 88        | 53        | 723       | 29        |
| PC 63  | 4,365     | 43        | 51        | 695       | 30        |
| PC 64  | 4,892     | ND        | 50        | 709       | 31        |
| PC 65  | 4,404     | 68        | 47        | 604       | 36        |
| PC 66  | 4,049     | 37        | 42        | 514       | 30        |
| PC 67  | 3,807     | 7         | 44        | 457       | 21        |
| PC 68  | 4,465     | ND        | 62        | 552       | 34        |
| PC 69  | 4,324     | 1         | 52        | 567       | 31        |
| PC 70  | 4,762     | 39        | 55        | 662       | 31        |
| PC 71  | 3,928     | 67        | 58        | 621       | 28        |
| PC 72  | 5,302     | 50        | 65        | 681       | 26        |
| PC 73  | 4,446     | 25        | 57        | 614       | 36        |
| PC 74  | 4,661     | ND        | 55        | 607       | 28        |
| PC 75  | 4,729     | 48        | 60        | 620       | 38        |
| PC 76  | 4,820     | ND        | 63        | 658       | 32        |
| PC 77  | 4,614     | 10        | 60        | 593       | 32        |

ND Below detection

Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 78  | 3,999     | 31        | 53        | 558       | 27        |
| PC 79  | 4,529     | 12        | 58        | 576       | 34        |
| PC 80  | 4,488     | 7         | 55        | 592       | 30        |
| PC 81  | 5,196     | 38        | 52        | 625       | 34        |
| PC 82  | 5,177     | 53        | 61        | 664       | 30        |
| PC 83  | 5,018     | ND        | 58        | 649       | 27        |
| PC 84  | 4,089     | ND        | 61        | 552       | 34        |
| PC 85  | 4,679     | ND        | 55        | 586       | 26        |
| PC 86  | 4,650     | ND        | 59        | 635       | 37        |
| PC 87  | 3,582     | ND        | 60        | 505       | 34        |
| PC 88  | 3,309     | 2         | 54        | 443       | 32        |
| PC 89  | 2,381     | 8         | 65        | 339       | 29        |
| PC 90  | 3,576     | 60        | 61        | 450       | 34        |
| PC 91  | 3,944     | ND        | 67        | 491       | 29        |
| PC 92  | 4,276     | ND        | 57        | 555       | 32        |
| PC 93  | 4,524     | ND        | 61        | 692       | 33        |
| PC 94  | 5,198     | 41        | 73        | 635       | 33        |
| PC 95  | 4,833     | ND        | 62        | 595       | 23        |
| PC 96  | 4,967     | 16        | 65        | 577       | 32        |
| PC 97  | 4,525     | 31        | 64        | 595       | 27        |
| PC 98  | 4,482     | 11        | 58        | 594       | 26        |
| PC 99  | 4,916     | 7         | 61        | 621       | 28        |
| PC 100 | 4,568     | ND        | 81        | 467       | 24        |
| PC 101 | 4,798     | 13        | 61        | 641       | 28        |
| PC 102 | 5,503     | 44        | 61        | 666       | 31        |
| PC 103 | 5,518     | 70        | 68        | 650       | 25        |
| PC 104 | 5,898     | 48        | 68        | 674       | 28        |
| PC 105 | 5,378     | 3         | 67        | 662       | 31        |
| PC 106 | 5,639     | 17        | 69        | 645       | 25        |
| PC 107 | 5,639     | 84        | 73        | 651       | 23        |
| PC 108 | 5,473     | ND        | 66        | 623       | 29        |
| PC 109 | 5,132     | ND        | 65        | 582       | 30        |
| PC 110 | 5,049     | 47        | 72        | 591       | 32        |
| PC 111 | 5,398     | 48        | 67        | 575       | 32        |
| PC 112 | 5,229     | 51        | 72        | 572       | 26        |
| PC 113 | 4,937     | 45        | 79        | 558       | 30        |
| PC 114 | 5,163     | 15        | 62        | 631       | 33        |
| PC 115 | 6,216     | 41        | 67        | 702       | 30        |
| PC 116 | 5,700     | 71        | 69        | 649       | 32        |

ND Below detection

Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 117 | 5,466     | ND        | 71        | 606       | 32        |
| PC 118 | 5,324     | 49        | 66        | 585       | 31        |
| PC 119 | 5,480     | 59        | 68        | 574       | 36        |
| PC 120 | 4,153     | ND        | 60        | 553       | 28        |
| PC 121 | 5,176     | 54        | 60        | 648       | 33        |
| PC 122 | 4,771     | 79        | 57        | 637       | 31        |
| PC 123 | 4,532     | 7         | 64        | 525       | 25        |
| PC 124 | 4,366     | 2         | 60        | 522       | 26        |
| PC 125 | 4,942     | 30        | 64        | 548       | 40        |
| PC 126 | 4,466     | ND        | 69        | 560       | 35        |
| PC 127 | 4,681     | 70        | 58        | 628       | 33        |
| PC 128 | 5,099     | ND        | 67        | 615       | 32        |
| PC 129 | 4,687     | ND        | 70        | 575       | 24        |
| PC 130 | 4,811     | ND        | 57        | 589       | 25        |
| PC 131 | 4,704     | 102       | 65        | 596       | 30        |
| PC 132 | 4,274     | ND        | 60        | 589       | 32        |
| PC 133 | 4,005     | 25        | 59        | 593       | 26        |
| PC 134 | 4,370     | 3         | 61        | 601       | 28        |
| PC 135 | 4,975     | 39        | 66        | 659       | 30        |
| PC 136 | 5,119     | ND        | 63        | 641       | 30        |
| PC 137 | 4,957     | 24        | 65        | 643       | 36        |
| PC 138 | 4,212     | ND        | 65        | 563       | 26        |
| PC 139 | 3,940     | 22        | 62        | 489       | 33        |
| PC 140 | 4,568     | 23        | 67        | 579       | 25        |
| PC 141 | 3,843     | 12        | 59        | 542       | 24        |
| PC 142 | 1,744     | 54        | 64        | 198       | 22        |
| PC 143 | 2,201     | 42        | 62        | 316       | 25        |
| PC 144 | 1,460     | 43        | 60        | 234       | 23        |
| PC 145 | 3,089     | 43        | 63        | 406       | 29        |
| PC 146 | 3,156     | 23        | 61        | 431       | 25        |
| PC 147 | 4,203     | ND        | 63        | 556       | 32        |
| PC 148 | 4,523     | 52        | 62        | 542       | 29        |
| PC 149 | 4,752     | 71        | 65        | 523       | 31        |
| PC 150 | 4,079     | 55        | 65        | 556       | 25        |
| PC 151 | 4,289     | 11        | 64        | 576       | 34        |
| PC 152 | 4,430     | ND        | 63        | 565       | 27        |
| PC 153 | 4,939     | ND        | 58        | 563       | 27        |
| PC 154 | 5,077     | ND        | 66        | 587       | 25        |
| PC 155 | 4,941     | 28        | 63        | 603       | 33        |

ND Below detection

Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 156 | 5,049     | 30        | 64        | 580       | 28        |
| PC 157 | 5,142     | 24        | 59        | 579       | 31        |
| PC 158 | 5,183     | 44        | 62        | 611       | 26        |
| PC 159 | 4,926     | 22        | 60        | 585       | 35        |
| PC 160 | 4,989     | 4         | 62        | 595       | 32        |
| PC 161 | 4,840     | 11        | 57        | 651       | 29        |
| PC 162 | 4,987     | 39        | 51        | 696       | 34        |
| PC 163 | 4,857     | 32        | 53        | 693       | 34        |
| PC 164 | 4,730     | 80        | 56        | 683       | 31        |
| PC 165 | 5,270     | 56        | 53        | 681       | 35        |
| PC 166 | 4,616     | 65        | 51        | 631       | 30        |
| PC 167 | 4,948     | 87        | 53        | 605       | 29        |
| PC 168 | 5,112     | ND        | 49        | 550       | 29        |
| PC 169 | 5,095     | 71        | 58        | 526       | 24        |
| PC 170 | 4,916     | 52        | 61        | 479       | 23        |
| PC 171 | 4,647     | 4         | 52        | 394       | 26        |
| PC 172 | 3,104     | 75        | 31        | 254       | 33        |
| PC 173 | 5,043     | ND        | 62        | 531       | 23        |
| PC 174 | 4,872     | 64        | 62        | 615       | 29        |
| PC 175 | 4,915     | 24        | 59        | 635       | 23        |
| PC 176 | 4,877     | 17        | 58        | 657       | 33        |
| PC 177 | 4,557     | 35        | 65        | 623       | 35        |
| PC 178 | 3,568     | ND        | 58        | 456       | 30        |
| PC 179 | 4,134     | 11        | 60        | 529       | 33        |
| PC 180 | 4,964     | 21        | 61        | 598       | 27        |
| PC 181 | 4,729     | 29        | 56        | 599       | 36        |
| PC 182 | 4,640     | 31        | 61        | 590       | 27        |
| PC 183 | 4,784     | ND        | 65        | 680       | 31        |
| PC 184 | 4,470     | 11        | 56        | 648       | 27        |
| PC 185 | 4,742     | 59        | 69        | 630       | 29        |
| PC 186 | 4,629     | 18        | 64        | 607       | 31        |
| PC 187 | 4,339     | 4         | 65        | 529       | 27        |
| PC 188 | 4,064     | 6         | 59        | 577       | 29        |
| PC 189 | 3,798     | 4         | 54        | 504       | 29        |
| PC 190 | 4,334     | ND        | 60        | 574       | 36        |
| PC 191 | 5,297     | 4         | 62        | 664       | 29        |
| PC 192 | 5,021     | 35        | 66        | 653       | 29        |
| PC 193 | 4,502     | ND        | 60        | 573       | 26        |
| PC 194 | 3,907     | ND        | 54        | 503       | 34        |

ND Below detection

Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 195 | 4,310     | 3         | 69        | 537       | 37        |
| PC 196 | 4,961     | 15        | 59        | 643       | 32        |
| PC 197 | 3,342     | 6         | 61        | 460       | 34        |
| PC 198 | 5,272     | ND        | 63        | 617       | 32        |
| PC 199 | 5,200     | 34        | 57        | 617       | 29        |
| PC 200 | 4,877     | 19        | 66        | 643       | 30        |
| PC 201 | 4,383     | ND        | 67        | 638       | 24        |
| PC 202 | 4,337     | 9         | 65        | 600       | 30        |
| PC 203 | 4,413     | 28        | 73        | 505       | 24        |
| PC 204 | 4,291     | 56        | 60        | 551       | 29        |
| PC 205 | 4,318     | 30        | 57        | 580       | 29        |
| PC 206 | 4,267     | ND        | 60        | 587       | 36        |
| PC 207 | 4,215     | ND        | 61        | 564       | 21        |
| PC 208 | 3,129     | 27        | 60        | 434       | 22        |
| PC 209 | 3,829     | 14        | 59        | 500       | 33        |
| PC 210 | 3,852     | 25        | 62        | 501       | 26        |
| PC 211 | 3,686     | 29        | 71        | 460       | 25        |
| PC 212 | 4,135     | 19        | 62        | 596       | 35        |
| PC 213 | 4,693     | 46        | 60        | 666       | 35        |
| PC 214 | 4,228     | 36        | 59        | 609       | 30        |
| PC 215 | 5,035     | 42        | 55        | 657       | 28        |
| PC 216 | 4,800     | 94        | 59        | 670       | 30        |
| PC 217 | 4,914     | 67        | 54        | 661       | 38        |
| PC 218 | 4,839     | 63        | 59        | 636       | 21        |
| PC 219 | 5,246     | 64        | 59        | 603       | 29        |
| PC 220 | 5,467     | 54        | 62        | 575       | 26        |
| PC 221 | 4,663     | 12        | 55        | 594       | 34        |
| PC 222 | 4,959     | 7         | 61        | 667       | 34        |
| PC 223 | 5,229     | 67        | 55        | 701       | 35        |
| PC 224 | 5,133     | 74        | 52        | 661       | 33        |
| PC 225 | 5,043     | 103       | 58        | 630       | 25        |
| PC 226 | 5,489     | 61        | 61        | 640       | 28        |
| PC 227 | 5,355     | 41        | 59        | 603       | 30        |
| PC 228 | 5,076     | 30        | 62        | 593       | 26        |
| PC 229 | 5,524     | 49        | 62        | 554       | 35        |
| PC 230 | 5,541     | 54        | 64        | 613       | 26        |
| PC 231 | 5,093     | 82        | 55        | 683       | 29        |
| PC 232 | 4,992     | ND        | 59        | 652       | 26        |
| PC 233 | 5,259     | ND        | 57        | 633       | 32        |

ND Below detection

Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 234 | 4,908     | 39        | 63        | 547       | 26        |
| PC 235 | 4,610     | ND        | 59        | 534       | 30        |
| PC 236 | 3,899     | 29        | 55        | 586       | 28        |
| PC 237 | 2,878     | 31        | 59        | 419       | 30        |
| PC 238 | 2,917     | ND        | 53        | 406       | 27        |
| PC 239 | 3,812     | ND        | 69        | 469       | 28        |
| PC 240 | 4,171     | ND        | 66        | 528       | 27        |
| PC 241 | 4,803     | 26        | 64        | 571       | 26        |
| PC 242 | 5,641     | 46        | 69        | 593       | 23        |
| PC 243 | 4,964     | 34        | 71        | 553       | 30        |
| PC 244 | 5,361     | ND        | 66        | 580       | 34        |
| PC 245 | 5,565     | 33        | 74        | 555       | 29        |
| PC 246 | 4,733     | 82        | 67        | 557       | 25        |
| PC 247 | 4,925     | 59        | 65        | 511       | 34        |
| PC 248 | 3,977     | 18        | 63        | 576       | 29        |
| PC 249 | 4,178     | 11        | 60        | 583       | 29        |
| PC 250 | 4,034     | 55        | 60        | 534       | 32        |
| PC 251 | 3,677     | ND        | 62        | 549       | 27        |
| PC 252 | 4,686     | 46        | 64        | 548       | 21        |
| PC 253 | 4,290     | 1         | 60        | 579       | 33        |
| PC 254 | 4,673     | 60        | 62        | 568       | 29        |
| PC 255 | 4,574     | 55        | 62        | 573       | 32        |
| PC 256 | 4,848     | 6         | 70        | 540       | 29        |
| PC 257 | 4,208     | 36        | 57        | 521       | 28        |
| PC 258 | 4,514     | ND        | 64        | 513       | 28        |
| PC 259 | 4,118     | 38        | 59        | 354       | 24        |
| PC 260 | 4,292     | 37        | 63        | 575       | 26        |
| PC 261 | 3,463     | 50        | 66        | 434       | 20        |
| PC 262 | 4,242     | ND        | 60        | 561       | 27        |
| PC 263 | 4,844     | ND        | 70        | 542       | 29        |
| PC 264 | 4,110     | ND        | 66        | 563       | 22        |
| PC 265 | 3,655     | ND        | 59        | 527       | 23        |
| PC 266 | 4,290     | ND        | 60        | 572       | 29        |
| PC 267 | 4,376     | 40        | 55        | 573       | 30        |
| PC 268 | 4,692     | ND        | 59        | 565       | 33        |
| PC 269 | 4,325     | 11        | 61        | 591       | 33        |
| PC 270 | 5,553     | ND        | 74        | 626       | 32        |
| PC 271 | 3,759     | 16        | 62        | 504       | 28        |
| PC 272 | 3,942     | ND        | 60        | 547       | 32        |

ND Below detection

Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 273 | 4,572     | 31        | 62        | 576       | 28        |
| PC 274 | 4,932     | 22        | 61        | 574       | 30        |
| PC 275 | 3,672     | ND        | 60        | 549       | 32        |
| PC 276 | 3,871     | 6         | 60        | 560       | 26        |
| PC 277 | 4,590     | 33        | 64        | 569       | 28        |
| PC 278 | 5,059     | 79        | 68        | 606       | 29        |
| PC 279 | 4,840     | 8         | 65        | 612       | 31        |
| PC 280 | 4,070     | ND        | 60        | 524       | 32        |
| PC 281 | 4,199     | ND        | 66        | 593       | 33        |
| PC 282 | 3,655     | ND        | 55        | 551       | 33        |
| PC 283 | 5,179     | 36        | 63        | 640       | 27        |
| PC 284 | 4,993     | 26        | 63        | 659       | 29        |
| PC 285 | 4,949     | ND        | 74        | 577       | 31        |
| PC 286 | 4,084     | 0         | 55        | 556       | 29        |
| PC 287 | 4,376     | 3         | 51        | 590       | 33        |
| PC 288 | 4,486     | 14        | 60        | 626       | 26        |
| PC 289 | 4,149     | 41        | 60        | 562       | 33        |
| PC 290 | 4,770     | 88        | 65        | 620       | 35        |
| PC 291 | 4,721     | 37        | 61        | 588       | 27        |
| PC 292 | 4,728     | 92        | 57        | 584       | 28        |
| PC 293 | 5,091     | 50        | 62        | 582       | 26        |
| PC 294 | 4,792     | 56        | 67        | 602       | 30        |
| PC 295 | 4,968     | 71        | 64        | 611       | 24        |
| PC 296 | 5,340     | 60        | 66        | 619       | 26        |
| PC 297 | 5,005     | 49        | 59        | 573       | 32        |
| PC 298 | 5,209     | 40        | 67        | 582       | 33        |
| PC 299 | 5,249     | 54        | 64        | 557       | 34        |
| PC 300 | 3,855     | 23        | 66        | 519       | 20        |
| PC 301 | 4,369     | 21        | 58        | 560       | 28        |
| PC 302 | 4,361     | 26        | 61        | 598       | 38        |
| PC 303 | 4,733     | ND        | 57        | 567       | 28        |
| PC 304 | 4,679     | 32        | 61        | 585       | 33        |
| PC 305 | 4,920     | 32        | 60        | 603       | 33        |
| PC 306 | 5,136     | 8         | 67        | 577       | 31        |
| PC 307 | 5,326     | 13        | 68        | 567       | 32        |
| PC 308 | 5,929     | 77        | 71        | 603       | 26        |
| PC 309 | 5,447     | 24        | 75        | 585       | 30        |
| PC 310 | 5,680     | 29        | 72        | 542       | 31        |
| PC 311 | 5,809     | 23        | 68        | 490       | 28        |

ND Below detection

Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 312 | 5,812     | 16        | 69        | 475       | 32        |
| PC 313 | 4,674     | ND        | 65        | 523       | 24        |
| PC 314 | 5,360     | 19        | 63        | 614       | 33        |
| PC 315 | 5,352     | 30        | 64        | 577       | 27        |
| PC 316 | 5,146     | 10        | 65        | 618       | 28        |
| PC 317 | 5,226     | 6         | 62        | 594       | 30        |
| PC 318 | 5,171     | 48        | 58        | 596       | 27        |
| PC 319 | 4,962     | 57        | 61        | 579       | 33        |
| PC 320 | 5,018     | 39        | 66        | 626       | 33        |
| PC 321 | 5,139     | 35        | 65        | 629       | 34        |
| PC 322 | 5,028     | 72        | 65        | 600       | 30        |
| PC 323 | 5,524     | 31        | 60        | 612       | 29        |
| PC 324 | 5,198     | 50        | 63        | 603       | 28        |
| PC 325 | 4,604     | 17        | 63        | 543       | 30        |
| PC 326 | 2,421     | 23        | 81        | 277       | 22        |
| PC 327 | 3,849     | ND        | 69        | 463       | 29        |
| PC 328 | 3,872     | ND        | 64        | 479       | 25        |
| PC 329 | 3,660     | ND        | 66        | 413       | 29        |
| PC 330 | 3,755     | ND        | 64        | 435       | 27        |
| PC 331 | 4,706     | ND        | 61        | 664       | 29        |
| PC 332 | 4,397     | ND        | 60        | 523       | 38        |
| PC 333 | 5,360     | 43        | 65        | 595       | 30        |
| PC 334 | 5,419     | 29        | 61        | 562       | 33        |
| PC 335 | 4,791     | 19        | 55        | 583       | 22        |
| PC 336 | 5,776     | 83        | 65        | 616       | 31        |
| PC 337 | 5,233     | 6         | 62        | 595       | 23        |
| PC 338 | 5,437     | 13        | 66        | 586       | 35        |
| PC 339 | 5,909     | 19        | 66        | 581       | 28        |
| PC 340 | 5,425     | 24        | 63        | 573       | 21        |
| PC 341 | 4,748     | 51        | 62        | 516       | 24        |
| PC 342 | 5,239     | 16        | 61        | 641       | 29        |
| PC 343 | 5,175     | ND        | 60        | 648       | 41        |
| PC 344 | 5,127     | ND        | 70        | 577       | 23        |
| PC 345 | 4,856     | ND        | 61        | 538       | 25        |
| PC 346 | 5,127     | 33        | 62        | 617       | 25        |
| PC 347 | 5,217     | 18        | 61        | 628       | 28        |
| PC 348 | 5,267     | 15        | 58        | 609       | 29        |
| PC 349 | 4,826     | 29        | 57        | 560       | 31        |
| PC 350 | 4,793     | 4         | 52        | 630       | 31        |

ND Below detection



Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 351 | 5,194     | 2         | 55        | 716       | 33        |
| PC 352 | 4,957     | ND        | 61        | 586       | 27        |
| PC 353 | 4,510     | 21        | 60        | 637       | 28        |
| PC 354 | 5,184     | 43        | 61        | 615       | 27        |
| PC 355 | 5,098     | 20        | 60        | 603       | 27        |
| PC 356 | 5,211     | 60        | 61        | 569       | 27        |
| PC 357 | 5,210     | 29        | 64        | 641       | 27        |
| PC 358 | 5,104     | 3         | 61        | 591       | 25        |
| PC 359 | 4,635     | 18        | 63        | 593       | 26        |
| PC 360 | 5,010     | ND        | 62        | 650       | 23        |
| PC 361 | 5,020     | 15        | 58        | 595       | 26        |
| PC 362 | 5,511     | 12        | 64        | 616       | 32        |
| PC 363 | 4,689     | 67        | 55        | 606       | 27        |
| PC 364 | 4,895     | 24        | 57        | 623       | 27        |
| PC 365 | 4,868     | 16        | 59        | 611       | 27        |
| PC 366 | 4,016     | ND        | 63        | 530       | 35        |
| PC 367 | 4,059     | 7         | 64        | 568       | 26        |
| PC 368 | 5,094     | 48        | 64        | 630       | 28        |
| PC 369 | 4,144     | 11        | 62        | 541       | 32        |
| PC 370 | 4,154     | 5         | 60        | 517       | 25        |
| PC 371 | 3,750     | 26        | 65        | 474       | 34        |
| PC 372 | 4,343     | ND        | 57        | 530       | 42        |
| PC 373 | 5,596     | 52        | 61        | 634       | 26        |
| PC 374 | 5,196     | 59        | 58        | 574       | 28        |
| PC 375 | 5,578     | 52        | 61        | 626       | 27        |
| PC 376 | 5,236     | 7         | 56        | 607       | 37        |
| PC 377 | 5,209     | ND        | 69        | 571       | 23        |
| PC 378 | 5,257     | ND        | 59        | 581       | 24        |
| PC 379 | 5,835     | 40        | 69        | 538       | 32        |
| PC 380 | 5,032     | 28        | 70        | 535       | 25        |
| PC 381 | 5,299     | 50        | 64        | 533       | 31        |
| PC 382 | 5,784     | 44        | 66        | 558       | 23        |
| PC 383 | 4,998     | 61        | 62        | 589       | 28        |
| PC 384 | 4,974     | 49        | 62        | 582       | 27        |
| PC 385 | 5,057     | ND        | 52        | 597       | 38        |
| PC 386 | 4,968     | 1         | 69        | 592       | 23        |
| PC 387 | 5,031     | 15        | 58        | 607       | 35        |
| PC 388 | 4,288     | ND        | 62        | 641       | 31        |
| PC 389 | 5,598     | 17        | 63        | 619       | 28        |

ND Below detection

Appendix C-2 Continued. Ti, Cr, Sr, Zr, and Mo geochemical data not used in this study.

| Sample | Ti<br>ppm | Cr<br>ppm | Sr<br>ppm | Zr<br>ppm | Mo<br>ppm |
|--------|-----------|-----------|-----------|-----------|-----------|
| PC 390 | 5,713     | 34        | 72        | 621       | 34        |
| PC 391 | 5,864     | ND        | 72        | 647       | 34        |
| PC 392 | 5,403     | ND        | 67        | 629       | 39        |
| PC 393 | 2,665     | 39        | 28        | 212       | 29        |
| PC 394 | 3,185     | ND        | 49        | 389       | 33        |
| PC 395 | 2,897     | 35        | 27        | 213       | 30        |
| PC 396 | 4,584     | ND        | 56        | 605       | 30        |
| PC 397 | 4,989     | 47        | 50        | 471       | 22        |
| PC 398 | 4,815     | 36        | 55        | 531       | 32        |

ND Below detection

**Total Carbon, Nitrogen, and Sulfur Analysis.** Carbon, Nitrogen, and Sulfur analysis was done with a Vario EL III CHNOS Elemental Analyzer per instructions from the standard operating procedures on 97 samples (OEWRI, 2007a). After sample preparation, approximately 20 mg of each sample were transferred into separate tin foil “boats,” formed into pellets using a hand press, and then loaded into the carousel. Two LDs, two foil blanks, and one natural standard were analyzed with each carousel. The foil-wrapped pellet is then dropped into the instrument where it undergoes catalytic combustion at 1150 C. The C, N, and S gases released are injected into a reduction tube where the vapors are cooled to 850 C and reduced into a detectable form. Water is removed from the gases via drying tubes and then separated into C, N, and S. Helium is used to carry nitrogen and sulfur to separate thermal conductivity detectors where the concentrations of each element are determined.

Appendix C-3. Carbon, nitrogen, and sulfur data

| Sample | Nitrogen (%) | Carbon (%) | Sulfur (%) | Nitrogen (mg) | Carbon (mg) | Sulfur (mg) |
|--------|--------------|------------|------------|---------------|-------------|-------------|
| PC 1   | 0.20         | 3.74       | 0.14       | 0.04          | 0.79        | 0.03        |
| PC 2*  | 0.26         | 3.09       | (0.09)     | 0.06          | 0.65        | 0.02        |
| PC 3*  | 0.15         | 2.41       | (0.09)     | 0.03          | 0.51        | 0.02        |
| PC 4*  | 0.10         | 3.17       | (0.07)     | 0.02          | 0.67        | 0.01        |
| PC 5*  | 0.11         | 2.68       | (0.04)     | 0.02          | 0.56        | 0.01        |
| PC 6*  | 0.08         | 5.31       | 0.26       | 0.02          | 1.12        | 0.06        |
| PC 7*  | 0.11         | 3.02       | (0.05)     | 0.02          | 0.64        | 0.01        |
| PC 8*  | 0.11         | 1.49       | (0.02)     | 0.02          | 0.31        | 0.00        |
| PC 9   | 0.07         | 7.65       | 0.15       | 0.01          | 1.61        | 0.03        |
| PC 10  | 0.04         | 6.13       | 0.12       | 0.01          | 1.31        | 0.03        |
| PC 11  | 0.06         | 7.93       | 0.24       | 0.01          | 1.68        | 0.05        |
| PC 12  | 0.06         | 9.33       | 0.55       | 0.01          | 1.97        | 0.12        |
| PC 13  | 0.04         | 8.06       | 0.40       | 0.01          | 1.70        | 0.08        |
| PC 14  | 0.36         | 4.33       | (0.04)     | 0.08          | 0.91        | 0.01        |
| PC 15  | 0.25         | 2.63       | (0.03)     | 0.05          | 0.55        | 0.01        |
| PC 16  | 0.14         | 1.35       | (0.02)     | 0.03          | 0.28        | 0.00        |

( ) Values below detection

\* Not used in study

Appendix C-3 Continued. Carbon, nitrogen, and sulfur data

| Sample | Nitrogen (%) | Carbon (%) | Sulfur (%) | Nitrogen (mg) | Carbon (mg) | Sulfur (mg) |
|--------|--------------|------------|------------|---------------|-------------|-------------|
| PC 17  | 0.12         | 1.41       | (0.02)     | 0.03          | 0.30        | 0.01        |
| PC 18  | 0.11         | 1.50       | (0.02)     | 0.02          | 0.32        | 0.00        |
| PC 19  | 0.14         | 2.06       | (0.03)     | 0.03          | 0.43        | 0.01        |
| PC 20  | 0.15         | 1.93       | (0.02)     | 0.03          | 0.41        | 0.00        |
| PC 21  | 0.16         | 1.55       | (0.02)     | 0.03          | 0.33        | 0.00        |
| PC 22  | 0.16         | 1.84       | (0.03)     | 0.03          | 0.39        | 0.01        |
| PC 23  | 0.13         | 1.24       | (0.02)     | 0.03          | 0.26        | 0.00        |
| PC 24  | 0.10         | 0.83       | (0.02)     | 0.02          | 0.18        | 0.00        |
| PC 25  | 0.09         | 0.74       | (0.02)     | 0.02          | 0.16        | 0.00        |
| PC 26  | 0.10         | 0.86       | (0.01)     | 0.02          | 0.18        | 0.00        |
| PC 27  | 0.24         | 3.02       | (0.03)     | 0.05          | 0.64        | 0.01        |
| PC 28  | 0.18         | 2.37       | (0.04)     | 0.04          | 0.50        | 0.01        |
| PC 29  | 0.14         | 2.11       | (0.08)     | 0.03          | 0.44        | 0.02        |
| PC 30  | 0.12         | 2.08       | (0.03)     | 0.03          | 0.44        | 0.01        |
| PC 31  | 0.10         | 3.00       | 0.26       | 0.02          | 0.63        | 0.05        |
| PC 32  | 0.10         | 5.01       | 0.33       | 0.02          | 1.06        | 0.07        |
| PC 33  | 0.09         | 3.32       | 0.09       | 0.02          | 0.70        | 0.02        |
| PC 34  | 0.10         | 2.01       | (0.04)     | 0.02          | 0.42        | 0.01        |
| PC 35  | 0.11         | 2.86       | 0.09       | 0.02          | 0.60        | 0.02        |
| PC 36  | 0.12         | 1.57       | (0.01)     | 0.03          | 0.33        | 0.00        |
| PC 37  | 0.16         | 1.76       | (0.02)     | 0.04          | 0.37        | 0.00        |
| PC 38  | 0.19         | 1.73       | (0.03)     | 0.04          | 0.36        | 0.01        |
| PC 39  | 0.27         | 2.57       | (0.03)     | 0.06          | 0.54        | 0.01        |
| PC 40  | 0.19         | 1.98       | (0.02)     | 0.04          | 0.42        | 0.00        |
| PC 41  | 0.12         | 1.06       | (0.01)     | 0.03          | 0.22        | 0.00        |
| PC 42  | 0.09         | 0.65       | (0.01)     | 0.02          | 0.14        | 0.00        |
| PC 43  | 0.06         | 0.38       | (0.01)     | 0.01          | 0.08        | 0.00        |
| PC 44  | 0.06         | 0.38       | (.)        | 0.01          | 0.08        | 0.00        |
| PC 45  | 0.06         | 0.33       | (.)        | 0.01          | 0.07        | 0.00        |
| PC 46  | 0.34         | 4.74       | (0.04)     | 0.07          | 1.00        | 0.01        |
| PC 47  | 0.18         | 2.15       | (0.03)     | 0.04          | 0.45        | 0.01        |
| PC 48  | 0.11         | 1.52       | (0.03)     | 0.02          | 0.32        | 0.01        |
| PC 49  | 0.12         | 2.20       | (0.04)     | 0.03          | 0.46        | 0.01        |
| PC 50  | 0.26         | 4.12       | (0.04)     | 0.06          | 0.87        | 0.01        |
| PC 51  | 0.10         | 3.85       | 0.07       | 0.02          | 0.81        | 0.01        |
| PC 52  | 0.12         | 3.70       | 0.05       | 0.03          | 0.78        | 0.01        |
| PC 53  | 0.12         | 3.23       | (0.02)     | 0.03          | 0.68        | 0.00        |
| PC 54  | 0.09         | 2.33       | (0.02)     | 0.02          | 0.49        | 0.00        |
| PC 55  | 0.09         | 4.22       | 0.06       | 0.02          | 0.89        | 0.01        |

(.) Values below detection

Appendix C-3 Continued. Carbon, nitrogen, and sulfur data

| Sample | Nitrogen (%) | Carbon (%) | Sulfur (%) | Nitrogen (mg) | Carbon (mg) | Sulfur (mg) |
|--------|--------------|------------|------------|---------------|-------------|-------------|
| PC 56  | 0.09         | 3.30       | (0.04)     | 0.02          | 0.70        | 0.01        |
| PC 57  | 0.11         | 1.92       | (0.02)     | 0.02          | 0.40        | 0.00        |
| PC 58  | 0.14         | 2.24       | 0.05       | 0.03          | 0.47        | 0.01        |
| PC 59  | 0.17         | 2.47       | 0.11       | 0.04          | 0.52        | 0.02        |
| PC 60  | 0.16         | 1.38       | (0.03)     | 0.03          | 0.29        | 0.01        |
| PC 61  | 0.16         | 1.16       | (0.02)     | 0.03          | 0.24        | 0.00        |
| PC 62  | (0.05)       | 0.31       | (0.01)     | 0.01          | 0.06        | 0.00        |
| PC 63  | (0.04)       | 0.26       | (0.01)     | 0.01          | 0.05        | 0.00        |
| PC 64  | (0.03)       | 0.22       | (0.01)     | 0.01          | 0.05        | 0.00        |
| PC 65  | (0.05)       | 0.25       | (0.01)     | 0.01          | 0.05        | 0.00        |
| PC 66  | (0.03)       | 0.23       | (.)        | 0.01          | 0.05        | 0.00        |
| PC 67  | (0.03)       | 0.18       | (0.01)     | 0.01          | 0.04        | 0.00        |
| PC 68  | 0.35         | 3.76       | (0.04)     | 0.07          | 0.79        | 0.01        |
| PC 69  | 0.21         | 1.90       | (0.02)     | 0.04          | 0.40        | 0.01        |
| PC 70  | 0.12         | 1.40       | (0.02)     | 0.03          | 0.30        | 0.01        |
| PC 71  | 0.15         | 1.70       | (0.02)     | 0.03          | 0.36        | 0.00        |
| PC 72  | 0.12         | 1.35       | (0.02)     | 0.03          | 0.28        | 0.00        |
| PC 73  | 0.12         | 1.87       | (0.02)     | 0.03          | 0.39        | 0.00        |
| PC 74  | 0.10         | 1.85       | (0.03)     | 0.02          | 0.39        | 0.01        |
| PC 75  | 0.12         | 1.67       | (0.03)     | 0.03          | 0.35        | 0.01        |
| PC 76  | 0.12         | 1.52       | (0.02)     | 0.03          | 0.32        | 0.00        |
| PC 77  | 0.12         | 1.35       | (0.02)     | 0.03          | 0.28        | 0.00        |
| PC 78  | 0.11         | 2.30       | (0.01)     | 0.02          | 0.48        | 0.00        |
| PC 79  | 0.13         | 1.48       | (0.01)     | 0.03          | 0.31        | 0.00        |
| PC 80  | 0.14         | 1.31       | (0.01)     | 0.03          | 0.28        | 0.00        |
| PC 81  | 0.11         | 1.07       | (0.01)     | 0.02          | 0.23        | 0.00        |
| PC 82  | 0.12         | 1.11       | (0.02)     | 0.03          | 0.23        | 0.00        |
| PC 83  | 0.12         | 1.15       | (0.02)     | 0.03          | 0.24        | 0.00        |
| PC 84  | 0.32         | 3.89       | (0.05)     | 0.07          | 0.82        | 0.01        |
| PC 85  | 0.21         | 2.20       | 0.08       | 0.05          | 0.46        | 0.02        |
| PC 86  | 0.14         | 1.48       | (0.04)     | 0.03          | 0.31        | 0.01        |
| PC 87  | 0.12         | 3.49       | 0.08       | 0.03          | 0.73        | 0.02        |
| PC 88  | 0.12         | 4.13       | 0.08       | 0.03          | 0.87        | 0.02        |
| PC 89  | (0.1)        | 5.41       | (0.06)     | 0.02          | 1.14        | 0.01        |
| PC 90  | (0.09)       | 4.01       | (0.05)     | 0.02          | 0.84        | 0.01        |
| PC 91  | 0.12         | 3.57       | (0.04)     | 0.03          | 0.75        | 0.01        |
| PC 92  | (0.11)       | 2.84       | (0.03)     | 0.02          | 0.60        | 0.01        |
| PC 93  | 0.13         | 1.29       | (0.02)     | 0.03          | 0.27        | 0.00        |
| PC 94  | (0.1)        | 1.25       | (0.02)     | 0.02          | 0.26        | 0.00        |

(.) Values below detection

Appendix C-3 Continued. Carbon, nitrogen, and sulfur data

| Sample | Nitrogen<br>(%) | Carbon<br>(%) | Sulfur<br>(%) | Nitrogen<br>(mg) | Carbon<br>(mg) | Sulfur<br>(mg) |
|--------|-----------------|---------------|---------------|------------------|----------------|----------------|
| PC 95  | (0.11)          | 1.38          | (0.02)        | 0.02             | 0.29           | 0.00           |
| PC 96  | 0.15            | 1.66          | (0.02)        | 0.03             | 0.35           | 0.00           |
| PC 97  | 0.15            | 1.84          | (0.02)        | 0.03             | 0.39           | 0.00           |

( ) Values below detection

**Inorganic and Organic Carbon Analysis.** Loss on ignition (LOI) was used in conjunction with the C-N-S analyzer to determine the concentration of organic carbon present per instructions in the standard operating procedures (OEWRI, 2007c). A five gram sample was measured, placed in a porcelain crucible, and put in a muffle furnace set to 400 C for 6 hours. The samples were removed, cooled, and a second CNS analysis was used to determine the remaining carbon in the sample. Organic carbon was calculated by subtracting post-LOI CNS analysis (inorganic carbon) data from pre-LOI CNS analysis (total carbon) data.

Twenty-five samples were analyzed for IC/OC to determine if Zn was bonded to organic matter or inorganic matter. Buried soil horizons contain high amounts of organic carbon in the form of organic matter while mining sediments contain high amounts of inorganic carbon in the form of limestone ( $\text{CaCO}_3$ ). CNS analysis does not distinguish between inorganic and organic carbon, making it is impossible to tell simply from the CNS results if a sample high in carbon is a buried soil or mining sediment. However, finding a relationship between Zn concentration and carbon is one way to distinguish between buried soils and mining sediment. If Zn is primarily bound to organic matter, a strong correlation will exist between Zn and organic carbon whereas a strong correlation between Zn and inorganic carbon will exist if Zn is primarily bound to the mining sediment (limestone). Figure C-1 shows total, inorganic, and organic carbon in relation to Zn (Appendix C.4). Samples used in the analysis were diverse in their Zn content, carbon content, and position in the core (top and bottom of core). The goal was to get a representative sample between mining sediment and the current organic-rich A horizon at the surface. The results show that Zn has a moderate positive correlation with total carbon ( $R^2=0.54$ ), a strong positive correlation with inorganic carbon ( $R^2=0.83$ ), and

nearly zero correlation with organic carbon ( $R^2=0.0019$ ). Based on these results, both mining sediment and buried soils contain high total carbon, however, mining sediment is characterized by high Zn concentrations while buried soils are characterized by low Zn concentrations. Therefore, buried horizons can be distinguished by the absence of Zn and mining sediment can be distinguished by the presence of Zn. Loss on ignition analysis of future samples would therefore not be necessary.



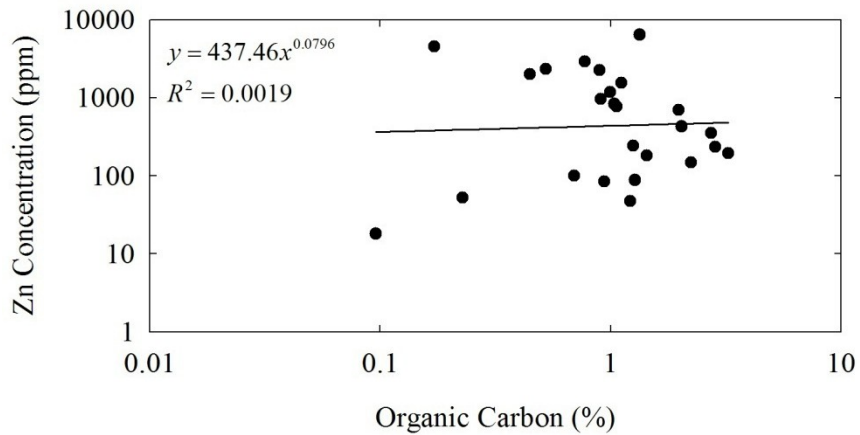
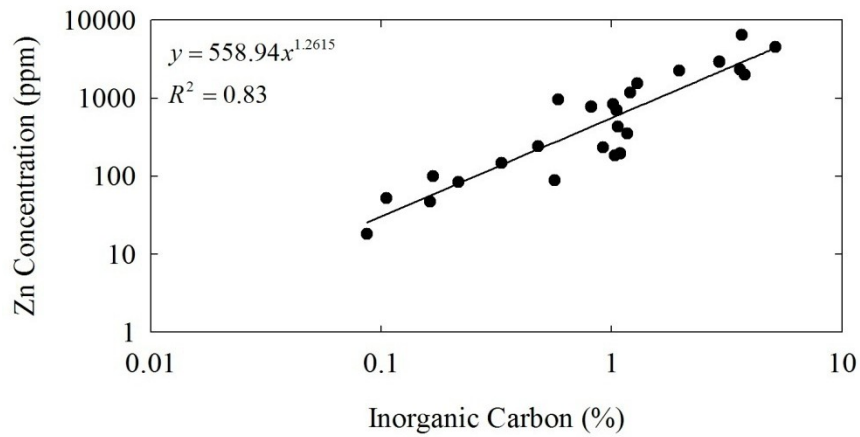
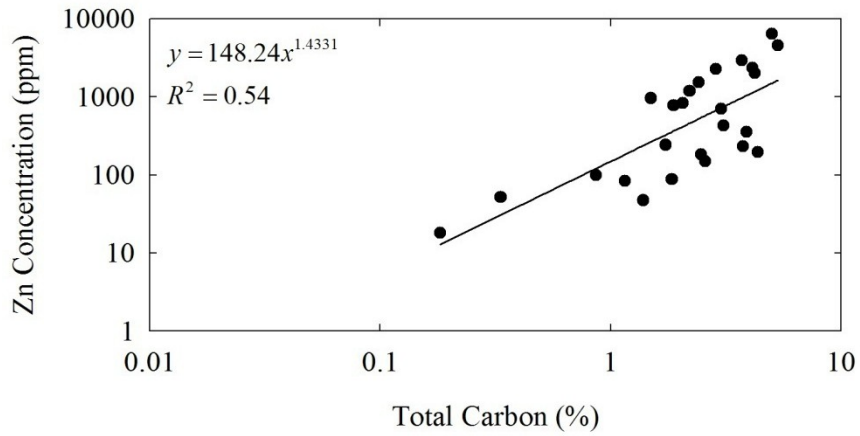


Figure C-1. Loss on ignition results for (A) total, (B) inorganic, and (C) organic carbon. The strong relationship between Zn and inorganic carbon indicates that Zn is primarily bonded to tailings sediment.

Appendix C-4. Total, inorganic, and organic carbon data from CNS and LOI analysis.

| Sample | Total Carbon (%) | Inorganic Carbon (%) | Organic Carbon (%) |
|--------|------------------|----------------------|--------------------|
| PC 14  | 4.33             | 1.09                 | 3.24               |
| PC 19  | 2.06             | 1.01                 | 1.04               |
| PC 2   | 3.09             | 1.06                 | 2.03               |
| PC 26  | 0.86             | 0.17                 | 0.70               |
| PC 27  | 3.02             | 1.05                 | 1.97               |
| PC 3   | 2.41             | 1.29                 | 1.12               |
| PC 32  | 5.01             | 3.67                 | 1.34               |
| PC 35  | 2.86             | 1.97                 | 0.90               |
| PC 38  | 1.73             | 0.48                 | 1.25               |
| PC 39  | 2.57             | 0.33                 | 2.23               |
| PC 45  | 0.33             | 0.11                 | 0.23               |
| PC 49  | 2.20             | 1.21                 | 0.99               |
| PC 52  | 3.70             | 2.93                 | 0.77               |
| PC 55  | 4.22             | 3.77                 | 0.45               |
| PC 59  | 2.47             | 1.03                 | 1.43               |
| PC 6   | 5.31             | 5.14                 | 0.17               |
| PC 60  | 1.38             | 0.16                 | 1.22               |
| PC 67  | 0.18             | 0.09                 | 0.10               |
| PC 68  | 3.76             | 0.92                 | 2.84               |
| PC 73  | 1.87             | 0.82                 | 1.06               |
| PC 8   | 1.49             | 0.59                 | 0.91               |
| PC 83  | 1.15             | 0.22                 | 0.94               |
| PC 84  | 3.89             | 1.17                 | 2.73               |
| PC 88  | 4.13             | 3.60                 | 0.52               |
| PC 97  | 1.84             | 0.57                 | 1.28               |

## **Appendix D. Cross-section Data**

All cross-section data start on river left (looking downstream) and proceed toward river right across the channel. References to banks (right or left) are also in relation to looking downstream. Elevation and depth to refusal are given as elevations relative to the thalweg elevation. Notes highlight key landforms, benchmarks, or other observations along the cross-section.

Appendix D-1. Cross-section data for Site 1A.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                                    |
|-------------|------------------------------------|----------------------------------|--|
| 0.0         | 2.65                               | 0.30                             | Edge of field                            |
| 5.0         | 2.72                               | 0.20                             |  |
| 10.0        | 2.44                               | 1.00                             | Rebar stake                              |
| 11.0        | 2.42                               |                                  |  |
| 15.0        | 2.08                               |                                  |  |
| 18.0        | 2.07                               |                                  |  |
| 20.0        | 2.02                               |                                  |  |
| 21.9        | 2.04                               | 1.85                             | Top of left bank                         |
| 21.95       | 2.01                               |                                  | Bench mark stake (ground)                |
| 22.5        | 1.87                               |                                  |  |
| 23.0        | 1.00                               |                                  |  |
| 23.8        | 0.00                               |                                  |  |
| 24.9        | 0.00                               | 0.05                             | Thalweg                                  |
| 27.6        | 0.07                               |                                  | Bed/bar                                  |
| 29.9        | 0.55                               |                                  | Bar crest                                |
| 31.0        | 0.60                               |                                  |  |
| 33.7        | 0.90                               |                                  |  |
| 35.7        | 1.02                               | 0.70                             | Base of fines                            |
| 36.9        | 1.37                               |                                  |  |
| 38.5        | 1.70                               |                                  |  |
| 39.3        | 2.16                               |                                  | Top of right bank                        |
| 39.6        | 2.17                               |                                  |  |
| 40.5        | 2.12                               |                                  |  |
| 42.4        | 1.05                               | 0.45                             | Scour hole/old cut                       |
| 43.4        | 1.11                               |                                  | Scour hole/old cut                       |
| 45.3        | 1.40                               |                                  |  |
| 47.0        | 1.87                               |                                  |  |
| 51.5        | 2.78                               |                                  | Tree high water mark; off the tape       |
| 52.0        |                                    |                                  | Bench mark stake                         |
| 52.6        | 1.75                               | 0.43                             |  |
| 54.4        | 1.45                               |                                  |  |
| 56.0        |                                    | 0.30                             |  |
| 58.4        | 1.47                               |                                  |  |
| 58.7        | 1.77                               |                                  | LT old tree (pedestal)                   |
| 60.3        | 1.97                               | 0.70                             | LT old tree base top                     |
| 60.35       | 2.21                               |                                  | Bench mark tree notch; 1 m south of tape |
| 60.8        | 1.95                               |                                  | Pedestal                                 |
| 61.7        | 1.62                               |                                  |  |
| 66.3        | 1.36                               | 0.30                             |  |
| 70.9        | 1.42                               |                                  |  |
| 72.7        | 1.99                               |                                  | Pedestal- dead tree                      |
| 74.2        | 1.98                               |                                  | Pedestal- dead tree                      |
| 76.7        | 1.12                               | 0.30                             |  |
| 77.15       | 1.18                               |                                  |  |

Appendix D-1 Continued. Cross-section data for Site 1A.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                        |
|-------------|------------------------------------|----------------------------------|------------------------------|
| 78.5        | 1.72                               |                                  |                              |
| 78.8        | 1.74                               |                                  | Pedestal 5m ds of tape, base |
| 80.0        | 1.12                               |                                  | High point, 5m ds of tape    |
| 80.6        | 1.88                               |                                  |                              |
| 82.0        | 2.19                               | 1.00                             | 5m ds of tape                |
| 82.7        | 0.93                               |                                  |                              |
| 83.0        | 1.12                               |                                  | High pt 5m ds of tape        |
| 83.7        | 0.90                               | 0.30                             |                              |
| 85.0        | 1.34                               |                                  | Pedestal 5m ds of tape, base |
| 88.3        | 1.25                               |                                  |                              |
| 92.0        |                                    | 0.30                             |                              |
| 97.8        | 1.34                               | 1.44                             |                              |
| 103.0       | 1.04                               | 0.57                             |                              |
| 105.0       | 1.52                               |                                  |                              |
| 105.0       | 1.26                               |                                  |                              |
| 106.0       | 2.15                               |                                  |                              |
| 107.5       | 2.30                               |                                  |                              |
| 110.2       | 1.67                               |                                  |                              |
| 115.0       | 1.42                               |                                  |                              |
| 119.0       | 1.24                               |                                  |                              |
| 130.0       | 1.67                               |                                  | Right of way                 |
| 133.0       | 1.98                               |                                  | Right of way                 |
| 140.0       | 2.07                               |                                  | Right of way                 |
| 146.0       | 2.37                               |                                  |                              |
| 146.0       | 2.69                               |                                  | Tree notch at end of survey  |

Appendix D-2. Cross-section data for Site 1B.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                            |
|-------------|------------------------------------|----------------------------------|----------------------------------|
| 0.0         | 2.32                               | 1.92                             |                                  |
| 7.0         | 2.66                               |                                  |                                  |
| 9.0         | 2.78                               | 0.38                             | 7.5YR at 65 cm                   |
| 11.7        | 2.735                              |                                  |                                  |
| 13.4        | 2.98                               |                                  |                                  |
| 14.6        | 2.90                               |                                  |                                  |
| 16.0        | 2.86                               | 0.56                             | Top of left bank; 7.5YR at 65 cm |
| 17.6        | 2.81                               |                                  | Top of stake                     |
| 19.5        | 2.02                               |                                  |                                  |
| 20.0        |                                    | 1.03                             |                                  |
| 21.3        | 1.60                               |                                  |                                  |
| 22.0        | 1.46                               | 0.82                             |                                  |
| 23.0        | 1.34                               |                                  |                                  |
| 23.8        | 1.28                               | 0.98                             | Edge of water                    |
| 24.6        | 0.92                               |                                  |                                  |
| 26.0        | 0.60                               |                                  |                                  |
| 27.5        | 0.72                               | -0.28                            |                                  |
| 29.0        | 0.54                               |                                  |                                  |
| 30.4        | 0.15                               |                                  |                                  |
| 32.0        | 0.00                               | -0.10                            |                                  |
| 33.1        | 0.18                               |                                  | Edge of water                    |
| 33.2        | 1.51                               |                                  |                                  |
| 34.1        | 2.12                               |                                  | Top of right bank                |
| 35.0        | 2.20                               |                                  |                                  |
| 37.0        | 2.24                               | 0.48                             |                                  |
| 38.3        | 2.29                               |                                  |                                  |
| 40.0        | 2.12                               |                                  |                                  |
| 42.0        | 1.91                               |                                  |                                  |
| 43.0        | 1.78                               |                                  |                                  |
| 44.0        | 1.61                               | -0.21                            |                                  |
| 46.0        | 1.60                               |                                  |                                  |
| 47.5        | 1.60                               |                                  |                                  |
| 48.7        | 1.65                               |                                  |                                  |
| 50.0        | 1.68                               |                                  |                                  |
| 53.0        | 1.57                               | 1.04                             |                                  |
| 56.0        | 1.54                               | 0.44                             |                                  |
| 58.0        | 1.64                               |                                  |                                  |

Appendix D-2 Continued. Cross-section data for Site 1B.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                          |
|-------------|------------------------------------|----------------------------------|--------------------------------|
| 60.7        | 1.47                               |                                  |                                |
| 62.0        | 1.37                               |                                  |                                |
| 64.0        | 1.32                               |                                  |                                |
| 65.0        | 1.34                               |                                  |                                |
| 68.0        | 1.25                               |                                  |                                |
| 72.0        | 1.12                               |                                  |                                |
| 74.4        | 1.17                               |                                  |                                |
| 77.0        | 1.28                               | 0.32                             |                                |
| 80.9        | 1.19                               |                                  |                                |
| 83.0        | 1.14                               |                                  |                                |
| 89.0        | 0.94                               | -0.41                            | Center of scoured channel      |
| 94.0        | 0.97                               | 0.29                             | Toe of scoured channel         |
| 96.0        | 1.13                               | 0.41                             |                                |
| 97.4        | 1.56                               |                                  |                                |
| 100.0       | 1.46                               | 0.26                             |                                |
| 102.0       | 1.55                               |                                  |                                |
| 102.8       | 1.98                               |                                  | Top of bank of scoured channel |
| 104.0       | 2.03                               |                                  |                                |
| 107.0       | 2.01                               |                                  | Bench mark stake (ground)      |
| 110.0       | 1.99                               | -0.61                            |                                |
| 112.0       | 1.98                               |                                  |                                |
| 114.0       | 1.93                               |                                  |                                |
| 118.0       | 1.90                               | 0.68                             |                                |
| 122.0       | 1.85                               |                                  |                                |
| 123.7       | 1.66                               |                                  |                                |
| 128.0       | 1.45                               | 0.35                             | Flood chute?                   |
| 133.5       | 1.74                               |                                  |                                |
| 135.0       | 1.89                               |                                  |                                |
| 138.0       | 1.97                               |                                  |                                |
| 143.0       | 2.09                               |                                  |                                |
| 148.0       | 2.23                               |                                  |                                |
| 153.0       | 2.23                               | 0.63                             |                                |
| 156.5       | 2.28                               | 2.12                             |                                |
| 159.5       | 2.43                               | 2.14                             |                                |
| 162.0       | 2.38                               |                                  |                                |
| 166.0       | 2.48                               |                                  |                                |
| 169.0       | 2.53                               | 2.37                             |                                |

Appendix D-2 Continued. Cross-section data for Site 1B.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                |
|-------------|------------------------------------|----------------------------------|----------------------|
| 172.0       | 2.70                               |                                  |                      |
| 175.0       | 2.83                               |                                  |                      |
| 178.0       | 2.93                               |                                  | Rebar stake (ground) |
| 196.0       | 3.18                               |                                  |                      |



Appendix D-3. Cross-section data for Site 2.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                                    |
|-------------|------------------------------------|----------------------------------|--|
| 0.0         | 3.23                               | 2.73                             |  |
| 6.0         |                                    | 2.55                             |  |
| 13.0        |                                    | 2.35                             |  |
| 18.0        | 2.87                               | 1.87                             |  |
| 23.0        |                                    | 1.72                             |  |
| 30.0        |                                    | 1.72                             |  |
| 43.0        | 2.57                               | 0.77                             |  |
| 66.0        | 2.72                               | 0.82                             | Edge of field                            |
| 82.0        | 2.11                               | 1.71                             |  |
| 86.0        |                                    | 1.81                             |  |
| 91.3        | 1.91                               | 1.21                             | Center of flood chute                    |
| 101.0       |                                    | 1.99                             |  |
| 102.9       | 2.20                               | -0.37                            |  |
| 105.0       |                                    | 1.73                             |  |
| 105.7       | 2.03                               |                                  | Edge of trail                            |
| 106.7       | 1.78                               |                                  | Bench mark stake on left bank            |
| 107.0       | 1.47                               |                                  | Top of left bank                         |
| 108.6       | 0.39                               | 0.39                             | Toe, boulders in bank                    |
| 110.2       | 0.24                               |                                  |  |
| 112.9       | 0.11                               |                                  |  |
| 114.3       | 0.00                               | -0.90                            | Thalweg                                  |
| 120.4       | 0.32                               |                                  |  |
| 120.8       | 0.58                               |                                  | Toe                                      |
| 120.9       | 1.54                               | 0.54                             | Top of right bank                        |
| 122.5       | 2.11                               |                                  |  |
| 124.0       |                                    | 1.39                             |  |
| 124.3       | 2.19                               |                                  | Top of colluvium?                        |
| 127.0       | 2.80                               |                                  | Crest of colluvium?                      |
| 129.1       | 3.25                               |                                  | Bench mark stake (ground), base of bluff |

Appendix D-4. Cross-section data for Site 3A.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                                   |
|-------------|------------------------------------|----------------------------------|---|
| 0.0         | 2.74                               | 1.84                             |   |
| 15.0        | 2.64                               | 1.74                             |   |
| 30.1        | 2.71                               |                                  |   |
| 36.4        | 2.58                               | 0.98                             | Fence near edge of field                |
| 38.7        | 2.55                               |                                  |   |
| 46.0        | 1.75                               | -0.90                            |   |
| 49.2        | 1.74                               |                                  | Center of flood chute                   |
| 53.7        | 1.84                               |                                  |   |
| 58.0        | 2.12                               |                                  |   |
| 65.3        | 2.00                               | -0.67                            | Bench mark stake (ground)               |
| 68.0        | 2.04                               |                                  |   |
| 70.5        | 2.02                               |                                  | Top of left bank                        |
| 71.4        | 0.46                               |                                  | Toe                                     |
| 75.3        | 0.58                               |                                  |   |
| 76.1        | 0.08                               |                                  |   |
| 76.9        | 0.00                               | -1.79                            | Thalweg                                 |
| 78.0        | 0.28                               |                                  | Edge of bar                             |
| 80.2        | 0.30                               |                                  |   |
| 81.7        | 0.50                               |                                  |   |
| 84.4        | 0.70                               |                                  | Large debris jam on right bank          |
| 85.3        | 0.75                               |                                  |   |
| 85.9        | 0.84                               |                                  |   |
| 86.6        | 1.09                               |                                  | Toe                                     |
| 87.2        | 1.53                               |                                  |   |
| 88.5        | 1.81                               | -1.37                            | Top of right bank                       |
| 89.5        | 1.61                               |                                  | Bench mark stake (ground), gravel splay |
| 91.5        | 1.89                               |                                  | Toe of splay                            |
| 95.0        | 1.37                               | -0.65                            | Scour area- large tree present          |
| 96.8        | 1.67                               |                                  |   |
| 99.0        | 1.57                               |                                  |   |
| 100.4       | 1.27                               | -1.33                            |   |
| 103.7       | 1.80                               |                                  |   |
| 108.5       | 1.72                               | -1.08                            |   |
| 109.5       | 1.55                               | -1.15                            |   |
| 119.5       | 1.59                               | -1.11                            |   |
| 129.5       | 1.19                               | 1.09                             |   |
| 139.5       | 0.96                               | 0.86                             |   |

Appendix D-4 Continued. Cross-section data for Site 3A.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes |
|-------------|------------------------------------|----------------------------------|-------|
| 149.5       | 1.34                               | 1.24                             |       |
| 154.5       | 2.34                               | 2.34                             |       |

Appendix D-5. Cross-section data for Site 3B.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal Relative<br>to TW<br>(m) | Notes                     |
|-------------|------------------------------------|----------------------------------|---------------------------|
| 0.0         | 2.79                               |                                  |                           |
| 7.0         | 2.75                               |                                  |                           |
| 9.3         | 2.56                               |                                  |                           |
| 11.0        | 2.33                               | 1.43                             | Bench mark stake (ground) |
| 12.5        |                                    | 0.99                             |                           |
| 14.0        | 2.26                               | 0.91                             |                           |
| 14.8        | 2.20                               | 0.85                             |                           |
| 15.5        | 1.82                               |                                  | Floodplain bench          |
| 16.6        | 0.85                               |                                  | Edge of water             |
| 16.7        | 0.68                               |                                  | Toe                       |
| 18.2        | 0.09                               | -0.26                            |                           |
| 20.8        | 0.00                               | -0.65                            |                           |
| 22.5        | 0.22                               |                                  |                           |
| 26.0        | 0.59                               |                                  | Toe                       |
| 27.9        | 1.57                               |                                  |                           |
| 30.2        | 2.13                               | -1.02                            | Edge of water             |
| 35.3        | 1.55                               | -0.55                            |                           |
| 39.0        | 1.53                               |                                  |                           |
| 44.0        | 1.66                               |                                  |                           |
| 48.0        | 1.58                               | -1.07                            |                           |
| 55.0        | 1.65                               |                                  |                           |
| 67.0        | 1.52                               | -0.83                            | BM stake (ground)         |
| 72.0        | 1.54                               |                                  |                           |
| 77.0        | 1.54                               |                                  |                           |
| 83.0        | 1.49                               | -1.28                            |                           |
| 89.0        | 1.40                               | -0.83                            |                           |
| 94.0        | 1.46                               |                                  |                           |
| 99.0        | 1.61                               |                                  |                           |
| 104.0       | 1.45                               |                                  |                           |
| 107.0       | 1.31                               |                                  | Toe of flood chute        |
| 111.0       | 0.98                               | -1.12                            | Thalweg of flood chute    |
| 117.0       | 1.06                               |                                  |                           |
| 120.0       | 1.11                               |                                  |                           |
| 123.0       | 1.00                               | 0.98                             |                           |
| 126.0       | 1.15                               |                                  |                           |
| 129.0       | 1.33                               |                                  |                           |
| 131.5       | 1.67                               |                                  |                           |

Appendix D-5 Continued. Cross-section data for Site 3B.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal Relative<br>to TW<br>(m) | Notes |
|-------------|------------------------------------|----------------------------------|-------|
| 133.5       | 2.21                               |                                  |       |
| 135.5       | 2.91                               |                                  |       |

Appendix D-6. Cross-section data for Site 4A.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal Relative<br>to TW<br>(m) | Notes             |
|-------------|------------------------------------|----------------------------------|-------------------|
| 0.0         | 3.07                               | 0.52                             | Stake             |
| 3.0         | 2.84                               |                                  |                   |
| 7.0         | 2.93                               | 0.38                             |                   |
| 10.7        | 2.69                               | 0.49                             |                   |
| 11.4        | 2.59                               |                                  |                   |
| 12.0        | 2.58                               |                                  | Bankfull          |
| 12.7        | 0.93                               |                                  |                   |
| 13.0        | 0.61                               |                                  | Toe               |
| 19.0        | 0.00                               | -1.25                            | Thalweg           |
| 21.8        | 0.04                               |                                  |                   |
| 22.9        | 0.18                               |                                  | Toe               |
| 23.2        | 1.00                               |                                  | Bench             |
| 23.4        | 1.00                               |                                  | Bench (added pt)  |
| 24.2        | 1.90                               |                                  |                   |
| 25.5        | 2.38                               | -0.68                            | Top of right bank |
| 26.3        | 2.33                               | -0.77                            |                   |
| 27.4        | 2.04                               |                                  |                   |
| 28.6        | 1.72                               |                                  | Toe of berm       |
| 32.0        | 1.59                               |                                  |                   |
| 36.0        | 1.53                               | -1.17                            |                   |
| 42.0        | 1.62                               |                                  |                   |
| 49.0        | 1.73                               |                                  |                   |
| 55.0        | 1.78                               | -0.87                            |                   |
| 62.0        | 1.84                               |                                  |                   |
| 65.5        | 1.92                               |                                  |                   |
| 68.3        | 2.40                               | 0.00                             |                   |
| 75.0        | 2.50                               | 0.40                             |                   |

Appendix D-7. Cross-section data for Site 4B.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal Relative<br>to TW<br>(m) | Notes                            |
|-------------|------------------------------------|----------------------------------|----------------------------------|
| 0.0         | 3.40                               | -0.03                            |                                  |
| 2.8         | 3.20                               |                                  |                                  |
| 6.5         | 2.90                               |                                  |                                  |
| 10.5        | 2.90                               | 0.04                             | Bench mark stake (ground)        |
| 12.0        | 2.60                               |                                  |                                  |
| 14.1        | 2.10                               |                                  |                                  |
| 15.0        | 1.70                               |                                  |                                  |
| 16.4        | 1.40                               | -0.05                            |                                  |
| 18.2        | 1.30                               | -0.86                            | Edge of water                    |
| 19.1        | 0.90                               |                                  | Toe                              |
| 21.3        | 0.60                               |                                  |                                  |
| 23.0        | 0.20                               |                                  |                                  |
| 24.0        | 0.20                               |                                  |                                  |
| 25.3        | 0.00                               | -1.10                            | Thalweg                          |
| 26.0        | 0.30                               |                                  | Toe                              |
| 27.3        | 1.10                               |                                  | Edge of water                    |
| 28.2        | 2.60                               |                                  |                                  |
| 29.5        | 2.60                               |                                  |                                  |
| 32.9        | 2.20                               | -0.15                            |                                  |
| 35.7        | 2.40                               |                                  |                                  |
| 40.3        | 2.60                               | -0.82                            |                                  |
| 44.0        | 2.50                               |                                  |                                  |
| 48.5        | 2.40                               |                                  |                                  |
| 51.7        | 2.40                               | 0.90                             | Intersection of Site 3 at 90.3 m |
| 56.1        | 2.50                               |                                  |                                  |
| 61.2        | 2.60                               | 0.10                             |                                  |
| 65.0        | 2.50                               |                                  |                                  |
| 72.6        | 2.40                               | -0.21                            |                                  |
| 78.4        | 2.61                               |                                  |                                  |
| 84.0        | 2.64                               |                                  |                                  |
| 91.0        | 2.81                               |                                  |                                  |
| 94.0        | 3.04                               |                                  |                                  |
| 96.0        | 3.31                               | 0.32                             | Bench mark                       |

Appendix D-8. Cross-section data for Site 4C.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes             |
|-------------|------------------------------------|----------------------------------|-------------------|
| 0.0         | 2.55                               | -0.85                            |                   |
| 6.0         | 2.46                               | -0.84                            |                   |
| 7.6         | 2.18                               |                                  |                   |
| 11.0        | 2.05                               |                                  |                   |
| 13.0        | 1.98                               | -0.94                            |                   |
| 15.0        | 2.03                               |                                  |                   |
| 17.5        | 1.95                               | -0.75                            | Trail             |
| 19.8        | 1.83                               |                                  | Top of left bank  |
| 20.2        | 0.18                               | -1.82                            | Toe               |
| 21.0        | 0.02                               | -1.18                            | Thalweg 1         |
| 22.3        | 0.20                               |                                  |                   |
| 23.7        | 0.36                               |                                  |                   |
| 26.1        | 0.28                               | -0.82                            |                   |
| 27.8        | 0.00                               | 0.00                             | Thalweg 2         |
| 28.9        | 0.23                               |                                  | Toe               |
| 29.3        | 0.43                               |                                  | Edge of water     |
| 29.7        | 0.83                               |                                  |                   |
| 30.0        | 0.93                               |                                  |                   |
| 30.5        | 1.13                               | 0.73                             | High Bf           |
| 31.7        | 0.95                               |                                  |                   |
| 31.7        | 0.98                               |                                  |                   |
| 32.6        | 1.23                               |                                  |                   |
| 32.8        | 1.43                               |                                  |                   |
| 33.2        | 1.73                               |                                  |                   |
| 33.3        | 1.93                               | -1.07                            |                   |
| 33.8        | 1.83                               |                                  | Top of right bank |
| 35.4        | 2.13                               |                                  |                   |
| 37.5        | 1.53                               |                                  | End of tape       |



Appendix D-9. Cross-section data for Site 4D.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                    |
|-------------|------------------------------------|----------------------------------|--------------------------|
| 0.0         | 2.85                               | -0.65                            | Rebar stake              |
| 5.0         | 2.91                               | -1.34                            | Middle of trail          |
| 7.75        | 2.92                               |                                  | Top of left bank         |
| 9.0         | 0.43                               |                                  | Toe                      |
| 10.2        | 0.10                               | -1.00                            | Thalweg                  |
| 12.0        | 0.00                               |                                  |                          |
| 13.6        | 0.72                               |                                  |                          |
| 15.3        | 0.80                               | 0.19                             | Low bar surface          |
| 17.5        | 0.92                               |                                  |                          |
| 21.0        | 1.11                               |                                  | High bar surface         |
| 23.2        | 1.33                               |                                  |                          |
| 26.6        | 1.23                               | 0.93                             | Active floodplain; fines |
| 30.0        | 1.84                               |                                  |                          |
| 33.0        | 2.70                               | -1.35                            | Top of right bank        |
| 40.0        | 2.91                               |                                  |                          |
| 50.0        | 2.92                               |                                  |                          |
| 60.0        | 2.93                               | 2.43                             |                          |
| 70.0        | 3.02                               | 2.82                             |                          |
| 75.0        | 3.13                               | 3.03                             |                          |
| 80.0        | 3.51                               |                                  | Bluff                    |

Appendix D-10. Cross-section data for Site 5.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes                           |
|-------------|------------------------------------|----------------------------------|---------------------------------|
| 0.0         | 4.31                               | 2.76                             | Field                           |
| 10.0        | 5.03                               |                                  |                                 |
| 12.4        | 5.06                               | 2.91                             | Bench mark 1 stake              |
| 12.75       | 5.00                               |                                  | Top of bank                     |
| 17.5        | 0.66                               |                                  | Toe                             |
| 18.6        | 0.45                               |                                  | Thalweg                         |
| 21.8        | 0.77                               |                                  | Bar                             |
| 24.5        | 1.22                               | 0.62                             | Bar                             |
| 26.6        | 1.33                               |                                  | Toe                             |
| 27.6        | 1.65                               |                                  |                                 |
| 30.9        | 3.92                               | 1.52                             | Top of bank                     |
| 40.0        | 4.11                               |                                  |                                 |
| 50.5        | 3.74                               | 0.81                             |                                 |
| 60.7        | 3.47                               | 0.27                             | Bench mark 2 stake              |
| 63.8        | 3.40                               |                                  | Top of bank                     |
| 66.55       | 0.73                               |                                  | Toe                             |
| 70.5        | 0.48                               | 0.48                             | Thalweg                         |
| 71.1        | 0.69                               |                                  |                                 |
| 76.2        | 0.95                               |                                  | Low bar                         |
| 78.0        | 1.07                               | 1.07                             | Toe                             |
| 78.7        | 1.45                               | 1.25                             | Bankfull indicator              |
| 83.5        | 2.10                               |                                  |                                 |
| 85.0        | 2.14                               | 1.92                             |                                 |
| 87.0        | 2.38                               |                                  |                                 |
| 89.0        | 2.80                               |                                  |                                 |
| 91.0        | 3.01                               |                                  |                                 |
| 93.0        | 3.29                               | 1.01                             |                                 |
| 98.0        | 3.45                               |                                  |                                 |
| 103.0       | 3.43                               | 0.92                             |                                 |
| 107.0       | 3.07                               |                                  |                                 |
| 108.5       | 2.80                               |                                  |                                 |
| 110.0       | 2.79                               |                                  |                                 |
| 113.3       | 2.91                               | 1.24                             | Bench mark 3 stake; top of bank |
| 115.9       | 0.24                               | -0.76                            | Toe                             |
| 117.1       | 0.04                               | -0.76                            |                                 |
| 119.1       | 0.11                               | -0.29                            |                                 |
| 121.0       | 0.00                               |                                  | Thalweg                         |

Appendix D-10 Continued. Cross-section data for Site 5.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes       |
|-------------|------------------------------------|----------------------------------|-------------|
| 123.1       | 0.24                               |                                  | Toe         |
| 123.3       | 1.13                               |                                  |             |
| 127.3       | 3.59                               |                                  |             |
| 130.3       | 4.29                               |                                  | Top of bank |
| 135.3       | 4.29                               |                                  |             |

Appendix D-11. Cross-section data for Site 6.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes  |
|-------------|------------------------------------|----------------------------------|--|
| 0.0         | 3.52                               | 0.82                             | Field  |
| 28.0        | 3.74                               |                                  |  |
| 30.5        | 3.74                               | 0.33                             | Bench mark stake                                       |
| 42.0        | 3.24                               |                                  |  |
| 48.0        | 3.02                               | -0.13                            |  |
| 61.0        | 2.78                               | -0.43                            |  |
| 67.5        | 2.42                               | -0.57                            | Bench mark stake                                       |
| 70.7        | 1.75                               | -0.25                            |  |
| 76.1        | 1.68                               | -0.32                            | Top of left bank                                       |
| 77.6        | 1.05                               |                                  |  |
| 79.2        | 0.80                               |                                  | High bar   |
| 83.0        | 0.49                               |                                  |  |
| 86.6        | 0.13                               |                                  |  |
| 87.3        | 0.00                               | -0.95                            | Thalweg  |
| 87.9        | 0.30                               |                                  |  |
| 90.0        | 2.55                               | -0.23                            | Top of right bank                                      |
| 98.0        | 2.65                               |                                  |  |
| 108.0       | 2.12                               |                                  |  |
| 113.0       | 1.94                               | -1.26                            |  |
| 118.0       | 1.89                               |                                  |  |
| 128.0       | 1.75                               | -1.68                            |  |
| 135.5       | 1.98                               |                                  |  |
| 143.0       | 4.44                               |                                  | Peridge terrace (10 m NW and 4.5-5 m above last point) |

Appendix D-12. Cross-section data for Site BG1.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes            |
|-------------|------------------------------------|----------------------------------|------------------|
| 0.0         | 1.99                               | 0.74                             |                  |
| 2.2         | 1.95                               |                                  | Top of left bank |
| 2.4         | 1.26                               |                                  | Edge of water    |
| 3.2         | 0.70                               |                                  |                  |
| 3.5         | 0.38                               | 0.18                             | Toe              |
| 4.8         | 0.00                               | -0.10                            | Thalweg          |
| 6.9         | 0.38                               |                                  |                  |
| 8.4         | 0.61                               |                                  |                  |
| 9.6         | 0.99                               | 0.69                             |                  |
| 10.2        | 1.24                               | 0.64                             | Gravel Bar       |
| 11.2        | 1.47                               |                                  |                  |
| 12.0        | 1.59                               | 1.09                             | Gravel           |
| 14.0        | 1.61                               | 1.21                             | Gravel           |

Appendix D-13. Cross-section data for Site BG2.

| Tape<br>(m) | Elevation<br>Relative to TW<br>(m) | Refusal<br>Relative to TW<br>(m) | Notes             |
|-------------|------------------------------------|----------------------------------|-------------------|
| 0.0         | 1.37                               |                                  |                   |
| 2.0         | 1.18                               | 0.98                             |                   |
| 4.1         | 0.76                               | 0.56                             |                   |
| 5.8         | 0.78                               |                                  | Top of left bank  |
| 6.2         | 0.39                               |                                  |                   |
| 6.6         | 0.25                               |                                  | Edge of water     |
| 7.4         | 0.06                               | -0.14                            |                   |
| 9.3         | 0.16                               |                                  |                   |
| 12.0        | 0.00                               |                                  |                   |
| 13.6        | 0.09                               | -0.11                            |                   |
| 14.7        | 0.25                               |                                  | Edge of water     |
| 15.4        | 1.01                               |                                  |                   |
| 16.1        | 1.37                               | 1.07                             | Top of right bank |
| 19.0        | 1.37                               |                                  |                   |